

In-Harbor and At-Sea Electromagnetic
Compatibility Survey for
Maritime Satellite L-Band Shipboard Terminal

August 1974

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ELECTROMAGNETIC COMPATIBILITY SURVEY FOR
MARITIME SATELLITE L-BAND SHIPBOARD
TERMINAL (RCA Service Co., Inc.) 1
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Government Services Operations

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Springfield, Virginia

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FOREWORD

This technical report was prepared in the RCA Service Company, Government Services Operations facility, Springfield, Virginia on NASA Contract NAS5-24035. The work was administered under the direction of Mr. Ralph E. Taylor, Code 953, Mobile Radiodetermination Branch, Goddard Space Flight Center, Greenbelt, Maryland.

The survey reported herein was initiated in May 1974 and concluded in August 1974. The activity was carried out by James S. Hill with the assistance of Ernest C. Powell, Jr.

The author would like to acknowledge a number of helpful suggestions from Ralph E. Taylor, Daniel L. Brandel and James F. Cottrell of the NASA Goddard Space Flight Center from Commander Harry Feigleson of the Department of Commerce, Maritime Administration, Orest J. Hanas and Richard Husta of AII Systems, Incorporated, and Captain William Kolbe and Donald E. Kadlac of the United States Lines.

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1. Introduction

Two, geostationary, maritime satellites, one over the Pacific and one over the Atlantic Ocean will make available high-speed communications and navigation (position determination) services to ships at sea (e.g. Reference 1). A shipboard satellite terminal, operating within the authorized maritime L-band, 1636.5 to 1645.0 MHz, will allow ships to pass voice, teletype, facimile and data messages to shore communication facilities with a high degree of reliability. The shore-to-ship link will also operate in the maritime L-band from 1535.0 to 1543.5 MHz.

A significant number of maritime/commercial ships are expected to be equipped with an L-band satellite terminal by the year 1980. Consequently, there is an interest in determining electromagnetic compatibility (EMC) between the proposed L-band shipboard terminal and existing, on-board, shipboard communications/electronics and electrical systems, as well as determining the influence of shore-based interference sources.

The shipboard, electromagnetic interference (EMI) survey described in this report was conducted on-board the United States Line's American Leader class (15,690 tons) commercial container ship, the "American Alliance" from June 16 to 20, 1974. Reference 2 describes the Test Plan. The 1.2 meters (m)-diameter (4 Ft.),

Ref.1: David W. King, "Satellite Telecommunications-Marisat" pp. J1-J9, 1974 Florida RTCM Assembly Meeting, Radio Technical Commission for Marine Services, Washington, D.C. 20554.

Ref.2: "EMC Test Plan for Shipboard In-Harbor and At-Sea Measurements for L-Band Terminal", 12 June 1974, prepared for NASA/Goddard Space Flight Center, Greenbelt, Maryland by RCA Service Company on NASA Contract-24035.

paraboloid antenna, duplexer, low noise amplifier and down converter of a prototype L-band shipboard terminal were used in a series of EMI measurements to investigate interference to the ship's 10 cm wavelength (S-band) and 3 cm wavelength (X-band) radars, as well as potential interference to the L-band shipboard terminal. Field intensity measurements from 1-10 GHz were made; also, conducted emissions were made on the ship's power lines using a field intensity meter in the frequency range of 150 kHz to 32 MHz and a spectrum analyzer in the range up to 100 MHz. For comparison measurements were also made on land-based power lines in the frequency range of 150 kHz to 32 MHz.

Field intensity measurements were made at several locations suitable for installation of the L-band terminal on the ship's flying bridge and on the radar mast, as well as in a below-deck equipment storage room where part of the L-band shipboard terminal may be installed near two radar cabinets. An evaluation was made of band-pass and low-pass microwave filters installed in the L-band terminal to alleviate potential interference.

Antenna sky-noise temperature measurements were made at 1.6 GHz using the L-band shipboard terminal and a Dicke radio-meter type microwave noise-power test set. Measurements were made at sea and repeated again in USA harbors where land-based noise sources received by antenna back-and side-lobes increased the apparent sky-noise temperature.

2. Description of Equipment

Portions of an operational L-band shipboard terminal were supplied for the survey by AII Systems, Incorporated, Moorestown, New Jersey, under a Maritime Administration contract.

The typical L-band shipboard terminal has an above deck complement housed in a radome consisting of a steerable 1.2 m diameter dish antenna, an L-band transmitter, a duplexer, a low-noise amplifier (LNA) and power and control elements. The below deck equipment includes a down converter with local oscillator and modems for communication services such as telephone, teletype and facsimile as well as special distress, warning and navigation services.

For the purpose of this shipboard EMC survey only certain basic parts of the L-band shipboard terminal were required. The equipment supplied by AII Systems, Incorporated, consisted of the following:

1. One 1.2 m (4 Ft.) diameter parabolic dish reflector, containing a RHCP feed for L-band (1535 to 1660 MHz) operation. The RF feed was circularly polarized (right hand, RHCP) and the antenna gain was 24 dB above an isotropic at 1559 MHz. The antenna was mounted on a hand-steerable, azimuth-elevation tripod mount containing a yoke with a neck to fit the tripod clamp.

2. One TACO antenna mounting tripod, counterweighted and provided with graduated scales for positioning the antenna in azimuth and elevation.

3. One duplexer adjusted for a receive test frequency of 1559 MHz and a transmit test frequency of 1659 MHz (e.g. Ref. 3) used in ATS-6 satellite experiments. Insertion loss is 0.5 dB with

Ref.3: "System Design Plan for Modifications of the Maritime Satellite System (Phase III)" Maritime Administration, U.S. Dept. of Commerce Report No. MAR044-P-002A, Issued December 7, 1973.

a bandwidth of 20 MHz. There is 90 dB isolation between the transmit and receive ports.

4. One low-noise amplifier (LNA) with a noise figure of 3 dB and a gain of 29 dB. The 3 dB bandwidth is 190 MHz and the amplifier reaches 1 dB compression at 029 dBm input.

5. One 5 MHz master oscillator and phase locked loop. These items were not a part of the prototype L-band terminal but were available substitutes.

6. One down-converter to convert from 1559 MHz to an IF of 50 MHz. This unit is not part of the L-band terminal but is an available substitute. A typical operational L-band down-converter has an IF output of 70 MHz.

7. One power supply cabinet. This unit provides +24 V, +15 V, and -15 V power for the LNA, down-converter, master oscillator and phase locked loop.

8. One low-loss 1/2 inch diameter Foam Wellflex coaxial cable, 12 m long. The cable loss at 1559 MHz is 1.4 dB.

9. Band-Pass Filters, one with a band centered at 1559 MHz to use between the LNA and the down-converter and one centered at 50 MHz for the output of the down-converter.

10. Low-Pass Filters to insert in the system to control possible harmonic and spurious emission interference. These filters have a maximum insertion loss of 0.7 dB and a 3 dB bandwidth of DC to 2000 MHz.

A measurement made on the overall system from the duplexer antenna port to the down-converter output showed a gain of 42.5 dB at 1560 MHz. The 3 dB bandwidth was 6.87 MHz and the system noise figure was 5.9 dB.

An antenna stand was fabricated of "erector set" type of structural steel by NASA. This stand raised the base of the antenna tripod off the deck by 1.8 meters and put the swivel axis for the antenna 2.8 meters above the deck so that the antenna main lobe could clear the railing and surrounding obstructions.

The characteristics of the two radars installed on the "American Alliance" are given in Table 2-1. The radar antennas were located on the radar mast and platform. Photo 1-1 shows the S-band radar antenna on the top of the mast and the X-band radar on the forward end of the platform. The L-band 1.2 m diameter dish antenna can be seen below the platform. Direct line from the L-band antenna to the S-band antenna is 9.2 meters and to the X-band antenna 7.4 meters.

Table 2-1 Radiomarine Radar Characteristics

	<u>S-Band</u> <u>Type CRM-N2C-30</u>	<u>X-Band</u> <u>Model CR-104A</u>
Frequency, MHz	3050	9375
Peak Power, KW	30	40
Range, Nautical Miles	0.5, 1, 2/6, 16, 40	1, 2, 4/8, 20, 40
Pulse Duration, μ s	0.1/0.4	0.25/0.65
Rep. Rate	2000/1000	2000/800
Average Power, W	6/12	20/20
Receiver BW, MHz	12/3	2.5/8
Power Tube	6043 Klystron	725A Magnetron



Photo 1-1, Radar Antennas and Shipboard Satellite Terminal Dish Antenna

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Photo 1-2 shows the wheelhouse port side. The two radar displays appear in the center of the photo with the curtains partially drawn. Photo 1-3 shows the wheelhouse starboard side. The survey instrumentation was located in the far corner where the spectrum analyzer and oscilloscope camera can be seen in the photo. The deck just below and aft of the flying bridge is shown in Photo 1-4. The HF whip antenna on the left is used to receive on 4, 6, 9, 12, 16, and 22 MHz while the top loaded vertical antenna is used to transmit on these same frequencies. A UHF coaxial antenna is mounted on the port-side, king post and the long wire antennas are used in the MF range, 410 to 512 kHz. Photo 1-5 shows the "erector set" antenna stand that was designed to elevate the L-band tripod and antenna above the railing. The antenna stand was lashed to the deck with wire rope.

3. Instrumentation

Four basic sets of instrumentation were used.

(1) Singer Stoddart NM-25T Radio Interference and Field Intensity Analyzer. This instrument covers a range of 150 kHz to 32 MHz. It was used with the Stoddart RF clamp-on current probe to measure power line conducted emissions.

(2) Singer Stoddart NM-65T Radio Interference Analyzer/Receiver. This instrument was used as a two-terminal voltmeter to measure signal and noise levels in the L-band terminal. It was also used with an L-band standard horn antenna and with a log-spiral conical antenna to measure field intensity in the storage room and above deck.

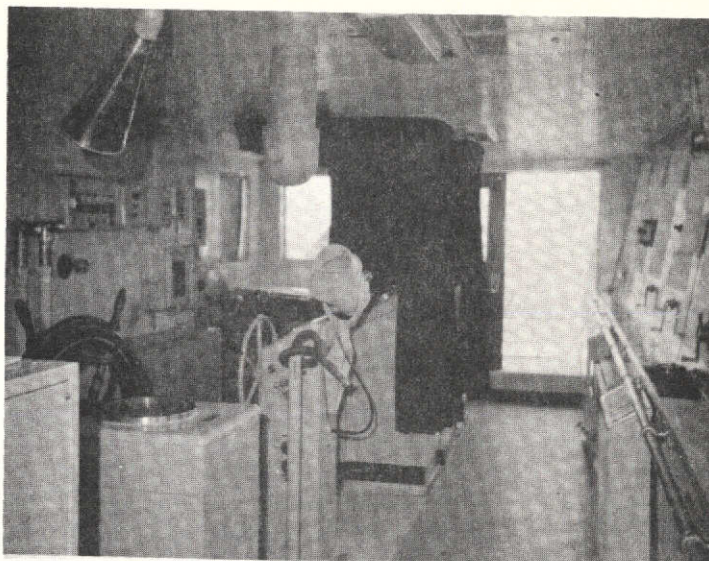


Photo 1-2, Wheelhouse, Port Side

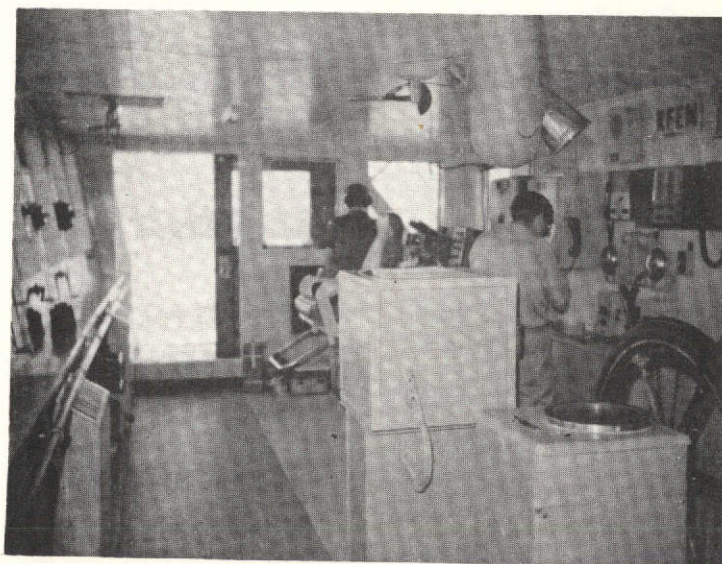


Photo 1-3, Wheelhouse, Starboard Side

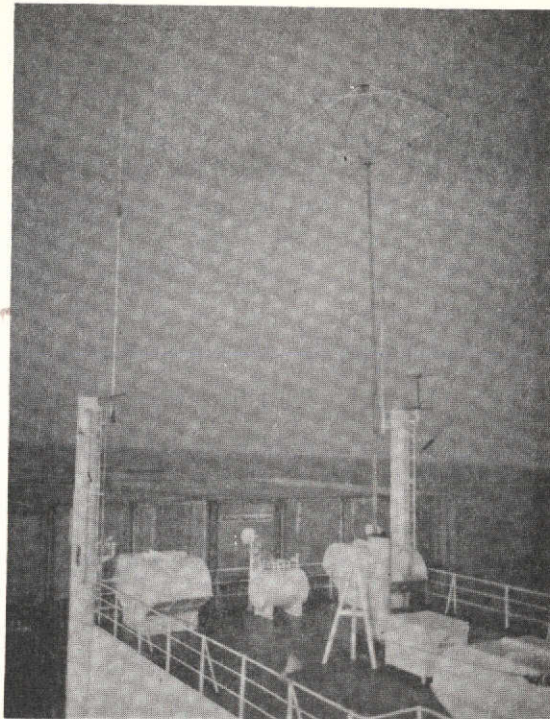


Photo 1-4, Antennas on Afterdeck

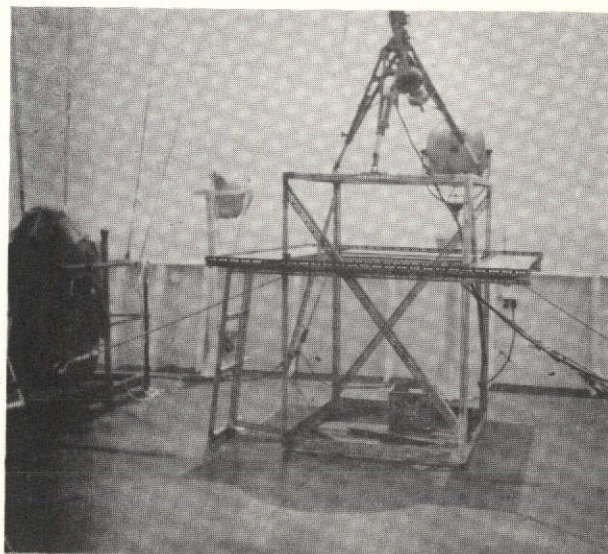


Photo 1-5, Antenna Stand with Tripod

(3) Hewlett-Packard Spectrum Analyzer consisting of the 8445B Automatic Preselector, 8555A Tuning Section, 8552B IF Section, 141T Variable Persistence Display Section, and a 196B Oscilloscope Camera. This instrument was used as a two terminal voltmeter to measure signal and noise levels in the L-band terminal. It was also used with the standard antennas to measure field intensity and with the clamp-on current probe to measure conducted emissions.

(4) AIL Type 2392B Radiometer Serial No. 124. This instrument was used as a noise power meter to establish a reference level of noise power from the L-band antenna and to match this reference level with noise power from the cold reference load through the ARRA Variable Attenuator Model 5614-60L, Serial No. 37. The Hewlett-Packard 7034A X-Y Recorder was used as an output indicator with the radiometer.

In addition to these basic systems the following ancillary items of equipment were used.

EMC Model 1000 tripod and pan-tilt head

EMC Model 1010 horn antenna, 1-2.5 GHz

EMC Model 1200 log-spiral conical antenna, 1-10 GHz

Hewlett-Packard Model 7034A X-Y recorder, serial no.
948-00112

Composite cold reference 50-ohm load

AIL type 124 power oscillator, 200-2500 MHz.

All instrumentation which was used for voltage level measurement was within the calibration period.

4. Description of Measurements

All of the measurements were made on-board the ship "American Alliance". The survey team boarded the ship when it docked at Port Elizabeth, N. J., at 0600 hours on Sunday June 16, 1974 and started the measurement program while the ship was docked. The measurements were continued while the ship was underway to Tioga Terminal in Philadelphia, PA, continued while the ship was docked there, while the ship was underway to Savannah, GA, and concluded with the ship docked in the Savannah harbor.

Five different categories of measurements were made as planned for the survey. Each of these was designed to collect specific information required for development of plans for the installation of the L-band satellite terminal on shipboard with a minimum amount of mutual interference with shipboard systems. The conducted emission measurements should be helpful to equipment designers to prevent possible interference with the L-band terminal from power-line conducted interference. The field intensity measurements show the potential of interference from the radar-radiated signals to the L-band terminal located near the radar platforms or on the starboard side of the flying bridge. Field intensity measurements made near the radar cabinets in the storage room should help the designer determine the degree of shielding required in the L-band terminal equipment cabinet. Filter evaluation measurements give information on the effectiveness and requirement for additional filtering in the front end, radio-frequency (RF) section of the L-band terminal. The antenna sky-noise temperature measurements give galactic (natural) and

man-made noise-level information. The possibility of interference to the radars by the L-band system was investigated by observation of the radar displays while a simulated L-band terminal signal was radiated.

A detailed description of these measurements is given in the following subsections.

4.1 Conducted Emissions

This test was run to investigate the conducted emission on the ship's power lines so that power line filters could be specified if required for the L-band terminal. For a comparison, measurements were also made of conducted emission on a power line in the RCA calibration laboratory, Springfield, Virginia.

The conducted measurements were made on the two radar units located in the storage room directly below the wheelhouse. Photos 4.1-1 and 4.1-2 show the S-band radar (left) and the X-band radar (right). A Stoddart clamp-on probe was clamped around each input power line on both radars to sample the interference current. Photo 4.1-3 shows the clamp-on probe coupled to an X-band radar power line. In Photo 4.1-4 the probe is coupled to an S-band radar power line. A tunable RF voltmeter, the Stoddart NM-25T, was used with the probe to investigate the spectrum from 150 kHz to 32 MHz. The Stoddart NM-25T is shown in Photo 4.1-5 with the H-P model 7034A X-Y recorder which plotted a chart for each of the 8 bands covering the 150 kHz to 32 MHz range. Since the intermediate frequency output of the L-band terminal down-converter is 70 MHz there is an interest in power line conducted emission near this frequency. The H-P 141T spectrum analyzer in combination with the Stoddart current probe was used for this purpose.

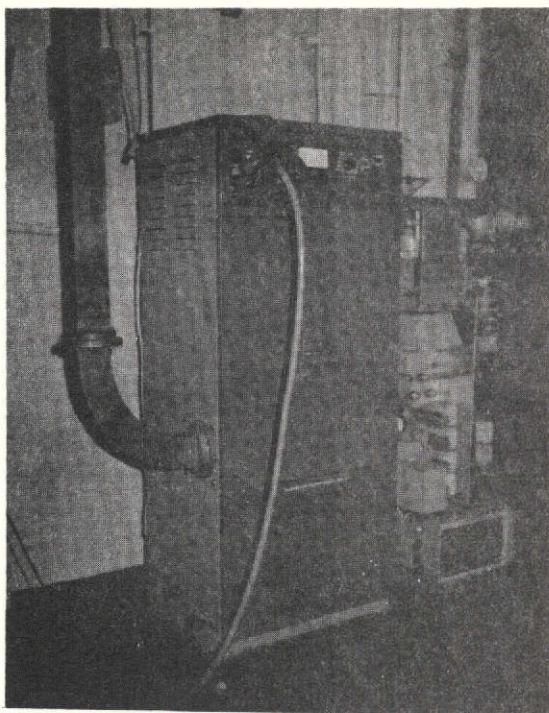


Photo 4.1-1, S-Band Radar
Cabinet in Foreground

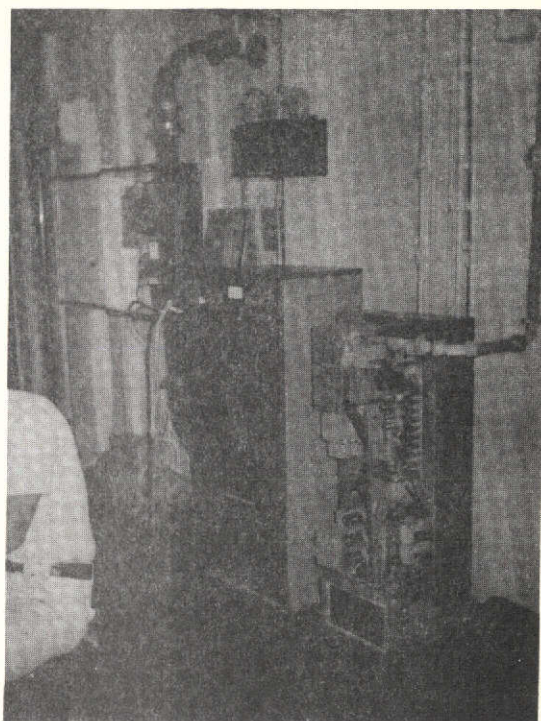


Photo 4.1-2, X-Band Radar
Cabinet in Foreground

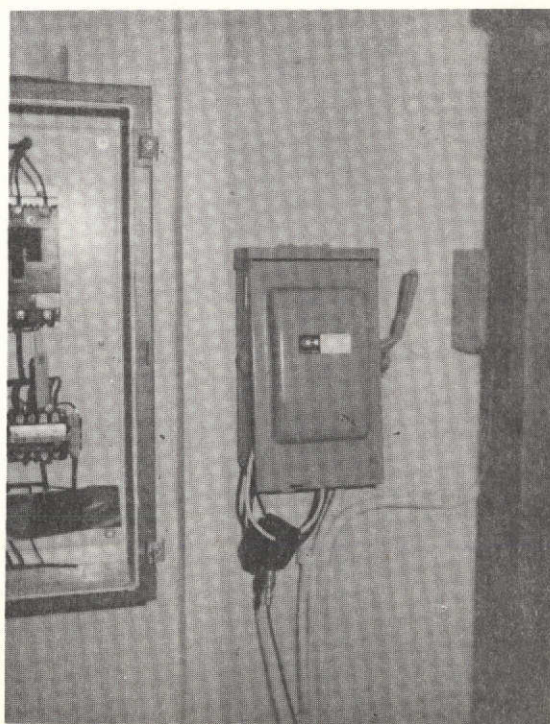


Photo 4.1-3, Current Probe on
X-Band Radar Power Line

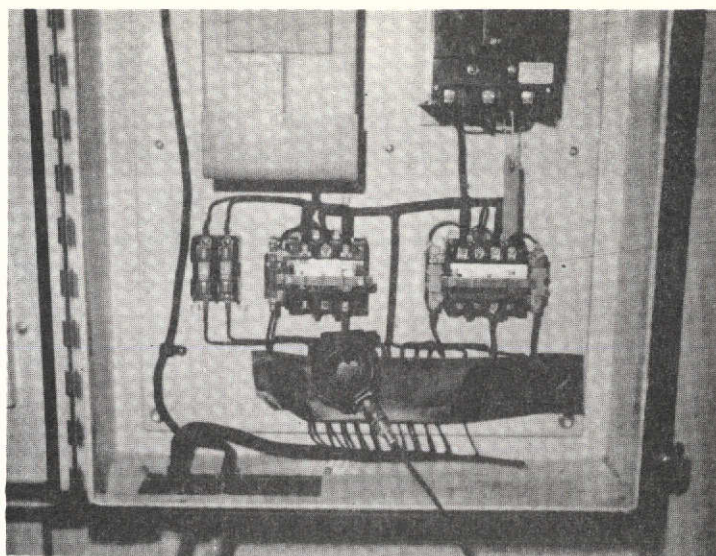


Photo 4.1-4, Current Probe on S-Band
Radar Power Line

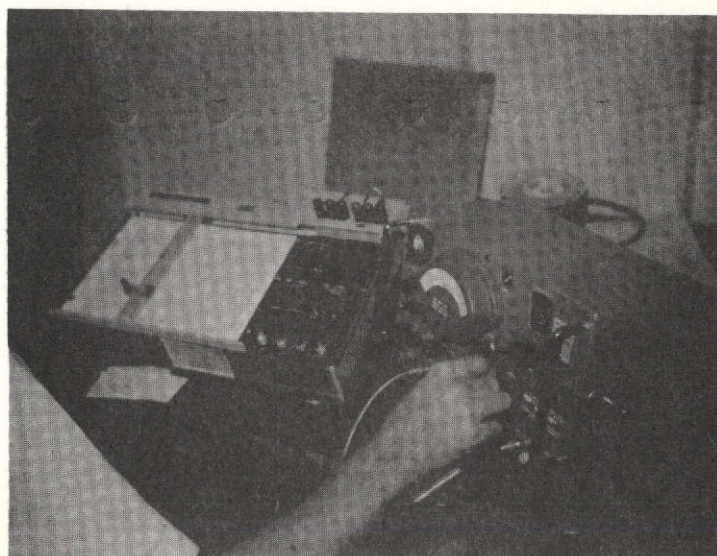


Photo 4.1-5, H-P 7034A X-Y Recorder
and Singer Stoddart NM-25T

4.1.1 Conduct of Test

Measurements were made on the X-band radar power lines while the radar was operating. A chart was made for each band of the NM-25T in the field intensity (FI) and again in the quasi-peak (QP) mode. In some cases, it was possible to run both records on one chart. After making the measurements on the black and white power lines, the two sets of results were compared; it was evident that they were similar and that either describes the interference existing on the power lines.

Consequently, the first measurements on the S-band radar T1 and T2 power lines were examined to determine if they were independent. Because of the similarity, only one line, T2, was measured completely. As a basis of comparison, the conducted emission on a similar power line in the RCA calibration laboratory was measured; a complete set of FI and QP charts was made on the black power line.

The resulting charts are included in Appendix A. Charts A-1 through A-15 were taken on the black power line, while Charts A-16 through A-30 are for the white power line of the X-band radar. The results of the S-band power line measurement are shown in Charts A-31 through A-41. Charts A-42 through A-52 were obtained in RCA's laboratory. Following the charts are the Spectrum Displays. Spectrum Displays A-1 and A-2 show the conducted emission from 0 to 100 MHz on the S-band and X-band radar power lines respectively as coupled into the clamp-on current probe; the reference level in each case being -30 dBm. Spectrum Displays A-3 and A-4 were made at a center frequency of 70 MHz with 5 MHz per division scan width to give a more detailed picture of the interference near 70 MHz, the reference level being -50 dBm.

4.1.2 Analysis

The X-Y charts have a vertical scale in decibels referenced to one microvolt, meter scale. To this has been added the attenuator setting, which in this set of measurements is -20, zero, or +20 dB. The FI trace on the chart can then be read in terms of decibels referenced to 1 μV (dB/ μV) for a two-terminal voltmeter. The QP trace must be adjusted by the attenuator setting plus 46 dB* as a bandwidth compensation factor to give the broadband emission level in dB/ μV /MHz. In order to convert the chart data to decibels referenced to 1 μA (dB/ μA), an adjustment must be made for the transfer impedance of the current probe. The calibration curve for the current probe is shown as Chart A-53. The adjustment factors for the bands have been quantized as shown on the chart. The adjustment for the first band, 0.15 to 0.305 kHz is 8 dB. Since the current, I , is equal to the voltage, E , divided by the impedance, Z , or $I=E-Z$ (in dB), the adjustment factor is subtracted from the sum of the meter reading and the attenuator setting. For the broadband conducted emission level in dB/ μA /MHz the bandwidth compensation factor of 46 dB* must be added. A similar data reduction process is employed for each band using the proper current probe transfer impedance factor.

Spectrum Displays A-1 through A-4 require an adjustment factor for the transfer impedance of the current probe in addition to an adjustment for bandwidth. Reference is made to Chart A-53 for the current probe transfer impedance. The bandwidth was adjusted by adding 20 dB to convert from 100 kHz (spectrum analyzer bandwidth)

*For impulse type broadband interference the data is a function of instrument impulse bandwidth. The impulse bandwidth of the NM-25T is 5 kHz. The bandwidth adjustment factor, BWF, to convert this data to the conventional dB/ μV /MHz is determined as follows:

$$\begin{aligned}\text{BWF} &= 20 \log 1 \text{ MHz} - 20 \log \text{BW (dB)} \\ &= 60 - 14 \text{ dB (for BW of 5 kHz)} \\ &= 46 \text{ dB}\end{aligned}$$

where BW the bandwidth of the measuring instrument

to 1 MHz bandwidth. Thus at 70 MHz the adjusted level is:

	<u>S-band</u>	<u>X-band</u>
from display	-89 dBm	-90 dBm
conversion to microvolts	<u>107</u>	<u>107</u>
	18 dB/ μ V	17 dB/ μ V
current probe factor	<u>-14</u>	<u>-14</u>
	4 dB/ μ A	3 dB/ μ A
bandwidth adjustment	<u>20</u>	<u>20</u>
conducted interference	24 dB/ μ A/MHz	23 dB/ μ A/MHz

4.1.3 Comments

Conducted emission measurements showed that the ship's power lines were "noiser" than the commercial power lines in the RCA Service Company Calibration Laboratory, which would be considered as average for an industrial park area.

A comparison of QP and FI traces will identify transients and impulsive type emissions where peaks exist only on the QP trace and are not in evidence at the same frequency on the FI trace (see Charts A-16 and A-17). The shipboard power lines evidenced broadband conducted emissions (QP) that were typically 50 dB higher than the RCA power line in the lower frequency part of the range (compare Charts A-17 and A-42). In the upper part of the frequency range the shipboard power lines were 25 to 30 dB higher than the RCA power line (compare Charts A-29 and A-52). Narrowband conducted emissions did not differ by as much but if protection from conducted emission levels is required in new shipboard installations, the protection must be designed to protect from the most severe condition.

Notes were entered on some of the charts indicating time related transients as well as other identified interference sources such as foreign broadcast stations.

The spectrum display photos which show the spectrum from 0 to 100 MHz give a good overall "look" at the conducted emission level and its frequency distribution (see Spectrum Display A-1 and A-2). These measurements were made while the ship was at sea. Conducted emission on the power line may possibly be more intense while the ship is in the harbor with loading machinery operating.

4.2 Field Intensity Measurements

Field intensity measurements were made using the Singer Stoddart NM-65T Radio Interference Analyzer with a standard horn antenna for the L-band measurements and a broadband log-spiral conical antenna for the 1 to 10 GHz frequency range. Data was recorded on an X-Y recorder. Both field intensity (FI), average value, and direct peak (DP) were recorded on each chart. Measurements were made in three locations; (1) in the storage room where the radar cabinets were located, (2) on the starboard side of the flying bridge at a location indicated in Figure 4.2-1, and (3) two sites each 1.2 meters outboard of the radar platform (one starboard and one aft).

4.2.1 Storage Room Location

The S-band (10 cm) and X-band (3 cm) radar transmitter cabinets are both located in a storage room below the wheelhouse. Since this is the proposed location for part of the L-band shipboard terminal, there is an interest in the electromagnetic environment in which the L-band system would operate to determine effective shielding requirements. The measurements were made with the measurement antenna positioned one meter in front of each radar cabinet, as shown in Photo 4.2-1.

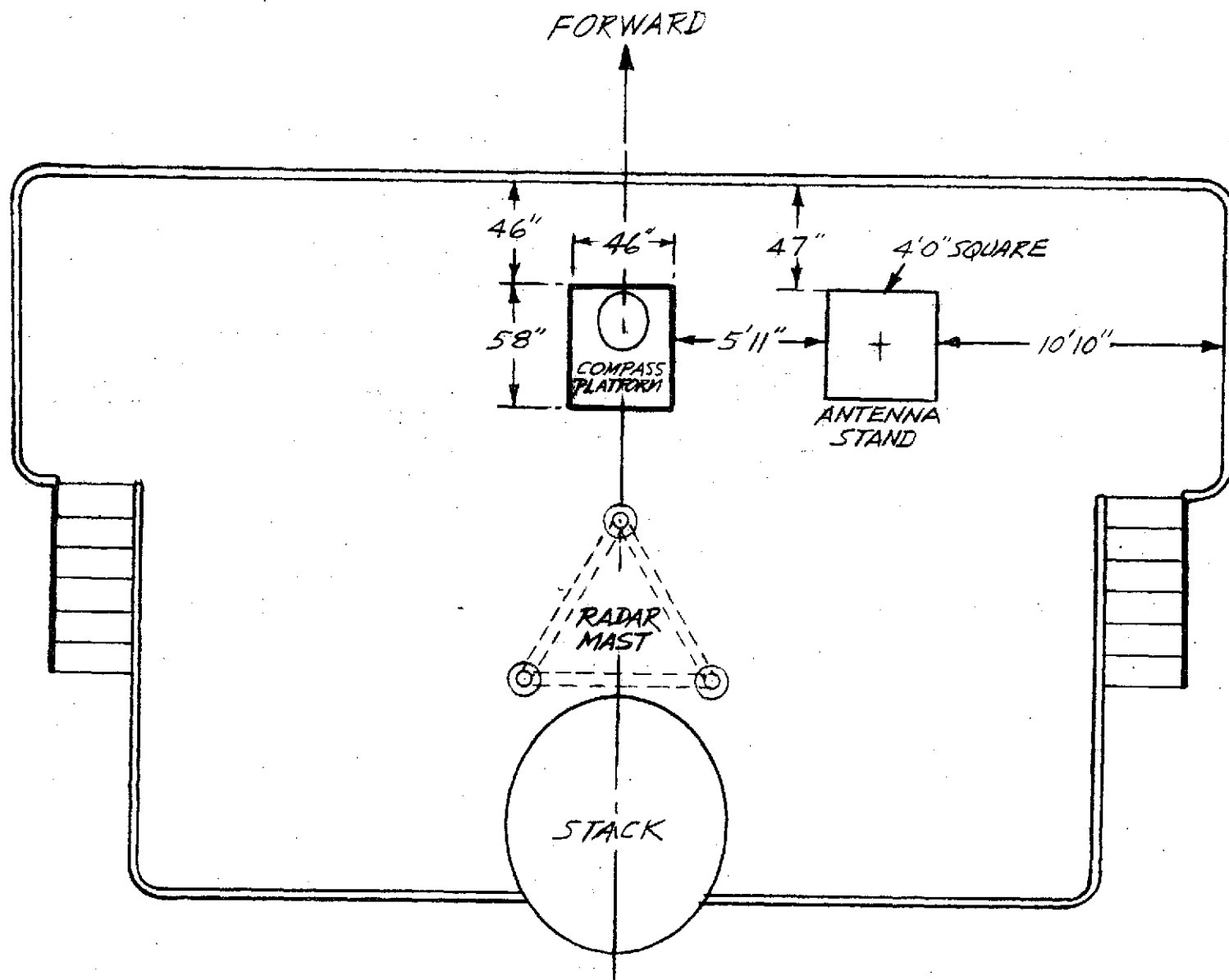


FIGURE 4.2-1
TOP VIEW OF FLYING BRIDGE
AND LOCATION OF ANTENNA STAND

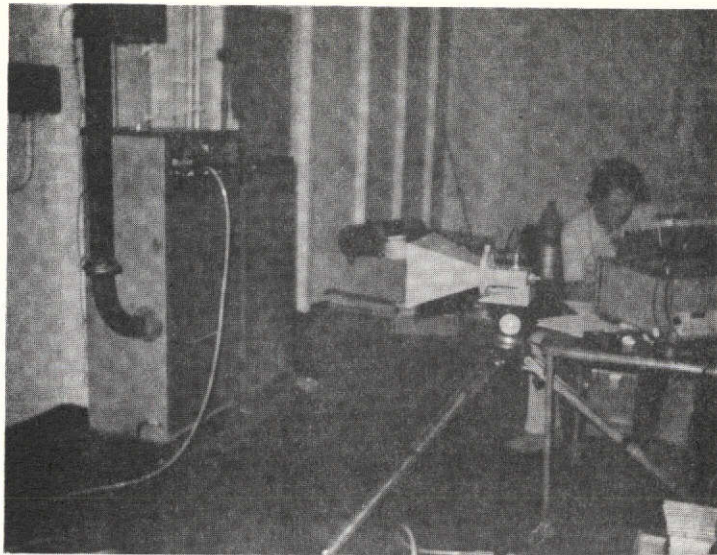


Photo 4.2-1, Radar Transmitter Cabinet
Field Intensity Measure-
ments with Horn Antenna

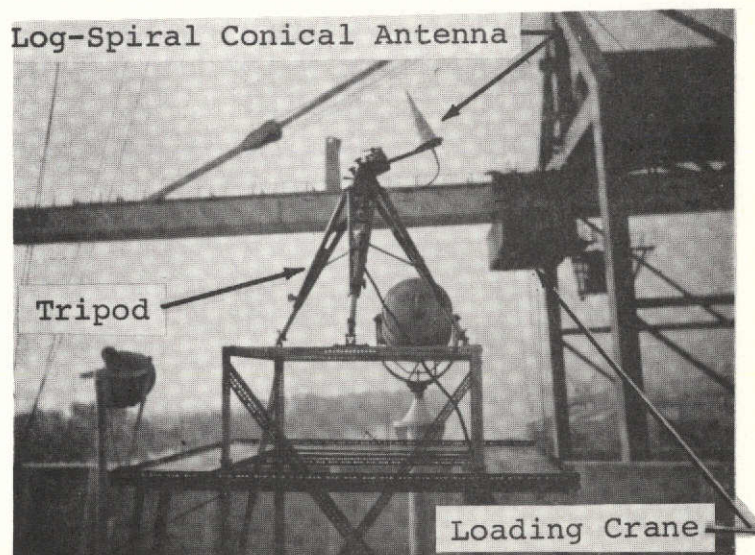


Photo 4.2-2, Field Intensity Measure-
ment with Log-Spiral Conical
Antenna on Starboard Side
of Flying Bridge

4.2.2 Flying Bridge Location

Measurements were made on the flying bridge at a location approximating the location on which an L-band terminal is being installed on a ship of the American Leader Class. These measurements will show the level of field intensity from the radars that must be withstood by the L-band terminal. As expected, the measurements indicate a worst case when the radar antennas face the L-band terminal antenna. Photo 4.2-2 shows the measurement antenna mounted on the tripod on the flying bridge.

4.2.3 Radar Platform Location

The radar platform is a possible location for the L-band terminal antenna. Measurements were made with the log-spiral conical antenna attached to a boom which was cantilevered out 1.2 meters aft of the platform and pointed to look at the radars as shown in Photo 4.2-3. For a second set of measurements, the boom was moved to a position 1.2 meters off the starboard edge of the platform and again pointed toward the radars as shown in Photo 4.2-4. A 15-meter-length of RG-214/U coaxial transmission line cable was used to connect the antenna to the field intensity meter located in the wheelhouse, as shown in Photo 4.2-5.

4.2.4 Conduct of Tests

Measurements were made with the NM-65T which was calibrated at 40 dB at 1 GHz. With this procedure it is necessary to make an adjustment in the data to compensate for the non-linearity of gain and of the calibration generator. Chart B-1 gives the adjustment factor curve to convert the data to field intensity where the horn antenna was used in the storage room.

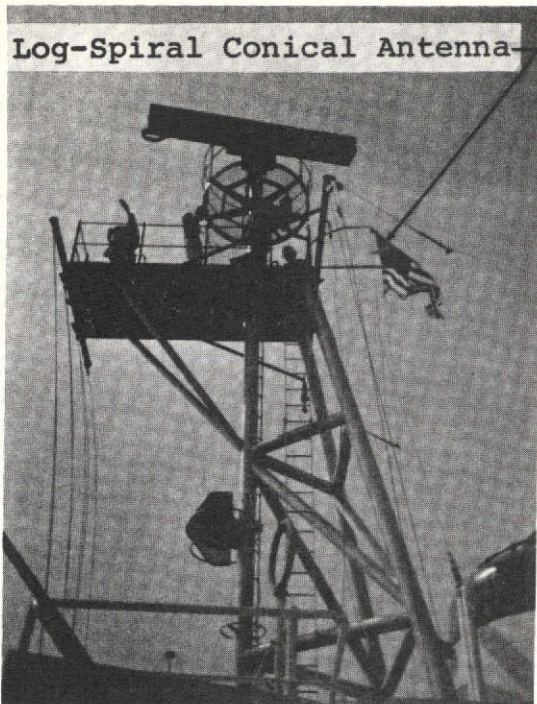


Photo 4.2-3, Field Intensity Measurement at Aft Position on Radar Platform

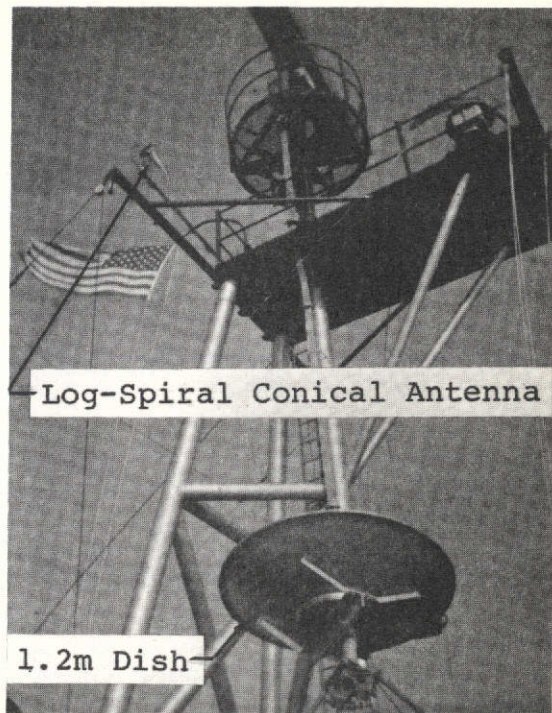


Photo 4.2-4, Field Intensity Measurement at Starboard Position on Radar Platform

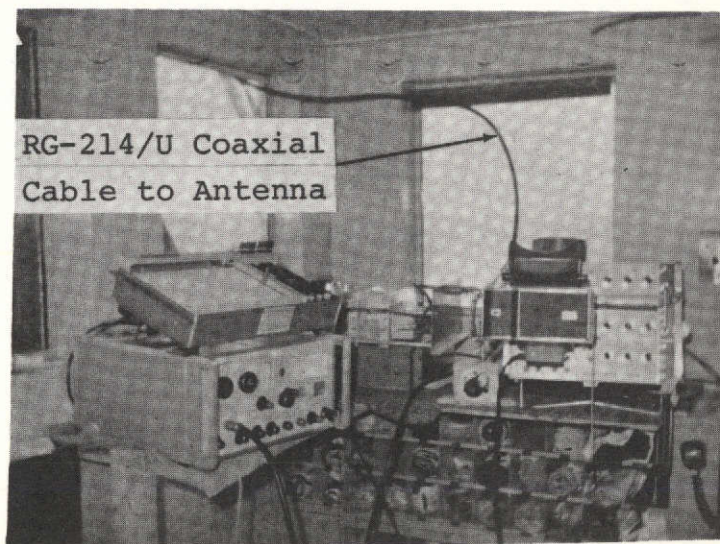


Photo 4.2-5, Instrument Setup in Wheelhouse for Field Intensity Measurement

Chart B-2 gives the adjustment factor curve to convert the data to field intensity where the log-spiral conical antenna was used. One curve applies to the storage room measurements where 3 meters of RG-9/U cable was used and the other curve applies to the radar mast measurements made using 15 meters of RG-214/U cable. Measurements on the starboard side of the flying bridge were made using the 12-meter-length of low-loss foam wellflex cable. The loss of this cable is within 1 dB of the loss of the 3 meter length of RG-9/U cable so the same antenna factor adjustment will be used for both of these cables. On each of these charts the ordinate scale on the left side is used to convert the meter reading to narrowband field intensity in dB/ μ V/m and the ordinate scale on the right side is used with the direct peak (DP) meter reading to convert to broadband field intensity in dB/ μ V/m/MHz.

4.2.5 Comments

Charts B-3 and B-4 were made with the antenna in front of the S-band radar with the radar off. Chart B-3 shows a signal at the S-band radar frequency. This is case radiation with the radar in standby mode. These should be compared with Charts B-5 and B-6, which were made with the radar on, where all the harmonics and spurious outputs clutter up the spectrum. The effect of the X-band radar is shown on Charts B-7 and B-8.

Chart B-9 shows the field intensity, at the starboard position on the flying bridge while the ship was in the Savannah harbor. The signal at 1.16 GHz, unidentified, was probably a radar at the nearby airbase or airport. The S-band radar signal, 91 dB/ μ V indicated on the meter, is 125.5* dB/ μ V/m/MHz and the

*The meter reading of 91 dB/ μ V is adjusted by the antenna factor, cable loss, and bandwidth factor plotted on Chart B-2. At 3050 MHz, the S-band radar frequency, this adjustment factor is 34.5 dB when the 12 m Foam Wellflex cable is used. $91 + 34.5 = 125.5$ (dB/ μ V/m/MHz)

X-band radar, 84 dB/ μ v indicated on the meter, is 125*dB/ μ v/m/MHz. Charts B-10 and B-11 were made to show field intensity at the radar platform level; aft and starboard sides respectively.

A summary of the broadband field intensity levels is given in Table B-1 below.

Table B-1

Broadband Field Intensity Levels in dB/ μ v/m/MHz at Selected Locations

<u>Location</u>	<u>1535-1660 MHz In-Band</u>	<u>3.1 GHz S-Band</u>	<u>9.5 GHz X-Band</u>
Storage Room			
1m from S-band radar	77.5	104.5	
1m from X-band radar	51		115
Flying Bridge			
Starboard Side	35	125.5	125
Radar Mast			
Aft	53.5	136.5	162
Starboard	52.5	131.5	157

Charts B-12 through B-15 were recorded in the Philadelphia harbor area on the Delaware River. Chart B-12 was made at 0930 hours while the antenna was directed toward the Ben Franklin Bridge, a major traffic artery, about 4 kilometers distant. Beyond the bridge the Philadelphia Naval Base is 12 kilometers distant and the Philadelphia International Airport is 16 kilometers distant. Charts B-13 and B-14 were taken with the antenna looking toward the downtown Philadelphia area. Chart B-15 was made as the ship was underway in the river and approaching the Ben Franklin bridge at a distance of 0.8 kilometers. Automobile and truck traffic on the bridge was normal for this time of day (1509 hours) and there was no indication of ignition interference

*The meter reading of 84 dB/ μ v is adjusted by the antenna factor, cable loss, and bandwidth factor plotted on Chart B-2. At 9375 MHz, the X-band radar frequency, this adjustment factor is 41 dB when the 12 m Foam Wellflex cable is used. 84+41 = 125 (dB/ μ v/m/MHz)

in the 1.3 to 1.9 GHz band. Even as the ship came closer to the bridge and passed under it there was no evidence on the meter or in the monitor headphones of impulsive type emissions.

4.3 Filter Evaluation

The purpose of this test was to evaluate the performance of the L-band shipboard terminal when low pass filters were inserted between various elements to provide additional protection from interference and to reduce L-band terminal interference to on-board radars.

The measurements were made with the 1.2 meter dish antenna mounted on the tripod which in turn was mounted on the metal stand on the starboard side of flying bridge deck. The antenna was pointed in the direction of the 3 cm and 10 cm (S- and X-band) wavelength radar antennas. The radar antennas were stopped from rotation and directed toward the L-band terminal antenna. Instrumentation was located in the wheelhouse as shown in Photo 4.3-1 and the 12-meter length of low-loss coaxial cable was used to connect the antenna to the EMI instrumentation located in the wheelhouse. A Hewlett-Packard Spectrum Analyzer and a Singer Stoddart NM-65T Radio Interference Analyzer were used to record data. Spectrum analyzer data was taken with a Polaroid camera while the radio interference analyzer data was taken with an X-Y recorder.

The L-band terminal is shown in block diagram form in Figure 4.3-1 with test points indicated. Low-pass (LP) filters are also shown with the point of insertion marked.

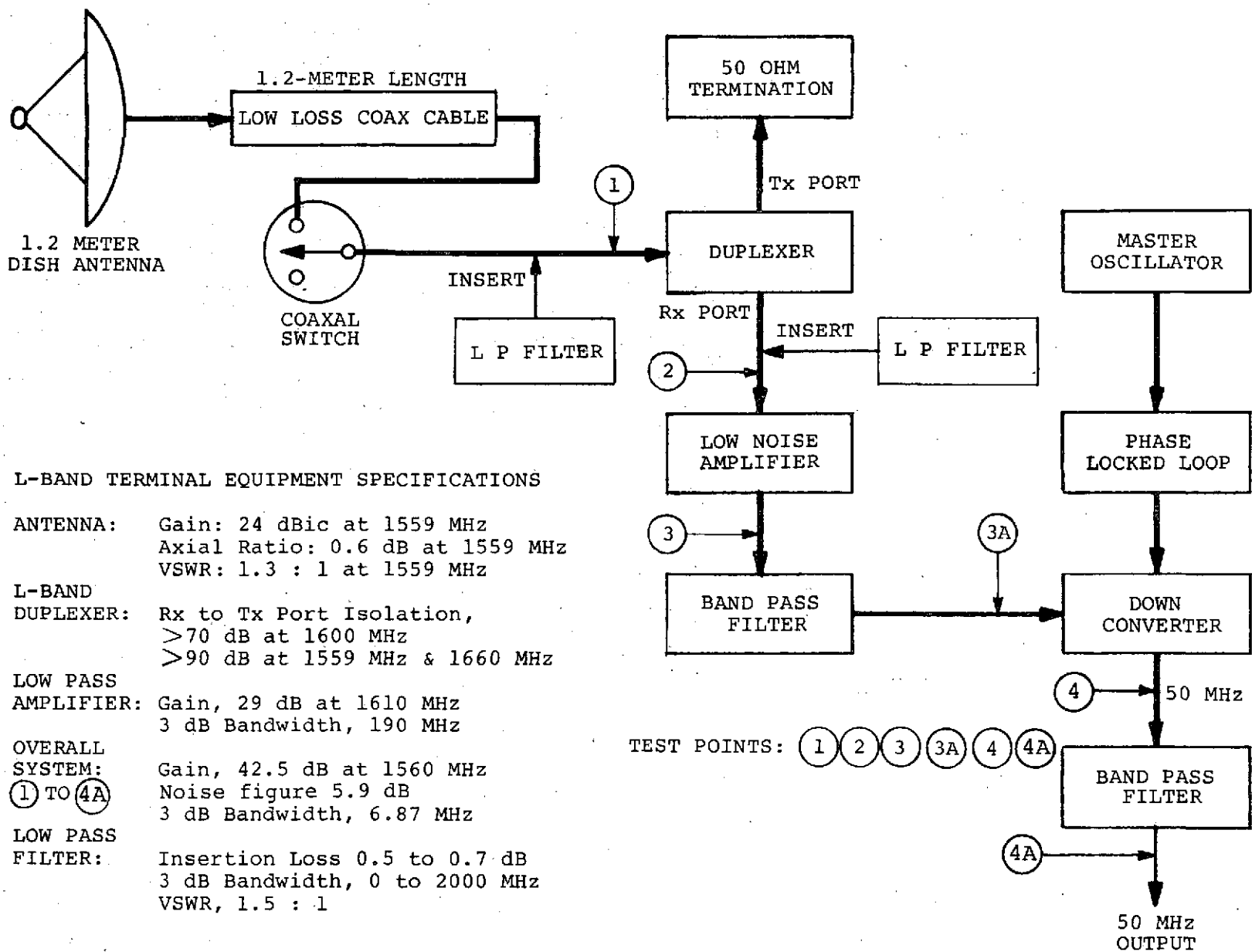


FIGURE 4.3-1 L-BAND SYSTEM

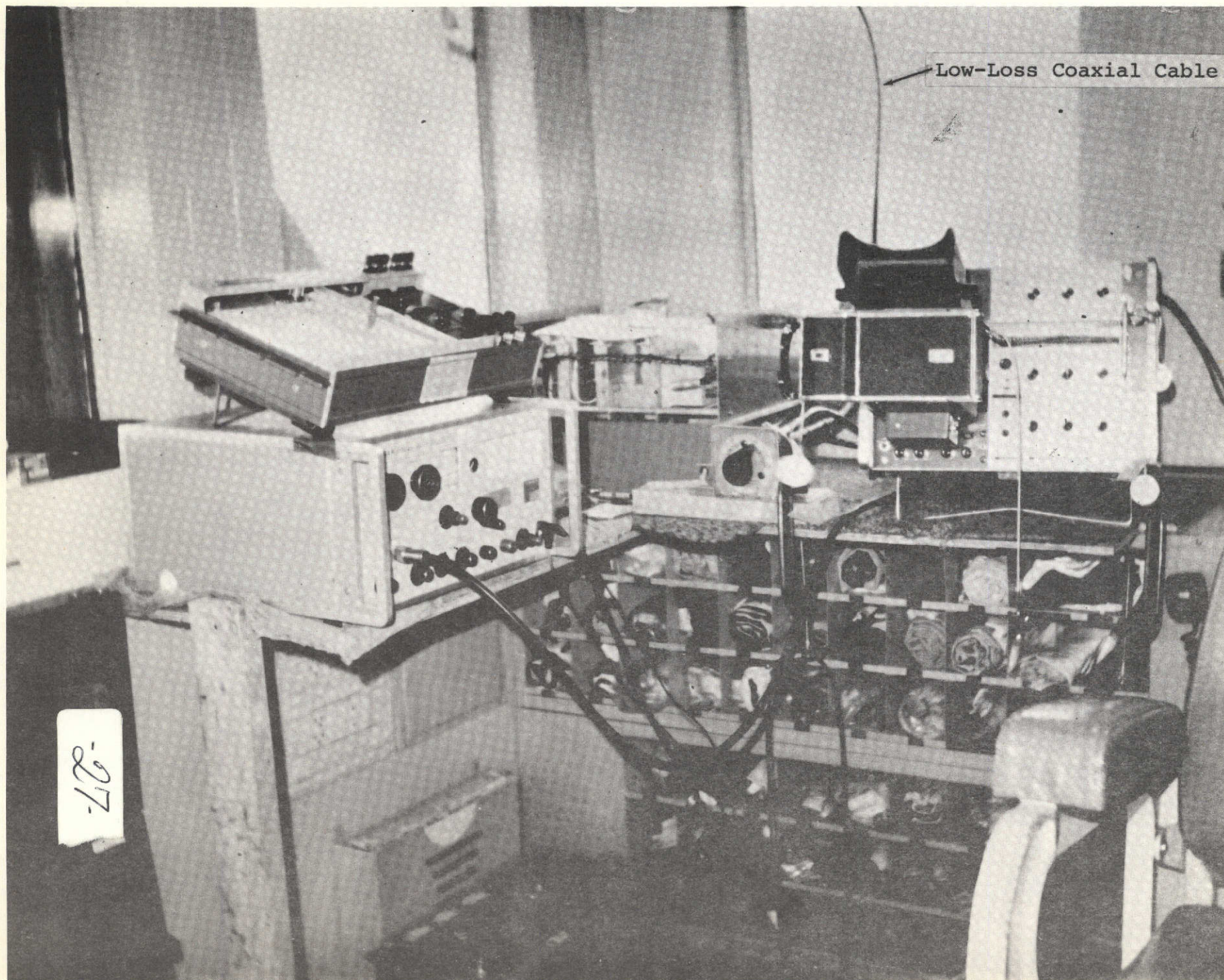


Photo 4.3-1 Instrumentation Setup in Wheelhouse for Filter Evaluation

4.3.1 Conduct of Test

The first measurements were made with the radars turned off and with the LP filters removed from the circuit. X-Y charts made under this condition show the ambient electromagnetic level in the Philadelphia harbor on the evening of June 17th as compared with the morning of June 18th in the harbor and again at sea on June 19th. A second set of measurements was made with the radars turned on while the measuring sets were connected to each test point in turn. It had been planned to insert an LP filter between the antenna and duplexer and between the duplexer and low noise amplifier in the receiving system. When the tests showed that only signals in the receive passband were getting through the duplexer, the second LP filter test was cancelled. It was also planned to insert a LP filter between the duplexer transmitter port and a power oscillator to investigate its effect on interference to the two radar sets. Since there was no interference to the radars without the filter it was not possible to test the effect of the filter in this position.

4.3.2 Analysis of Data

The X-Y charts are printed with a dB scale which is directly related to the meter scale of the Singer Stoddart NM-65T. The NM-65T was calibrated at 1 GHz at 40 dB. Since neither the gain of the NM-65T nor the output of the calibration generator is flat across the 1 to 10 GHz band it is necessary to make an adjustment which varies across the band, to convert the data to dB above 1 μ v at the input terminals of the NM-65T. The correction factors for the direct peak (DP) and field intensity (FI) functions are shown on an adjustment Chart C-23. This includes a factor of

14 dB to adjust from a receiver bandwidth of 5 MHz used for all of the measurements. By using an adjustment factor found on this chart it is possible to convert any data information taken from a chart into dB relative to one microvolt for the field intensity (FI) function or dB relative to one microvolt per megahertz for the direct peak (DP) function.

The data shown on the spectrum analyzer photographs can be read in relative amplitude directly from the photograph. The legend with each photograph notes operating parameters such as bandwidth, scan width and the reference level which is the top line on the grid. The scale is 10 dB per division. To convert to broadband voltage levels for impulsive signals, an adjustment of +20 dB must be made to convert from the 100 kHz to 1 MHz bandwidth. For example, an impulsive noise which shows a level of -60 dBm (47 dB/ μ V) on the spectrum analyzer display should be read as 67 dB/ μ V/MHz.

4.3.3 Comments

The X-Y charts were made by tuning the NM-65T across either the 1.3 to 1.9 GHz band or across the three bands that range from 1 to 10 GHz. The direct peak (DP) detector function was used for one scan trace and the field intensity (FI) for a second scan trace. The DP trace is easily identified by its irregularity consisting of short horizontal and vertical lines. These are a result of the circuit action in sampling the signal, holding, and dumping. This gives a response based on peak value and it is calibrated in RMS of an equivalent sine wave. A dump time of 0.3 seconds was selected. The field intensity (FI) function gives a smooth trace indicating the average value of the

signal. This is suitable for the measurement of narrowband or CW signals. The identification "field intensity" is misleading when the instrument is used as a two terminal voltmeter to measure signal levels that are not converted to field intensity.

The discussion which follows is related to the X-Y charts appearing in Appendix C. Charts C-1, C-2, and C-3 show signals that were found in the Philadelphia harbor at 2152 hours in the evening of June 17th and again at 0900 hours the following morning, June 18th, compared with midday at sea on June 19th, the following day. Chart C-4 shows the lack of in-band signals at sea. Charts C-5, C-6, and C-7 were made with the radar antennas rotating. It was evident that this procedure would not give consistent results because of the variation of signal as the NM-65T scans the band while antennas rotate so the antennas were stopped in a position facing the L-band antenna and the balance of the measurements were made in this condition. Charts C-8 and C-9 show the effectiveness of the filter between the antenna and the duplexer in reducing the signal from the radars. At test point 2 the radar signal has been filtered out and the insertion of the LP filter between the duplexer and the low-noise amplifier produces no noticeable effect as shown in Charts C-10, C-11, C-12, C-13, and C-14. Unidentified signals were found at test point 3. To allay the possibility that these were generated in the low noise amplifier, a spare amplifier-serial no. 010, was substituted for the original amplifier, serial no. 001. The chart record was unchanged and it was surmised that the spurious signals were coming from the down converter feeding forward. The results of this test are shown on Charts C-15 through C-21. Chart C-22 was made to

determine if the S-band radar would produce any in-band signal at the transmitter part of the duplexer.

4.4 Antenna Sky-Noise Temperature Measurements

Antenna sky-noise temperature measurements were made using parts of the L-band terminal and an AIL Type 2392B Radiometer as a noise power measuring device. The antenna-noise temperature measurement, T_A , is referenced to the antenna output terminals at 1559 MHz. Figure 4.4-1 is a block diagram showing the arrangement of the system elements for this measurement. The 1.2-meter parabolic reflector antenna was mounted on a TACO tripod which could be manually adjusted in elevation angle and azimuth to predetermined positions. The tripod was mounted on a metal stand so that the top of the tripod was 2.8 meters above the deck. The metal stand, tripod, and antenna are shown in Photo 4.4-1 as installed on the flying bridge deck, starboard side. A 12-meter, low-loss coaxial cable connected the antenna through a coaxial switch to the instrumentation located in the wheelhouse below the flying bridge. Photo 4.4-2 shows the instrumentation positioned on a shelf above the flag storage locker. The white container on the left is a styrofoam cup containing the cold reference load. The cup was kept filled with liquid nitrogen to establish a reference temperature of 77.35 degrees Kelvin ($^{\circ}\text{K}$). This was calibrated to be 80°K at the end of the 10-cm long transmission line which extended through the cup. The coaxial switch was used to alternately connect the antenna or the cold reference load to the L-band system and radiometer. An X-Y recorder was used as the readout for the radiometer. Each measurement was made by adjusting the variable attenuator in the cold reference load line so that the

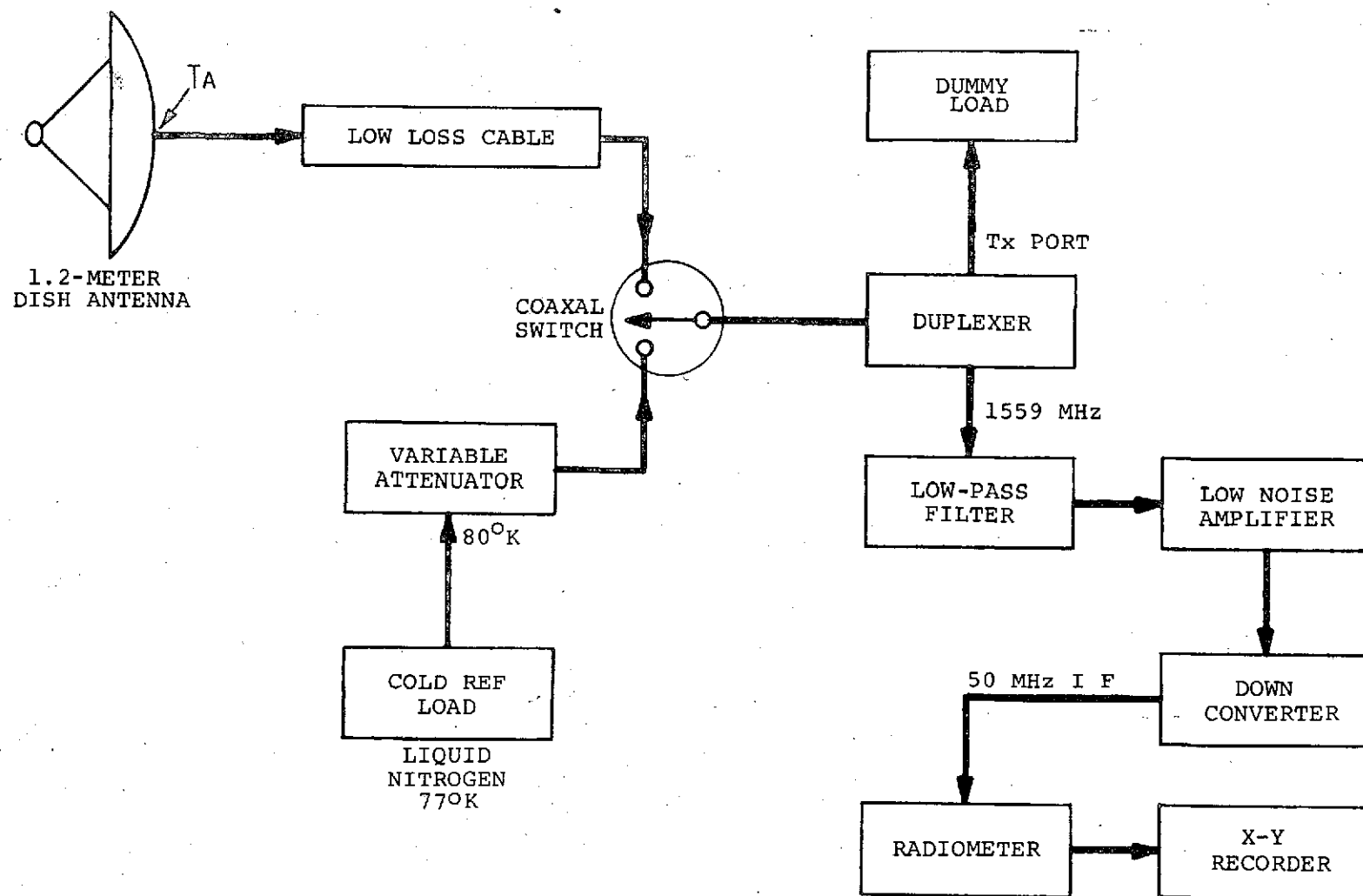


FIGURE 4.4-1
RADIOMETER INSTRUMENTATION FOR ANTENNA SKY-NOISE MEASUREMENT
AT 1559 MHz

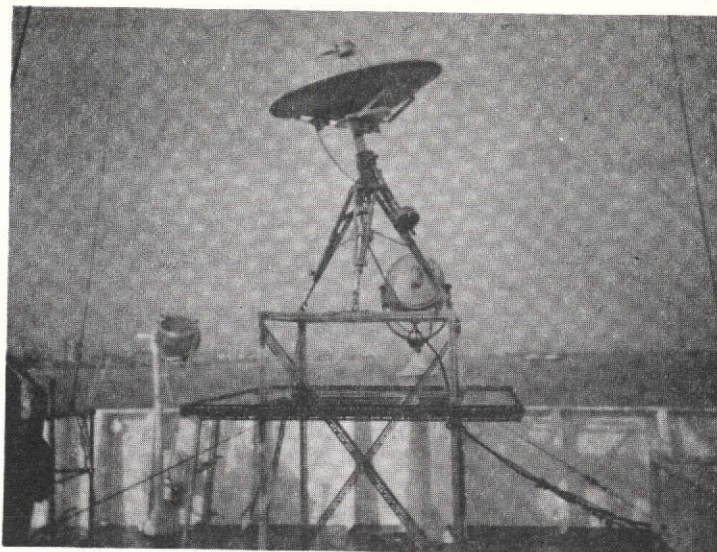


Photo 4.4-1, 1.2 Meter Diameter L-Band Dish Antenna Mounted on Tripod and Stand on Starboard Side of Flying Bridge



Photo 4.4-2, Instrumentation Setup in Wheelhouse for Antenna Sky-Noise Temperature Measurements

REPRODUCED
ORIGINAL PA

IE
R

X-Y recorder readout was unchanged as the coaxial switch was switched from the antenna to the cold reference load.

4.4.1 Location of Measurements

Two sets of measurements were made, one designated "in-harbor" and the other "at-sea". The in-harbor measurements were started on June 16th while the ship was in-harbor at Port Elizabeth and concluded on June 18th while the ship was at the Tioga Terminal in Philadelphia. The at-sea measurements were started on June 17th while the ship was off the coast of New Jersey bound for Philadelphia and concluded on June 19th while the ship was underway from Philadelphia to Savannah.

The tripod with its azimuth scale was mounted on the platform in such a manner that when the antenna was pointed directly forward on the ship the azimuth scale read 288° . All of the data was recorded using this azimuth bearing. Consequently, the data shown in Tables D-1 and D-2 is referenced to a 0° which is 72° off the starboard bow. In the plots of the data shown in Figs. 4.4-3 and 4.4-4 an adjustment has been made to locate the bow of the ship at 0° . This also applies to Fig. 4.4-5 showing the relative location of ship structures.

4.4.2 Reduction of Data

To reduce the data to units of noise temperature the variable attenuator was calibrated at 1559 MHz using a Hewlett-Packard model 614A signal generator and Hewlett-Packard model 431B power meter. This calibration was again confirmed using a Hewlett-Packard 8614A signal generator and a Hewlett-Packard 432A power meter. The 12-meter, low-loss coaxial cable was measured at 1559 MHz using a Hewlett-Packard model 8410S network analyzer.

ANGLE	ELEVATION ANGLE													
Az	0°	5°	10°	15°	20°	25°	30°	35°	40°	45°	55°	65°	75°	85°
0°	184	13	37	28	46	49	46	188	40	25	49			43
20°	139	10	37	28	52	46	46	55	28	34	43			
40°	151	16	37	28	79	61	58	37	43	31	37	37	43	
60°	148	34	34	28	142	139	97	37	46	31	46			
80°	103	13	34	28	124	139	100	31	37	31	43			
100°	130	4	37	37	85	85	58	43	64	37	37	34	37	43
120°	107	64	46	49	70	76	58	40	49	37	40			
140°	101	76	82	58	82	61	58	55	52	46	52			
160°	103	103	85	76	82	73	76	85	70	67	61	85	76	
180°	220	37	55	52	79	112	106	97	70	85	94			43
200°	103	61	37	37	46	127	40	43	37	55	94			
220°	184	64	46	37	34	118	31	52	40	55	82	122	52	
240°	184	64	64	42	58	37	52	262	211	397	52	133		
260°	178	49	49	52	46	37	43	214	37	31	76			
280°	178	46	49	46	40	43	49	52	37	31	58	43	43	43
300°	142	37	49	43	40	43	43	97	43	31	85			
320°	166	13	49	37	49	37	37	169	49	31	58			
340°	190	55	37	28	55	49	46	205	40	31	76	37	43	

TABLE D-1

IN-HARBOR ANTENNA SKY-NOISE TEMPERATURE MEASUREMENTS, T_A , IN DEGREES KELVIN, °K, AT 1559MHZ

ANGLE	ELEVATION ANGLE														
Az	0°	5°	10°	15°	20°	25°	30°	35°	40°	45°	55°	65°	75°	85°	
0°	115	70	37	46	31	31	28	25	25	25	25			37	
20°	151	76	34	43	37	31	31	28	25	28	31	31			
40°	136	76	49	46	37	34	31	31	25	28	31		34		
60°	139	76	52	55	34	31	34	31	31	31	31	22			
80°	130	67	37	49	34	31	31	31	31	31	31				
100°	88	61	37	22	37	34	31	25	25	31	31	34	34	34	
120°	61	43	34	37	34	19	34	31	25	31	31				
140°	49	58	61	61	25	46	43	40	37	31	31	43			
160°	76	64	58	67	31	46	58	49	58	49	49		49		
180°	76	58	37	58	67	76	73	70	58	58	64	85		46	
200°	88	43	22	46	49	43	37	34	31	37	67				
220°	76	43	13	46	43	37	34	28	31	37	67	97	157		
240°	85	43	25	43	28	34	31	25	17	31	67				
260°	70	46	34	43	25	31	25	25	25	25	28	34			
280°	73	49	25	43	34	31	25	25	25	28	25		34	43	
300°	85	58	31	43	31	25	25	25	28	25	25	43			
320°	100	58	31	46	28	28	25	25	19	25	25				
340°	115	67	31	46	37	31	31	28	25	31	25	31	34		

TABLE D-2

AT-SEA ANTENNA SKY-NOISE TEMPERATURE MEASUREMENTS, T_A , IN DEGREES KELVIN, °K, AT 1559MHZ

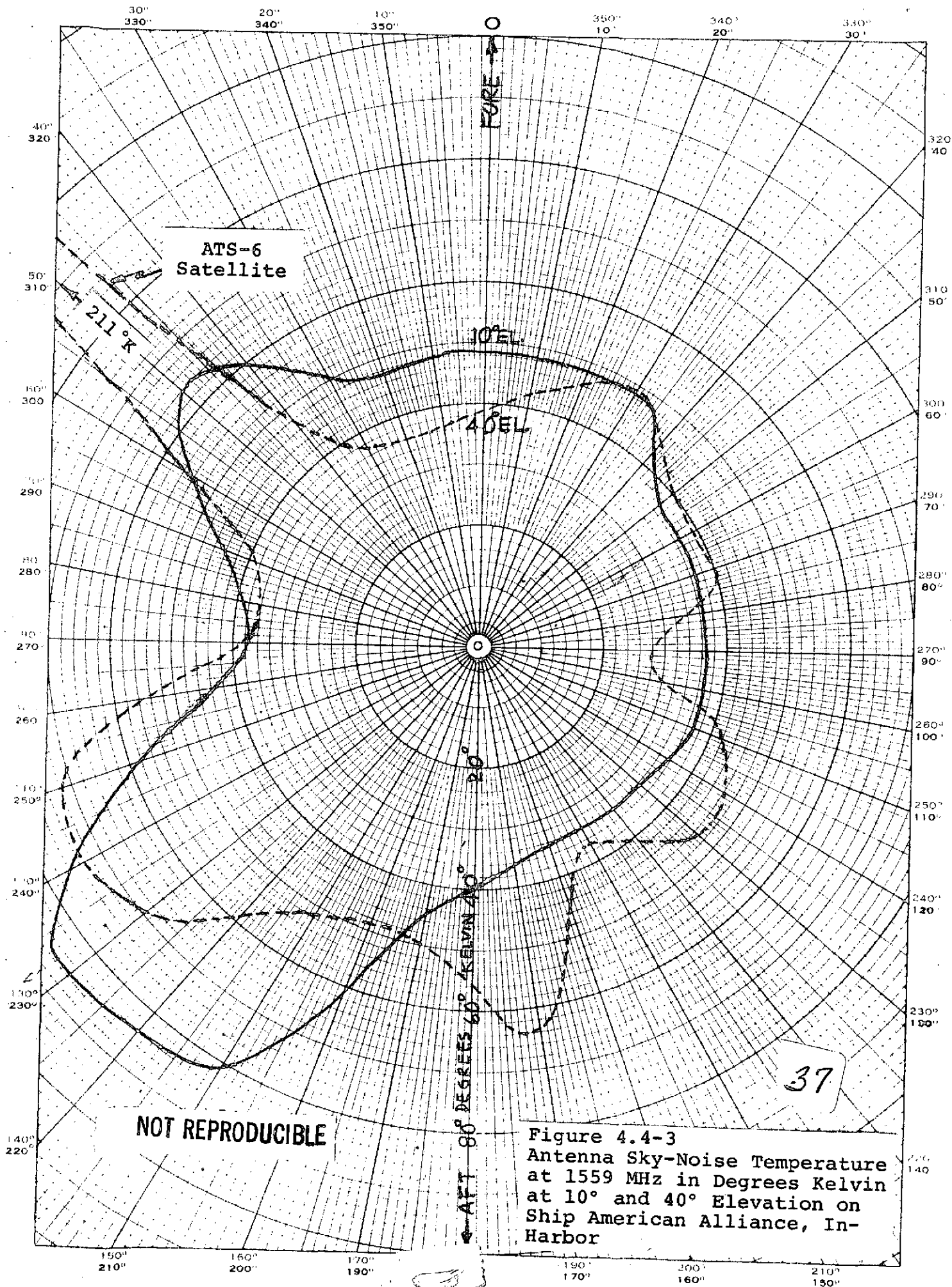


Figure 4.4-3
Antenna Sky-Noise Temperature
at 1559 MHz in Degrees Kelvin
at 10° and 40° Elevation on
Ship American Alliance, In-
Harbor

MADE IN U.S.A.
ELECTRONIC INDUSTRIES

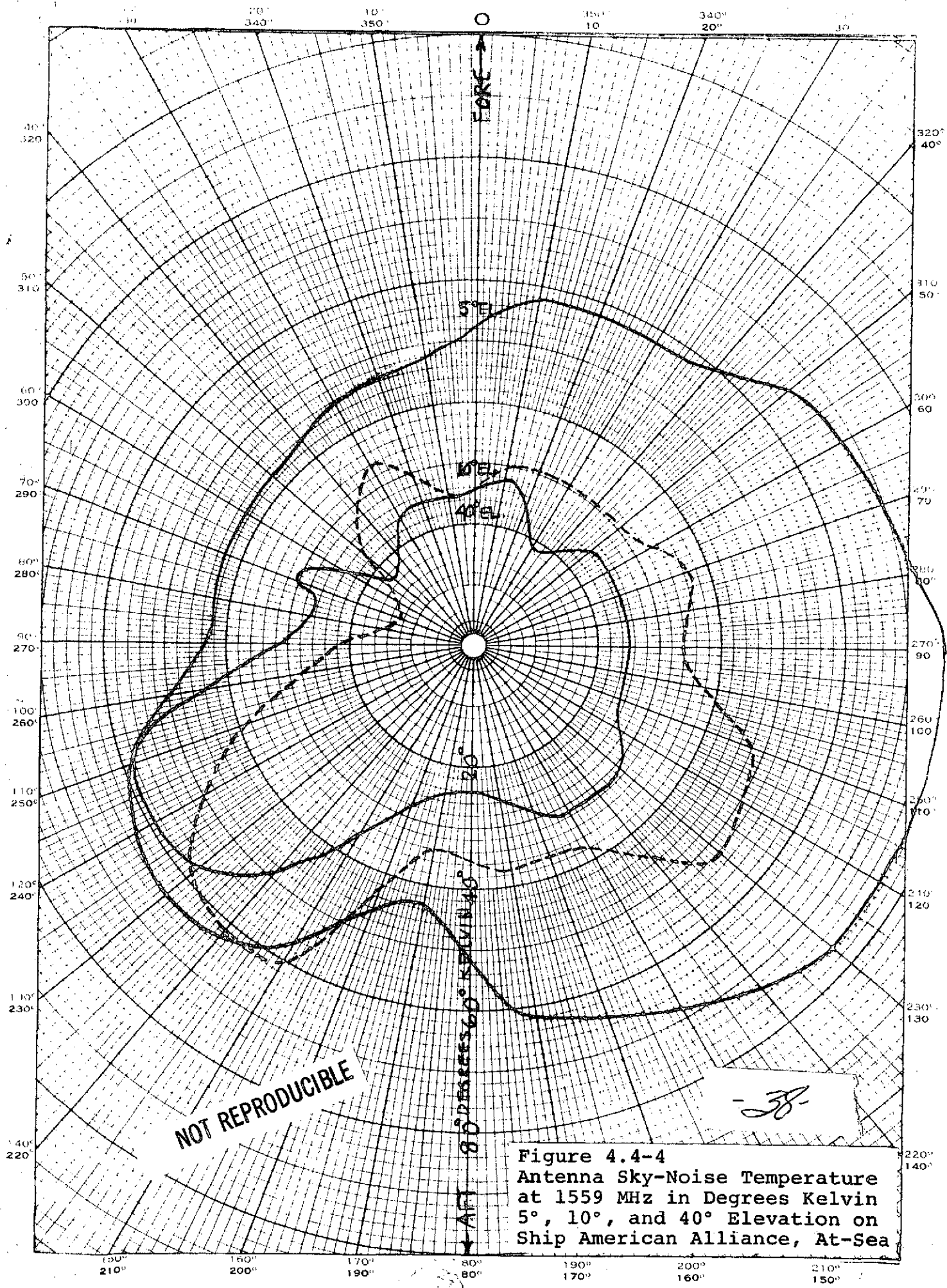
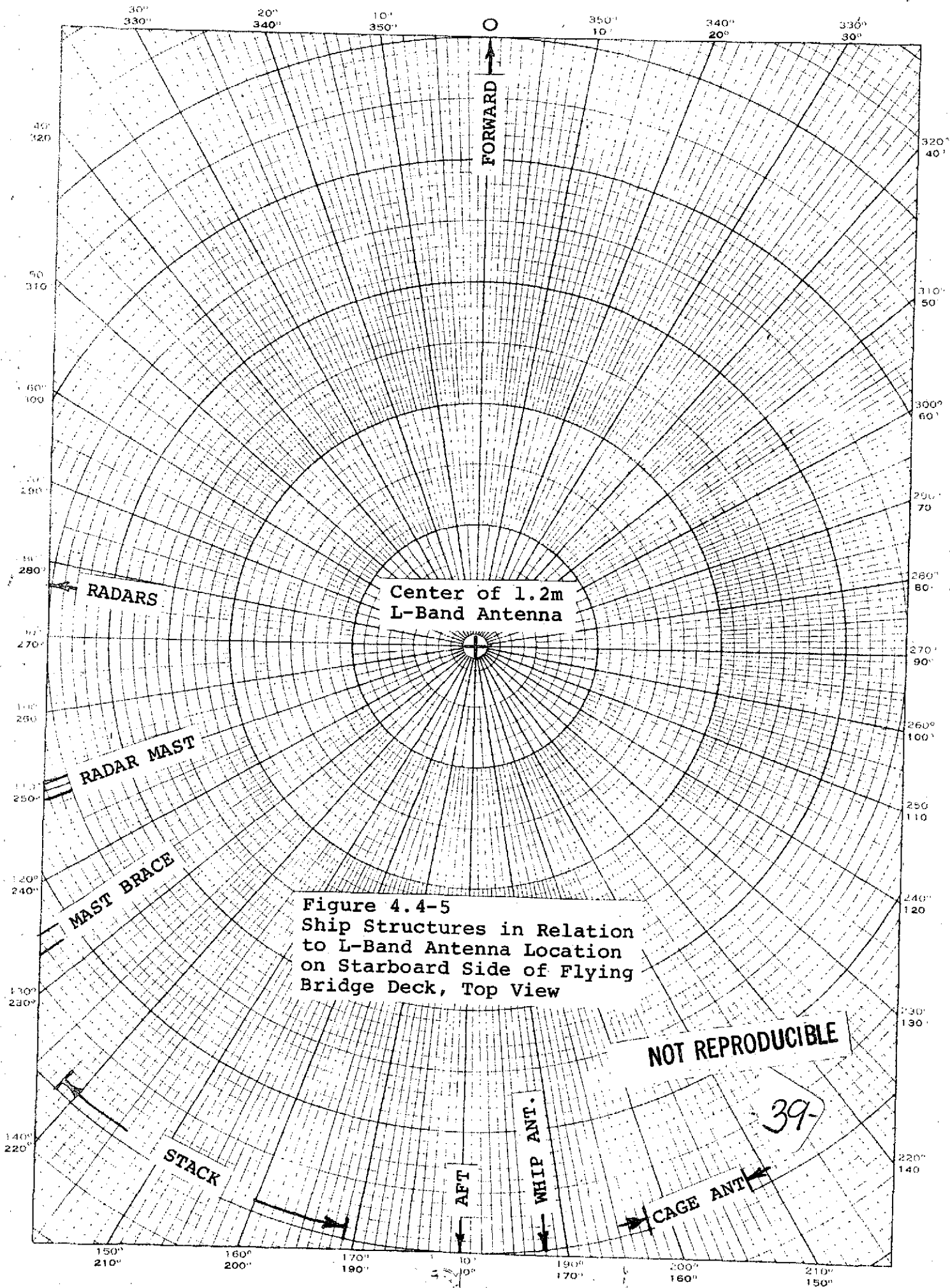


Figure 4.4-4
Antenna Sky-Noise Temperature
at 1559 MHz in Degrees Kelvin
5°, 10°, and 40° Elevation on
Ship American Alliance, At-Sea



The shorter cables were measured with the same instrumentation used to calibrate the variable attenuator. Cable and attenuator loss was converted to temperature difference using the equations:

$$T_A = T_\alpha + 80 - 154$$

$$T_A = T_\alpha - 74$$

$$\text{where, } T_\alpha = (10^{\alpha/10} - 1) 300$$

where: T_α = noise temperature representing loss of attenuator and associated coaxial cable, °K

α = attenuation in decibels

T_A = antenna sky-noise temperature at 1.2 m dish antenna output terminals

154 = noise temperature representing loss in coaxial line to antenna, °K

300 = ambient temperature, °K

80 = cold load reference temperature, °K

Example:

where attenuator dial reads 22.5, attenuation is 0.9 dB (from the calibration curve, Fig. 4.4-2). The two short coaxial cables in the attenuator circuit add 0.7 dB for a total of 1.6 dB = α in the cold reference load circuit.

$$T_\alpha = (10^{\alpha/10} - 1) 300$$

$$= (10^{1.6} - 1) 300$$

$$= (1.445 - 1) 300$$

$$= (0.445) 300$$

$$= 133.5$$

$$T_A = 133.5 - 74$$

$$= 59.5^\circ\text{K}$$

4.4.3 Comments

While making the measurements on June 18th at the Tioga Terminal at Philadelphia it was noticed that the readings over Camden were much higher than over the surrounding area. It was suggested that the L-band 1.2 m dish antenna might be looking at the NASA ATS-5 or ATS-6 Applications Technology Satellites (ATS). Consequently, a check was made of the daily operations plan and it was found that ATS-6 was operating at L-band from 1000 to 1330 EDST. ATS-6 is positioned at 94° West Longitude within one degree of the equator. This would indicate a compass bearing of 208° East of North at the Tioga Terminal and this is in agreement with the observed bearing of approximately 209°. The calculated elevation angle was 40° and this is also in agreement with the high noise-temperature readings which were recorded at 35°, 40° and 45° elevation angle, referenced to the deck of the ship (Table D-1).

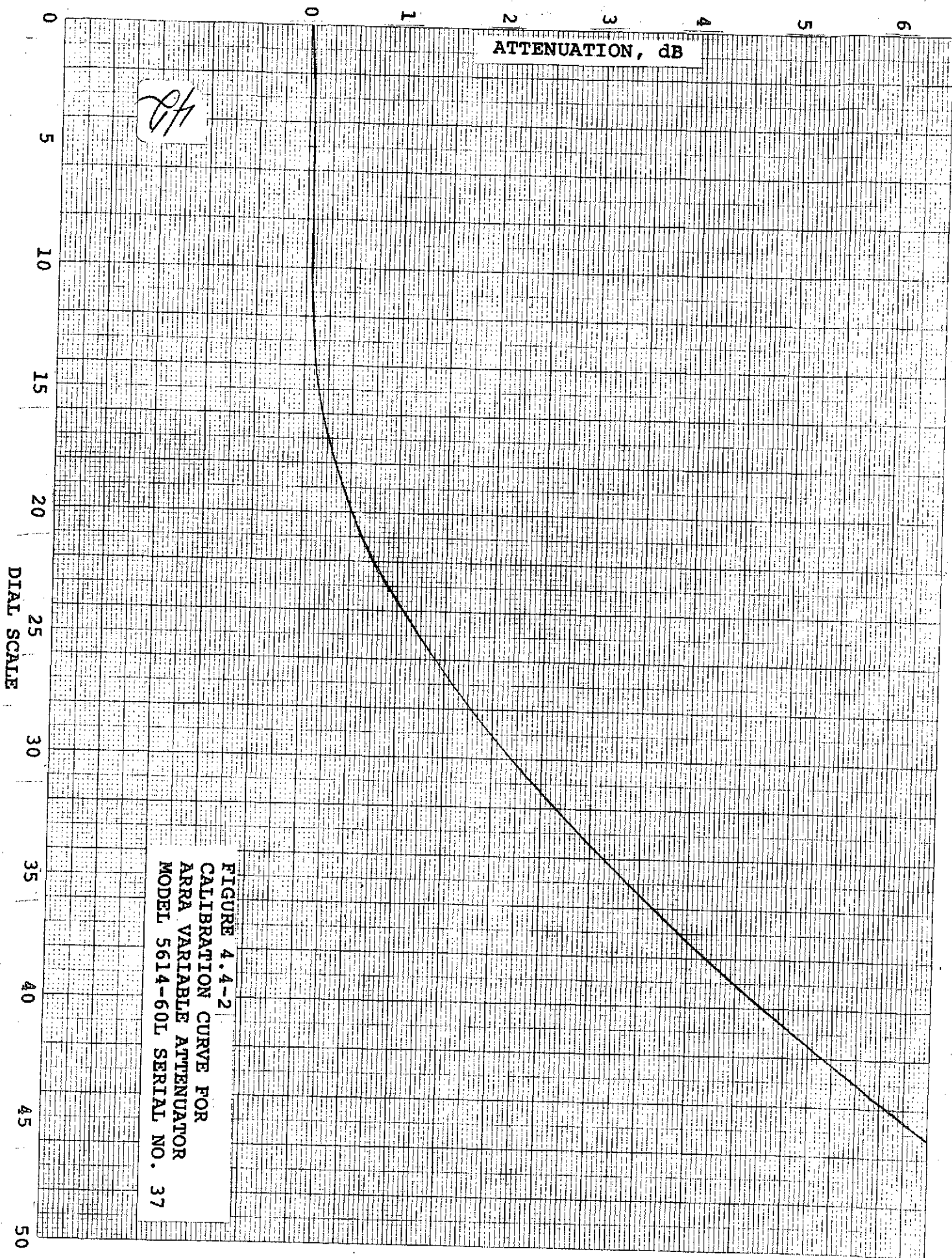
The measurement error of antenna noise-temperature will be influenced by factors such as (a) calibration error for the attenuator, (b) the error in reading the vernier scale on the attenuator and (c) the measurement error for cable loss of the coaxial cables interconnecting the antenna and the coaxial switch, the cold reference load and the variable attenuator, and the variable attenuator and the coaxial switch. For example:

$$\text{let } T_A = 50^\circ\text{K}$$

$$\text{then } T_\alpha = 50 + 74 = 124$$

$$\text{so } 1 + (124/300) = \text{anti log } \alpha/10$$

$$\text{and } \alpha = 1.5 \text{ dB}$$



Thus, the total attenuation between the cold load reference point and the coaxial switch is 1.5 dB. Part of this is attenuator loss and part is coaxial cable loss. Typically the cable loss is 0.6 dB leaving an attenuator loss of 0.9 dB. If the error in cable loss measurement is 0.1 dB the attenuation is $1.5 \text{ dB} \pm 0.1 \text{ dB}$. However, cable loss measurements should be accurate to within 0.1 dB.

$$\text{Let } \alpha = 1.5 - 0.1 = 1.4 \text{ dB}$$

$$T_{\alpha} = (10^{.14} - 1) 300$$

$$T_{\alpha} = (1.380 - 1) 300$$

$$T_{\alpha} = 114$$

$$T_A = T_{\alpha} - 74$$

$$T_A = 40^{\circ}\text{K}$$

Compare this with 50°K for 1.5 dB attenuation. Thus, an error of 0.1 dB in cable loss results in a change of 10°K in antenna noise-temperature at 50°K . An error in reading the variable attenuator by one division of the vernier scale represents approximately 0.0175 dB at 25 on the dial (less at lower dial readings).

$$\text{Let } \alpha = 1.5 - 0.0175 = 1.4825 \text{ dB}$$

$$T_{\alpha} = (10^{.14825} - 1) 300$$

$$T_{\alpha} = (1.407 - 1) 300$$

$$T_{\alpha} = 122.1$$

$$T_A = T_{\alpha} - 74$$

$$T_A = 48.1^{\circ}\text{K}$$

Compare this with 50°K for 1.5 dB attenuation. Thus, an error in reading the attenuator of 0.1 division will result in an error of 1.9°K . The root-sum-square of these combined errors

is 10.2°. It is estimated that the overall accuracy of the antenna-noise temperature measurements are at least this good, or better.

The results of the measurements have been tabulated in Table D-1 for the in-harbor measurements and Table D-2 for the at-sea measurements. The measurements were influenced by ships structures such as the stack as well as by shore-based structures while the ship was in the harbor. Plots were made of the measurements at certain elevation angles both in-harbor and at-sea as shown in Figures 4.4-3 and 4.4-4. Figure 4.4-5 shows the relative position of certain structures on the ship in reference to the L-band terminal antenna position on the starboard side of the flying bridge deck.

4.5 Interference to Radar

The test of L-band interference to the radars was planned as a part of this survey. The radars were turned on and made operational while the L-band dish antenna was directed toward the radars and the radar display observed for evidence of interference. An AIL model 124 power oscillator was used as a substitute for the L-band transmitter. The L-band antenna had been set up on its tripod and stand on the starboard side of the flying bridge. This put the L-band antenna at a line-of-sight distance of approximately 7.4 meters from the X-band radar antenna and approximately 9.2 meters from the S-band radar antenna. Photo 4.5-1 shows these antennas.

4.5.1 Conduct of Test

The test was conducted while the ship was in the harbor at Port Elizabeth, New Jersey. Photo 4.5-2 shows a section of the wheelhouse with the two radar display and control units and a service cabinet between them. The S-band radar is on the left

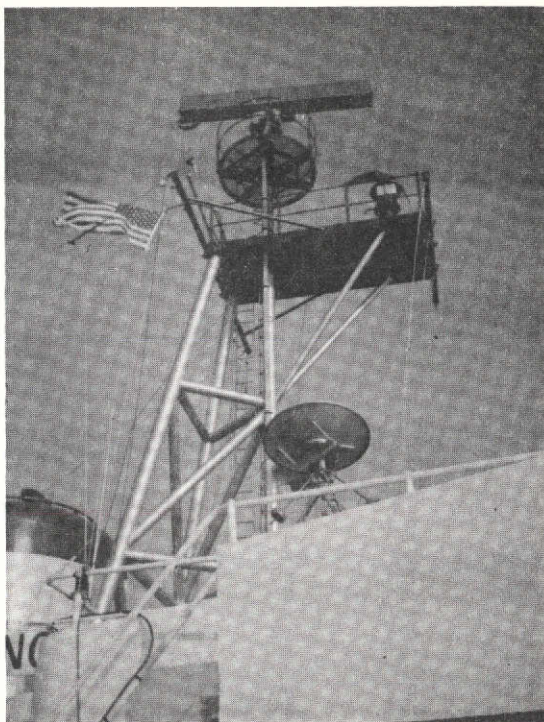


Photo 4.5-1, Radar Platform with
S-Band and X-Band
Radar Antennas.
L-Band 1.2 Meter
Dish Antenna Below
on Flying Bridge

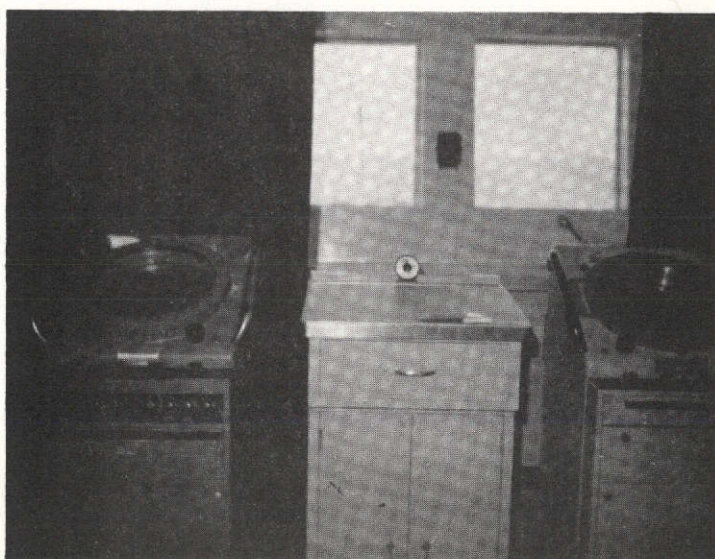


Photo 4.5-2, Radar Display
Units in Wheelhouse

and the X-band radar on the right. The transmitter, receiver, and power supply for each radar is located in the storage room on the deck directly below the wheelhouse. A camera mounting bracket was installed in the ceiling directly above each radar so that a Polaroid camera could be used to photograph each display. Photos 4.5-3 and 4.5-4 show the radar displays before the L-band terminal was energized.

The L-band terminal was set up in another section of the wheelhouse and connected to the 1.2 meter L-band dish antenna on the flying bridge with a 12-meter-length of low-loss coaxial cable. An AIL power oscillator was connected to the transmitter port of the duplexer and tuned to 1659 MHz, the L-band up-link frequency. With the power oscillator adjusted to full output of 15 watts and the L-band antenna directed toward the radar antennas, a photograph was made of each radar display. There was no evidence of interference on either display as shown in Photos 4.5-5 and 4.5-6. To verify that the L-band signal was being radiated, the log-spiral conical antenna was set up on the flying bridge and connected to the H-P Spectrum Analyzer to sample the radiated signal.

4.5.2 Comments

In this test neither radar was equipped with waveguide filters which are available to control interference effects. The S-band radar was operating in the 1-nautical-mile range which selects a pulse duration of 0.1 microseconds and a pulse repetition rate of 2000. Average power output is 6 watts and the receiver bandwidth is 12 MHz. The X-band radar was also operating in the 1-nautical-mile range. The pulse duration is 0.25 microseconds



Photo 4.5-3, S-Band Radar Display with
L-Band Transmitter Off,
Port Elizabeth

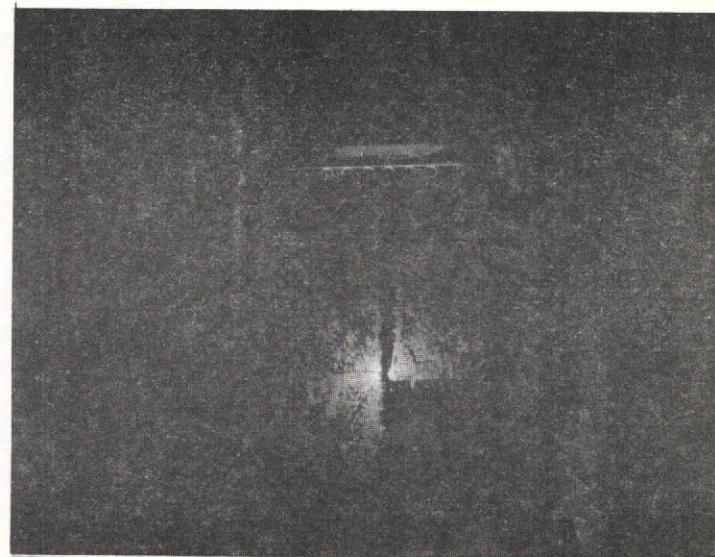


Photo 4.5-4, X-Band Radar Display with
L-Band Transmitter Off,
Port Elizabeth

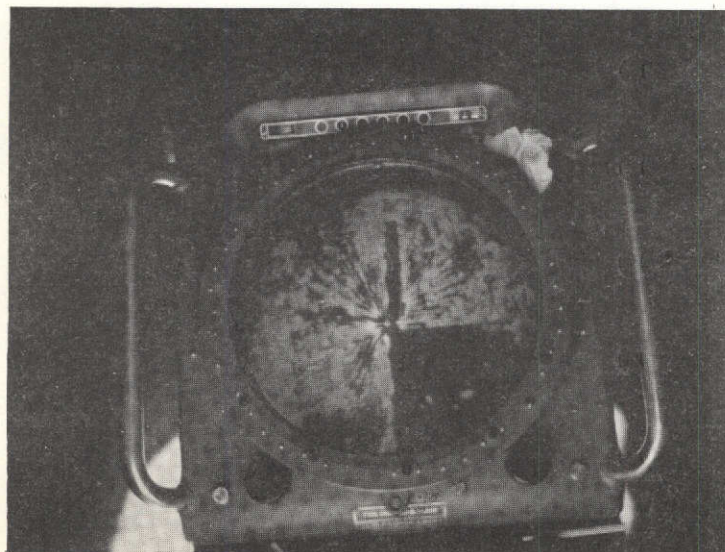


Photo 4.5-5, S-Band Radar Display with
L-Band Transmitter On,
Port Elizabeth

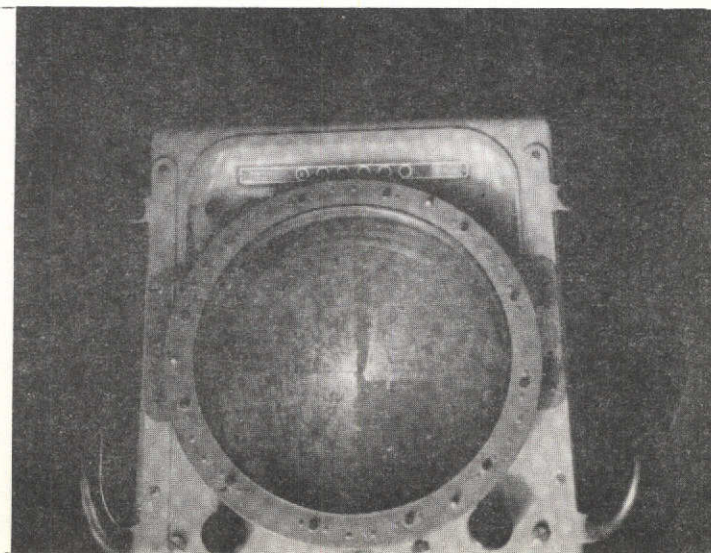


Photo 4.5-6, X-Band Radar Display with
L-Band Transmitter On,
Port Elizabeth

with a pulse repetition rate of 2000. The average power is 20 watts and the receiver bandwidth is 2.5 MHz. If the S-band radar were operated in the 6, 16, or 40-nautical-mile range, the average power would be increased to 12 watts and the receiver bandwidth reduced to 3 MHz. Each of these changes are in the direction of reducing potential interference and since the second harmonic of the L-band transmitter (3318 MHz) is sufficiently removed from the operating frequency of the S-band radar (3050 MHz), the possibility of interference is remote.

The X-band radar characteristics also change when it is operated in the 8, 20, or 40-nautical mile range. While the average power remains at 20 watts, the receiver bandwidth is increased to 8 MHz. This increase in bandwidth should not be significant in view of the frequency separation between the X-band radar operating frequency (9375 MHz) and the L-band terminal (1659 MHz), or even the sixth harmonic of the L-band terminal (9954 MHz).

5. Analysis of Results

5.1 Conducted Emissions

The conducted emissions measured on the ship's power lines at the terminals of the radar sets were in almost all cases higher than that measured on the commercial power lines in the RCA calibration laboratory. The comparison was made on an octave-by-octave basis over the frequency range of 150 kHz to 32 MHz. Narrowband and broadband emissions were on the order of 50 dB higher on the lower bands and about 15 dB higher on the upper bands. The broadband measurements on each shipboard power line exceeded the limits specified in MIL-STD-461A.

An examination of the charts shows many sharp peaks in the broadband measurements. Many of these were transients occurring on a time basis. Others were steady in the frequency spectrum. Some represented broadcast station signals in the broadcast band, 540 to 1600 kHz, and even foreign broadcast stations as noted on the charts.

The spectrum display pictures centered at 70 MHz show that the noise level at this frequency is 36 dB/ μ A/MHz which is well below the MIL-STD-461A limit extrapolated to 70 MHz. The level of conducted emissions existing on the power lines indicates that any sensitive equipment connected to the power lines should include a power line filter. The insertion loss of the filter would be determined by the sensitivity of the equipment.

5.2 Field Intensity

Measurements of field intensity one meter from the radar transmitter cabinets in the storage room showed that the cabinet radiation in the maritime L-band was not excessive and was reasonable when compared with MIL-STD-461A, Electromagnetic Interference Characteristics, Requirements for Equipment, which is a generally recognized standard for this type of equipment. While the limits of the standard do not exceed 1000 MHz for broadband interference, they can be extrapolated up to the X-band radar frequency range. This extrapolation would put the case radiation in S-band and X-band about 5 dB above the limit in each case. Equipment built to meet MIL-STD-461A requirements would withstand a radiated field intensity of 1 volt/meter which would be adequate protection under the circumstances.

Field intensity measurements at the above deck locations showed levels in the maritime L-band that were equivalent to or less than the levels measured in the storage room. The field intensity measurements in the S-band and X-band were, as expected, severe enough to require special attention to shielding requirements for equipment that might be installed in these locations, particularly on the radar platform where levels were greater than 10 v/m/MHz. On the flying bridge deck level the field intensity was 2 v/m/MHz.

5.3 Filter Evaluation

Measurements made at five different interfaces in the L-band shipboard terminal system indicated that additional low-pass filtering would not be required to prevent interference from the radars as installed on the "American Alliance". The combined

filtering action of the duplexer, the LNA, and the installed filters so completely suppressed the radar signals that the addition of low-pass filters produced no discernable change at the output of the duplexer or any other interface downstream from this point.

Radar interference to the L-band shipboard terminal will be influenced by the relative location of the antennas. On the "American Alliance", the antenna separation from the L-band antenna to the S-band antenna was 9.2 meters and to the X-band antenna, 7.4 meters. Closer spacing might justify the requirement for an additional low-pass filter.

5.4 Antenna Sky-Noise Temperature

The in-harbor measurements were made in Port Elizabeth (0°, 5°, 10° and 15° elevation) and Tioga Terminal, Philadelphia (20°, to 90° elevation). In Port Elizabeth the ship was berthed on its port side while at Tioga Terminal it was berthed on its starboard side. This is significant in that the loading crane and other dockside structures which affect the antenna noise temperature change sides of the ship as the elevation angle changes from 15° to 20°.

While the measurements were being made at the Tioga Terminal, several very high readings were recorded at the 240° azimuth, the highest being at 45° elevation. It was later determined that the antenna was looking at the ATS-6 satellite.

Both in-harbor and at-sea the 0° elevation measurements were considerably higher than the 5° elevation measurements at the same azimuth direction. This was anticipated because of ship structure and noise sources on the horizon especially in-harbor.

At-sea the measurements on the starboard side are much higher than on the port side at 0° elevation. This is accounted for by the fact that the ship was proceeding south, and shore based noise sources were off the starboard side of the ship.

5.5 Interference to Radars

The test for L-band shipboard terminal interference to the S-band and X-band radars as installed on the "American Alliance" showed that this should not be a problem with 15 watts power from the L-band transmitter. Without a higher power source being available, it was not possible to determine at what power interference would exist. It is also conceivable that a lesser separation between antennas and a more nearly beam-to-beam aspect could produce an interference situation.

APPENDIX A, CONDUCTED EMISSIONS

Chart A-1 to A-15, X-Band Radar, Black Line
Chart A-16 to A-30, X-Band Radar, White Line
Chart A-31 to A-41, S-Band Radar, T2 Terminal
Chart A-42 to A-52, RCAS Laboratory, Black Line
Chart A-53, Current Probe Calibration
Spectrum Display A-1, S-Band Radar, T₂ Terminal
Spectrum Display A-2, X-Band Radar, Black Line
Spectrum Display A-3, S-Band Radar, T₂ Terminal
Spectrum Display A-4, X-Band Radar, Black Line

COMMENTS ON THE USE OF THESE CHARTS AND SPECTRUM DISPLAYS

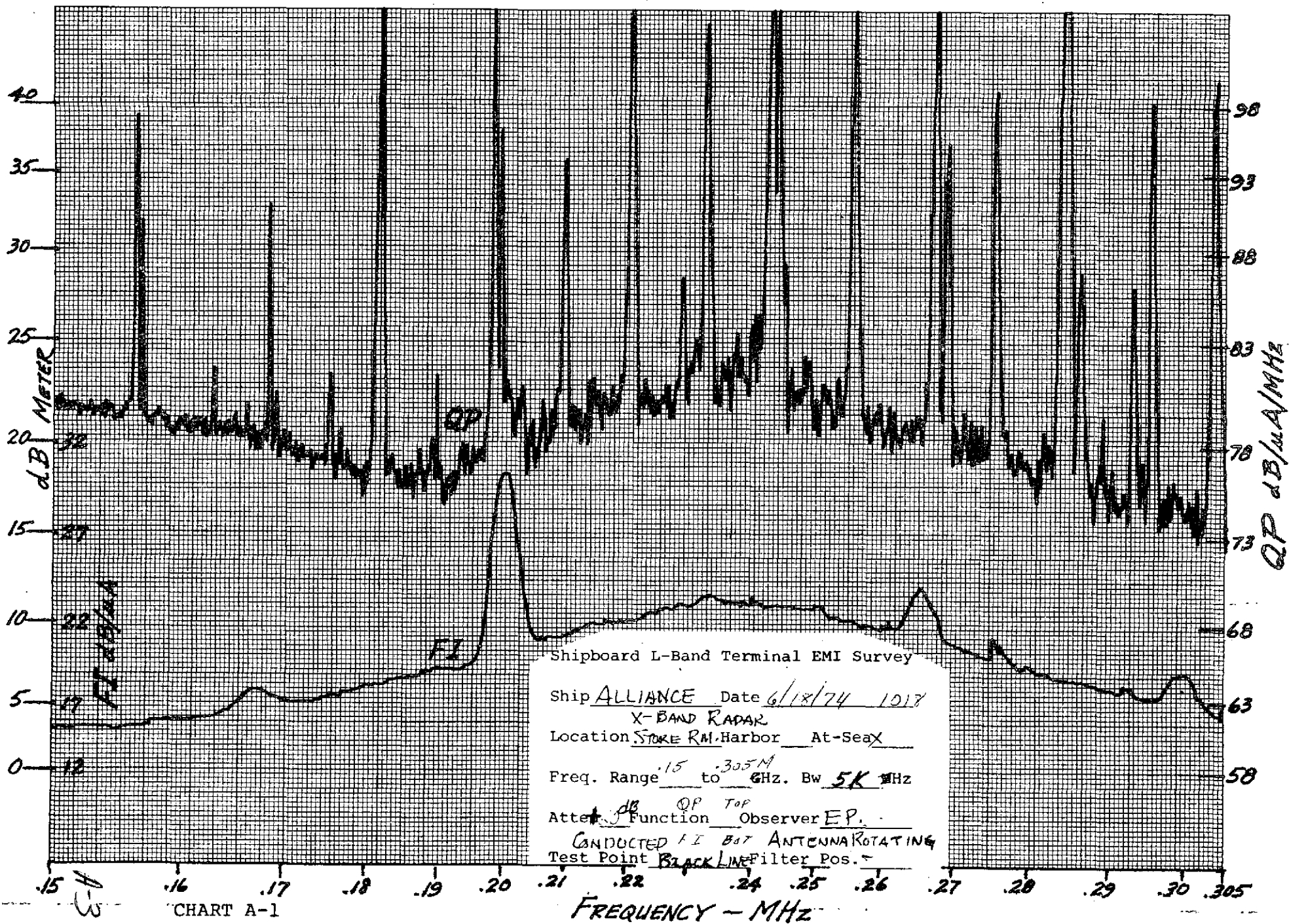
Charts A-1 through A-52 bear vertical scales for signal amplitude. The scale in the left hand margin is calibrated in dB from the meter scale of the measuring instrument (Stoddart NM-25T). The scale just inside the left margin (on the grid) is calibrated in dB/ μ A to read narrowband signals using the F1 (Field Intensity) trace on the chart. The calibration of this scale includes adjustments for the attenuator loss and current probe transfer impedance. The scale in the right hand margin is calibrated in dB/ μ A/MHz to read broadband signals using the QP (Quasi Peak) trace on the chart. This calibration includes adjustments for the attenuator loss, current probe transfer impedance and instrument bandwidth. Attenuator loss is noted on the label on each chart. The current probe transfer impedance factor is taken from Chart A-53. The value for each frequency range is shown on the chart. It should be noted

that while the transfer impedance values are positive they have been subtracted from signal amplitude in dB/ μ V to convert to dB/ μ A. The bandwidth of the Stoddart NM-25T is 5 kHz. To convert the broadband readings to dB/ μ A/MHz a factor of $20 \log \frac{BW2}{BW1}$ has been added, where BW1 is the instrument bandwidth (5 kHz) and BW2 is the normalized bandwidth (1 MHz). This factor, $20 \log \frac{1 \text{ MHz}}{5 \text{ kHz}}$ is 46 dB.

Spectrum Displays A-1 through A-4 show signal levels in dBm as measured by the spectrum analyzer with the current probe. To convert these values to dB/ μ A it is necessary to use a transfer impedance value for the particular frequency of interest by reference to the current probe calibration, Chart A-53. At the same time the spectrum analyzer power level in dBm must be converted to voltage level in dB/ μ V by adding 107 dB. For example from Spectrum Display A-2 at 52 MHz the level is -82 dBm.

From spectrum analyzer	- 82 dBm
convert to μ V	<u>+107 dB</u>
	+ 25 dB/ μ V
transfer impedance	<u>(-)+ 15 dB/ohm</u>
	+ 10 dB/ μ A

Thus 10 dB/ μ A is the peak value of the current in the X-band radar black power line at 52 MHz as measured with the spectrum analyzer with a bandwidth of 100 kHz. To normalize this to 1 MHz it is necessary to add 20 dB which is $20 \log$ of the bandwidth ratio. This gives a value of 30 dB/ μ A/MHz.



Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 1056

X-BAND RADAR

Location STONE RM Harbor At-Sea X

Freq. Range .29 to .59 ^MHz. Bw 5K MHz

Atten 0 ^{dB} Function FI Observer EP

Test Point CONDUCTED
BLACK LINE Filter Pos. -

Note SECURED ROTATION OF ANTENNA

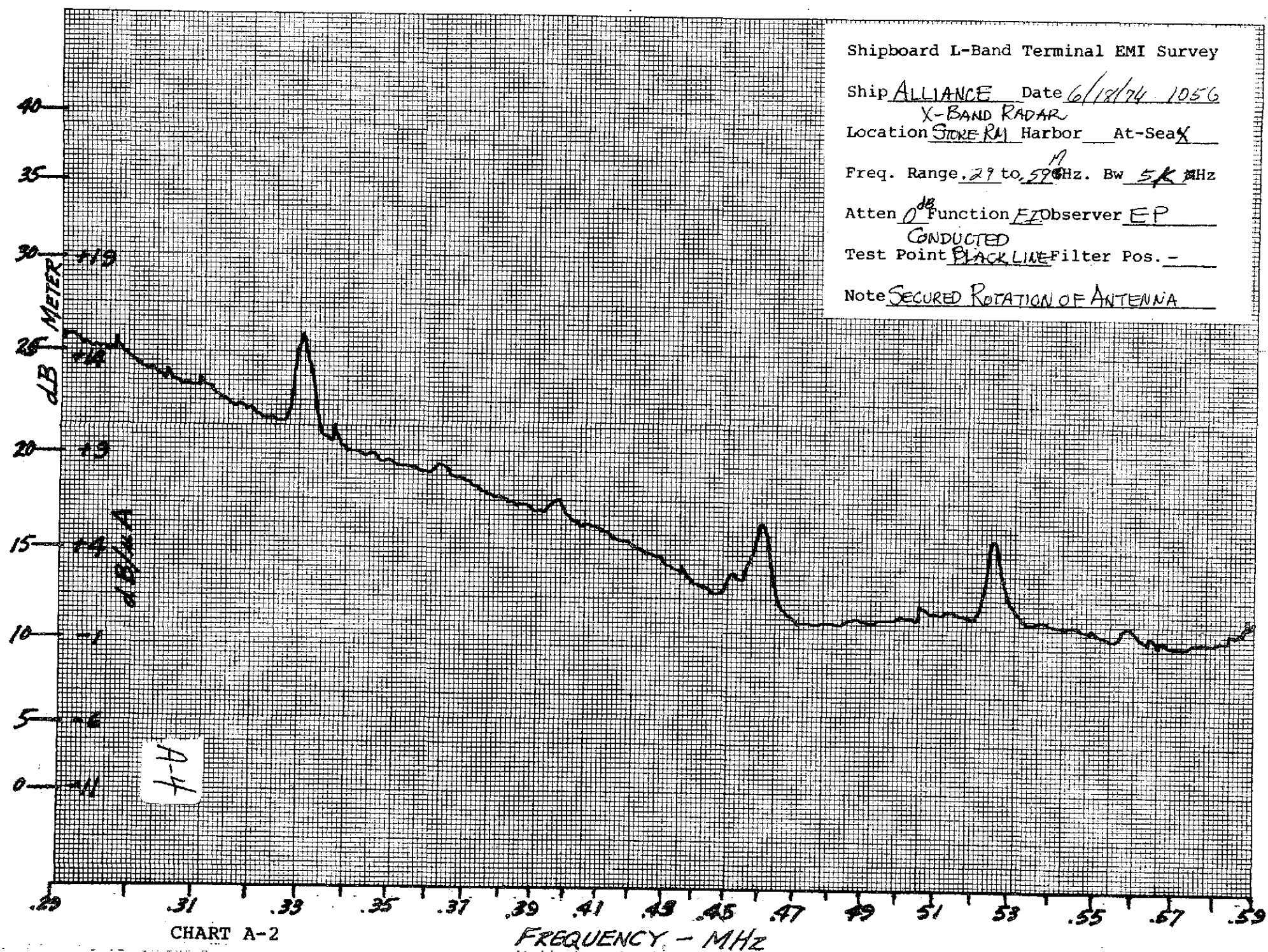
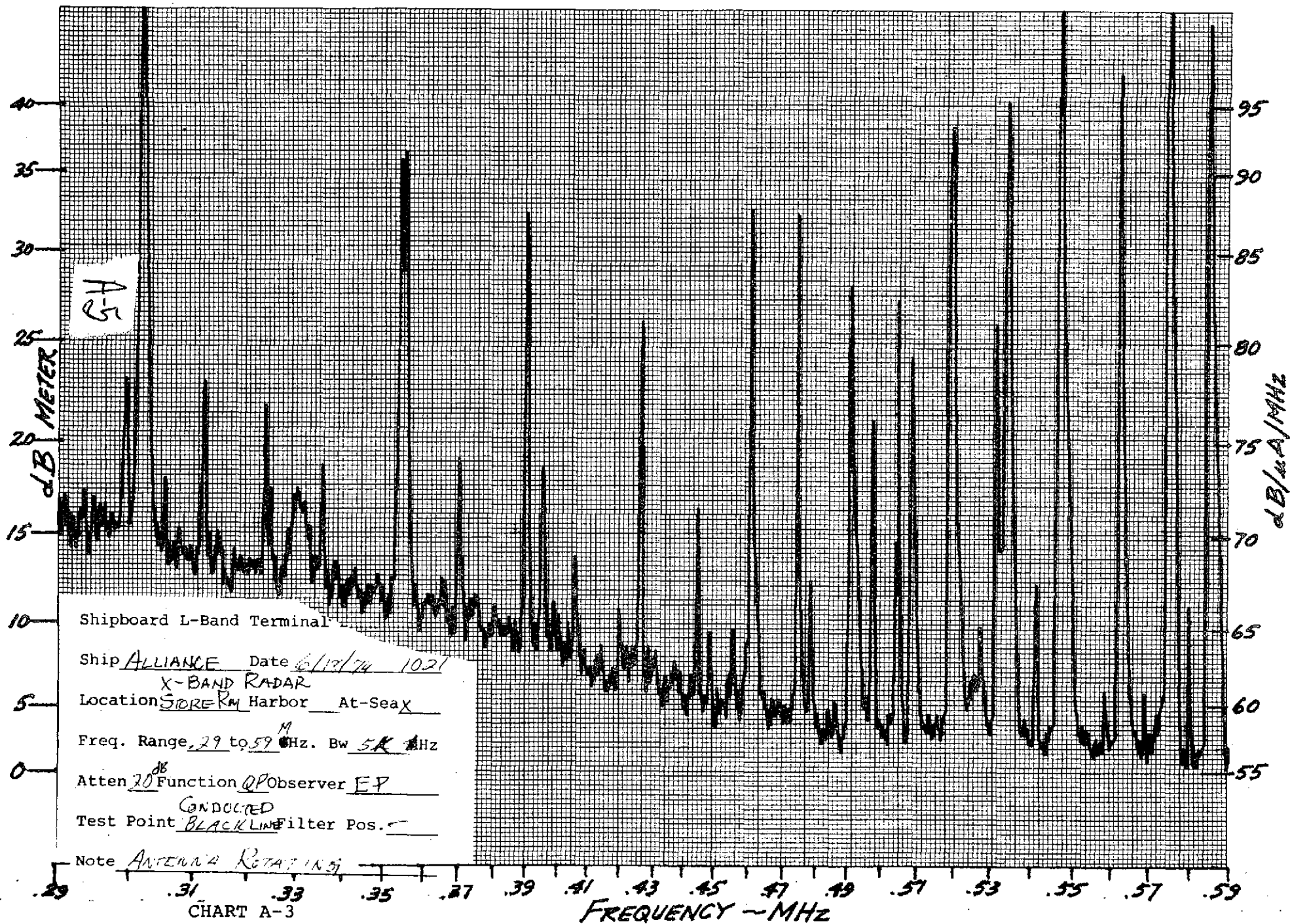


CHART A-2

FREQUENCY - MHz



Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 1/17/79 1980

X-BAND RADAR

Location ST. PETERSBURG Harbor At-Sea

Freq. Range .27 to .57 GHz. Bw 20 MHz

Atten AB Function 2 Observer EP

Test Point CONDUCTED Filter Pos. ANTENNA

Note SECURED ROTATION OF X-BAND

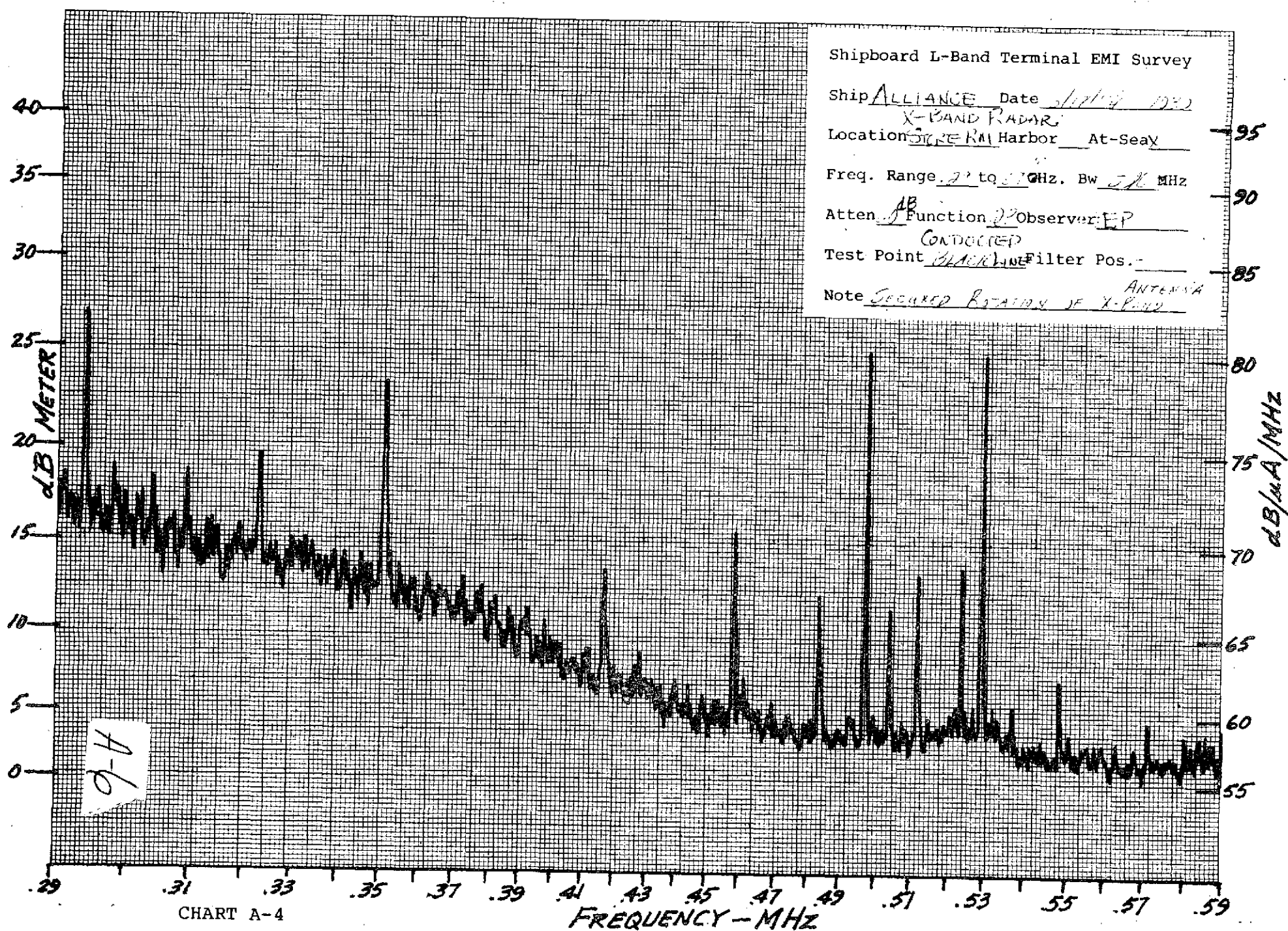
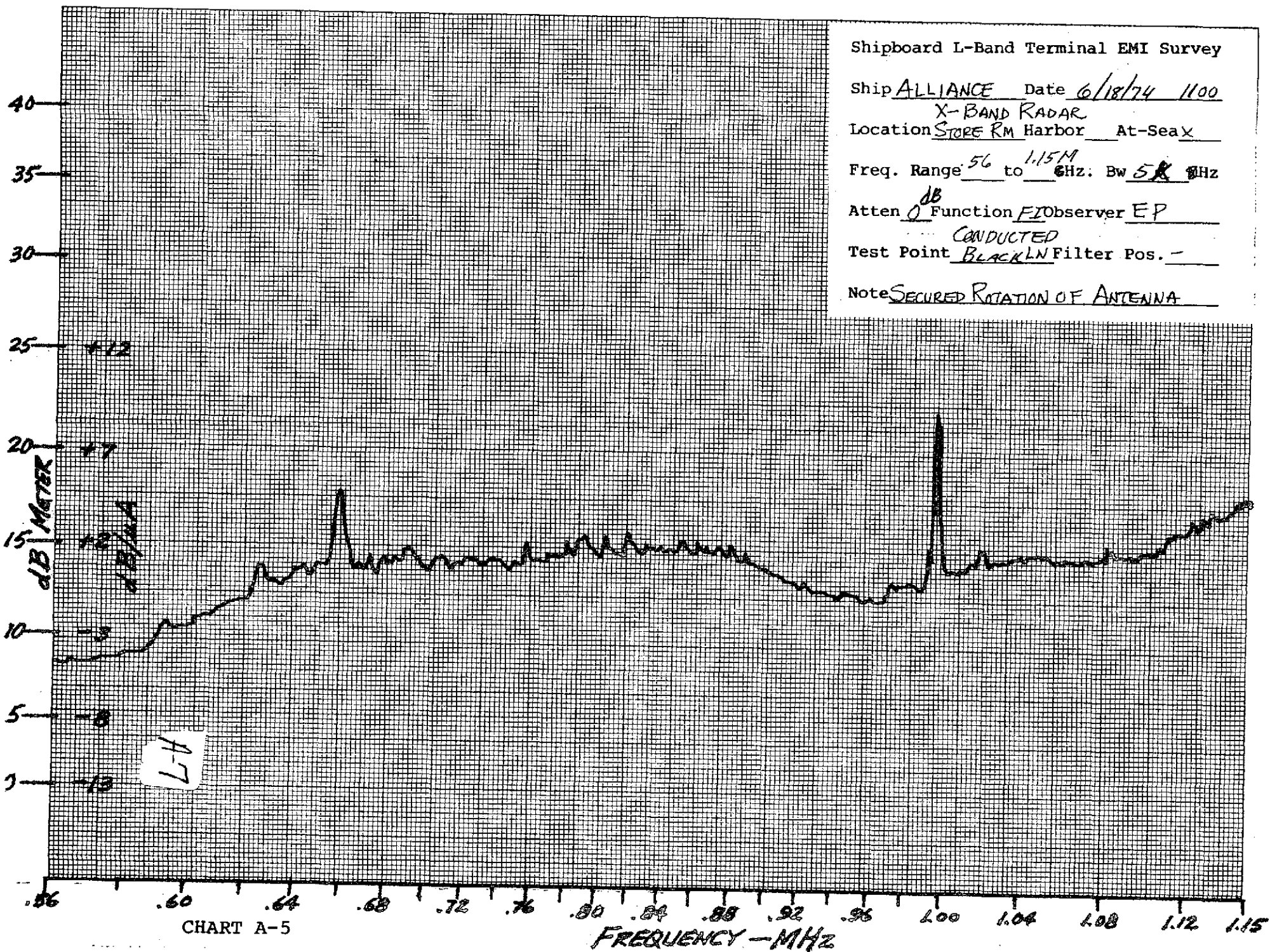


CHART A-4

Note SECURED ROTATION OF ANTENNA



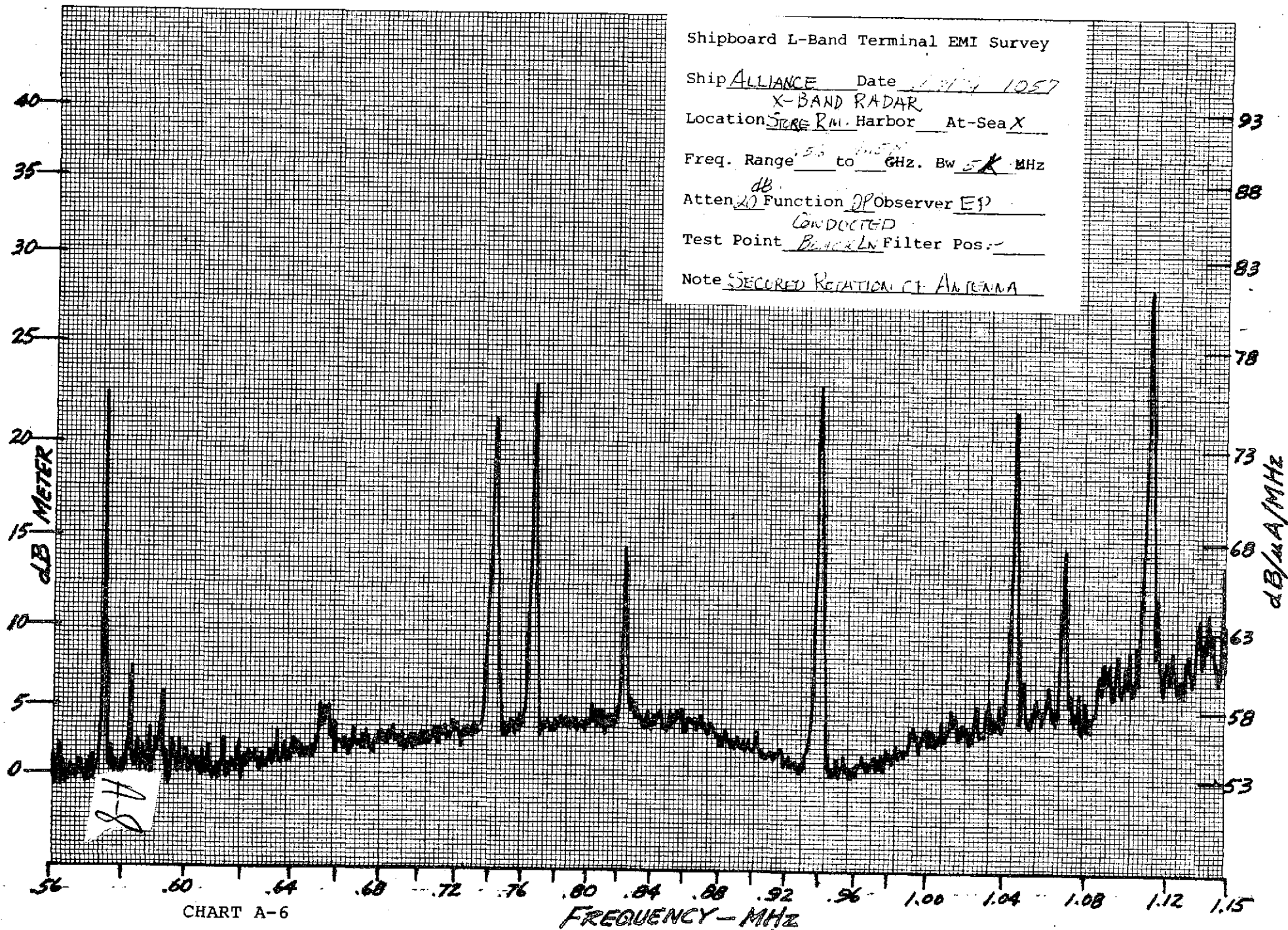
Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 1/17/57

X-BAND RADAR

Location STRE Rm. Harbor At-Sea XFreq. Range .56 to 1.15 GHz. Bw 5K MHzAtten 20 ^{dB} Function DP Observer EP

CONDUCTED

Test Point BLACK LN Filter Pos. -Note SECURED ROTATION OF ANTENNA

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 1104

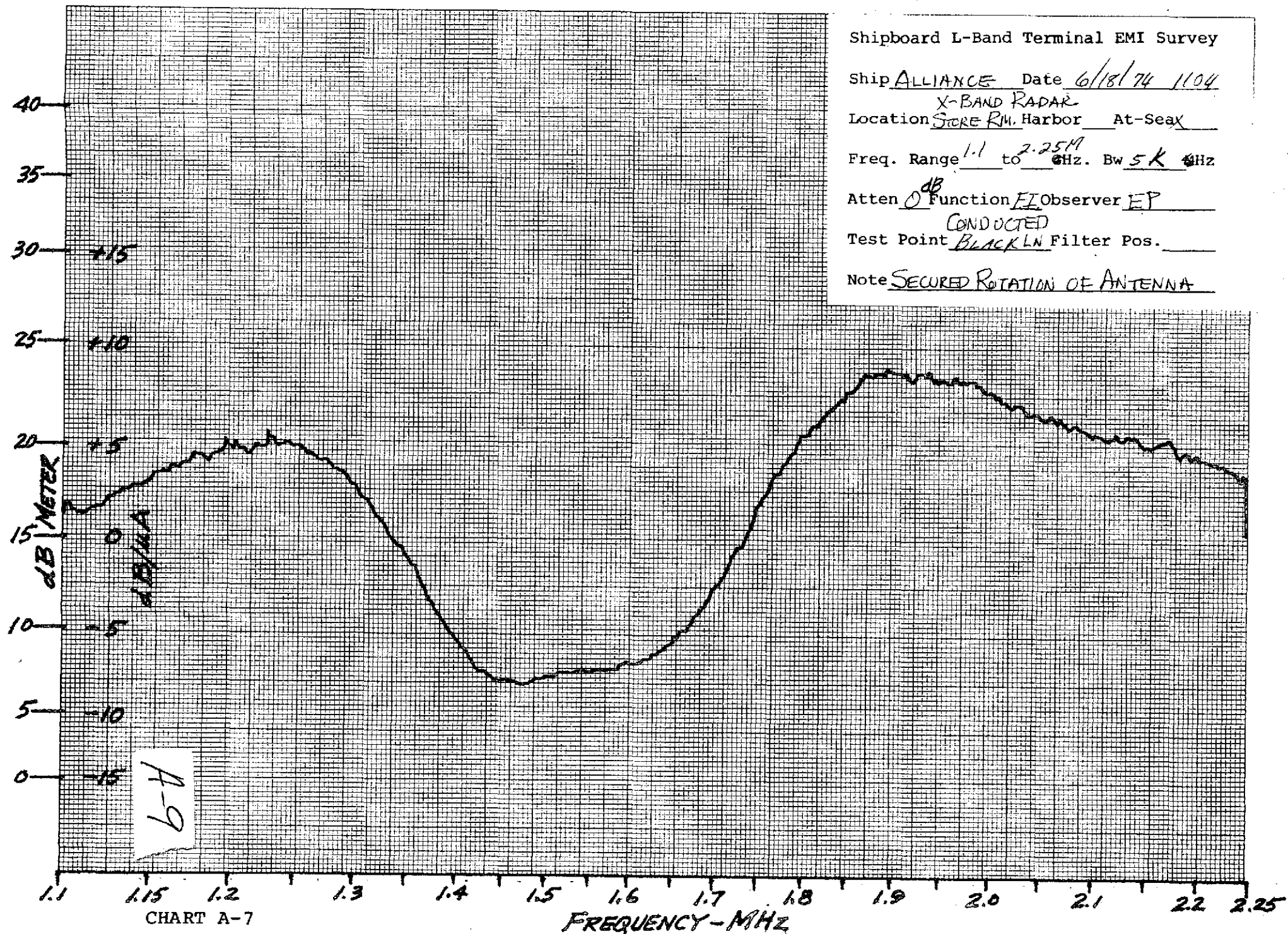
X-BAND RADAR
Location STORE RM. Harbor At-Sea

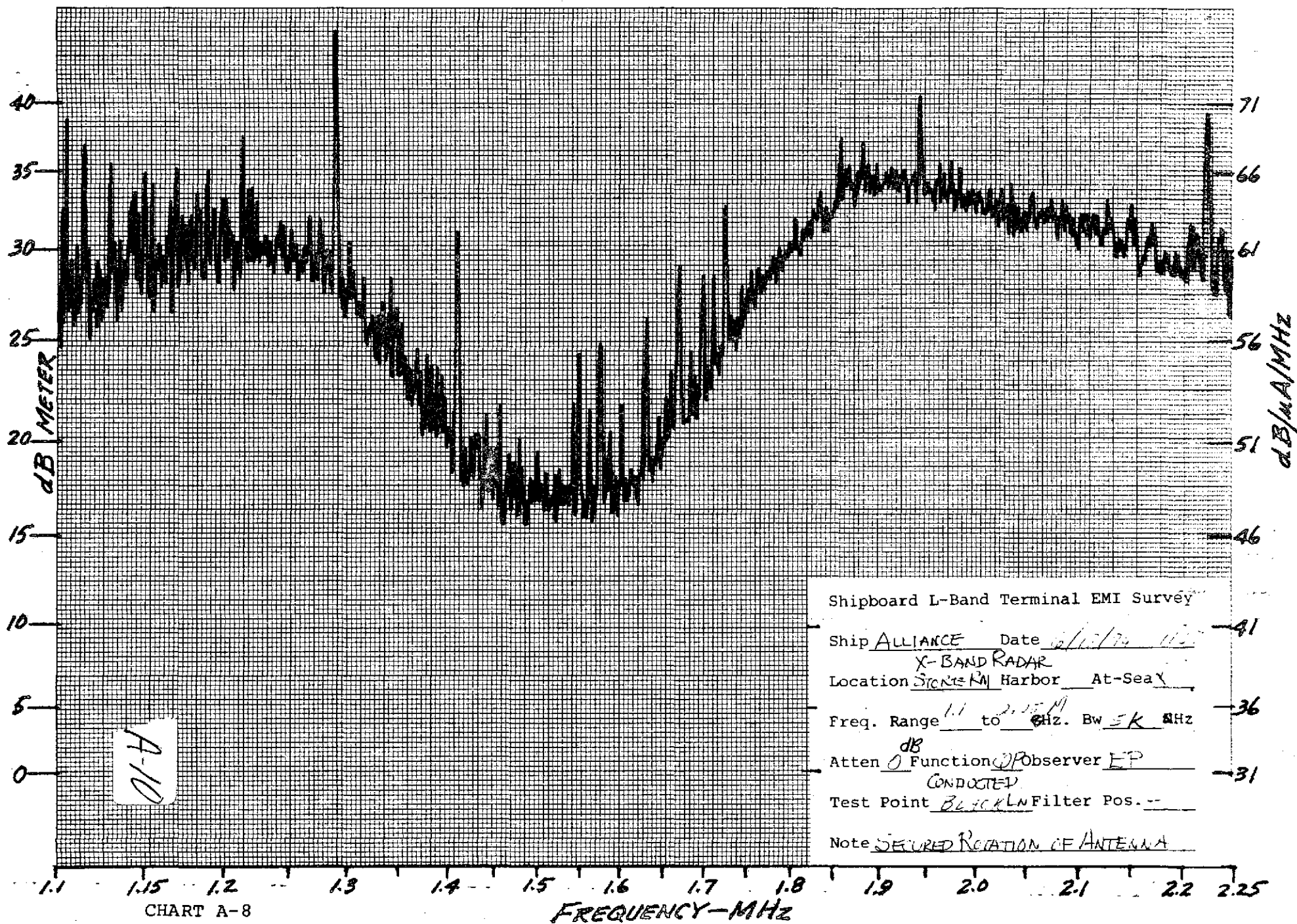
Freq. Range 1.1 to 2.25 MHz. Bw 5K Hz

Atten 0 dB Function FI Observer EP

Test Point CONDUCTED
BLACK LN Filter Pos.

Note SECURED ROTATION OF ANTENNA





Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 1111

X-BAND RADAR

Location STOR RM Harbor At-Sea X

Freq. Range 2.1 to 4.3 GHz. Bw 5K MHz

Atten 0 dB Function FI Observer EP

CONDUCTED

Test Point BLACK LN Filter Pos.

Note SECURED ROTATION OF ANTENNA

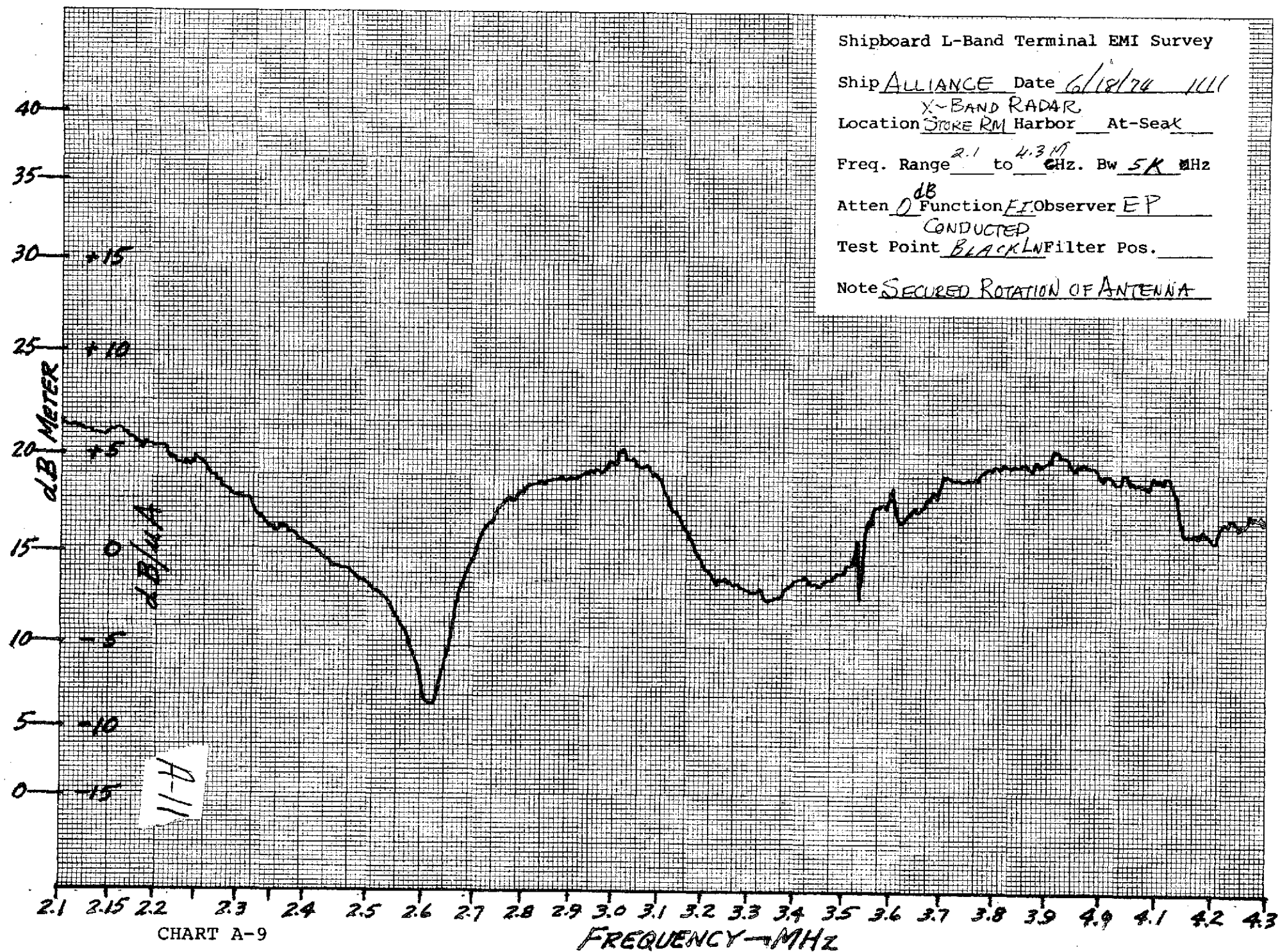
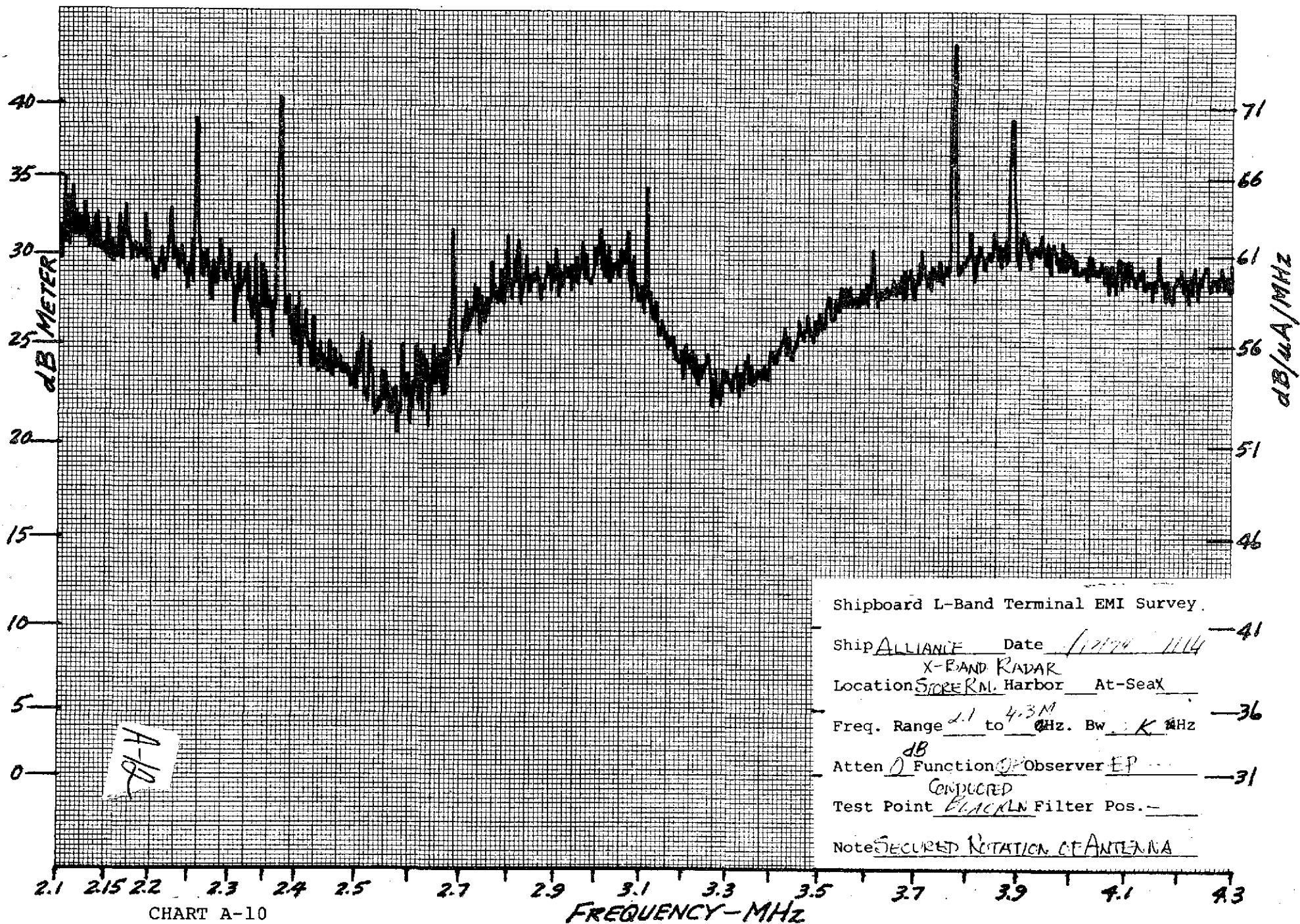
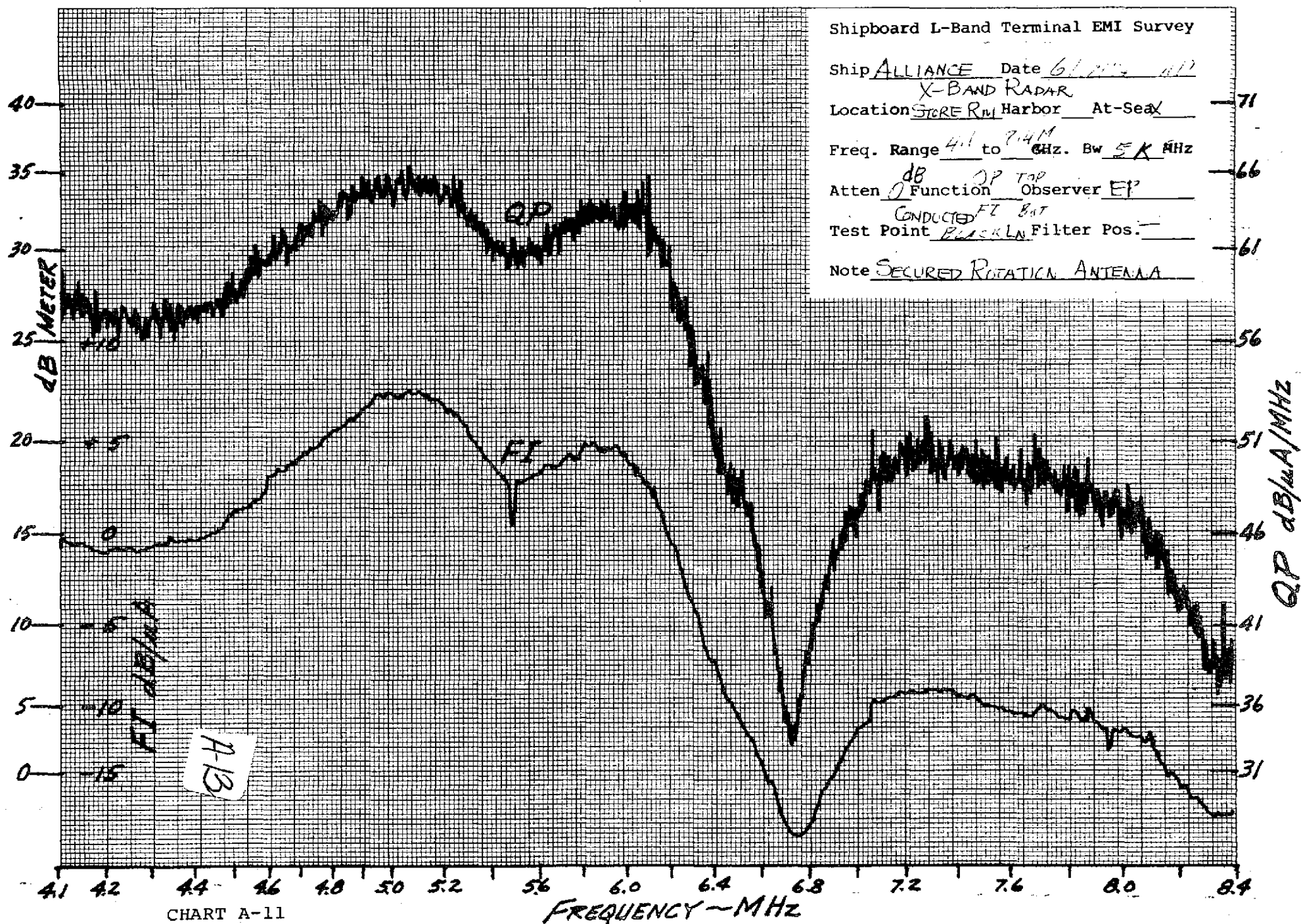


CHART A-9





Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1123

X-BAND RADAR

Location STORER Harbor At-Sea X

Freq. Range 8 to 16.5M Hz. Bw 5K MHz

Atten -20dB Function FI Observer EP

Test Point CONDUCTED BLACK LN Filter Pos. -

Note SECURED ROTATION ANTENNA

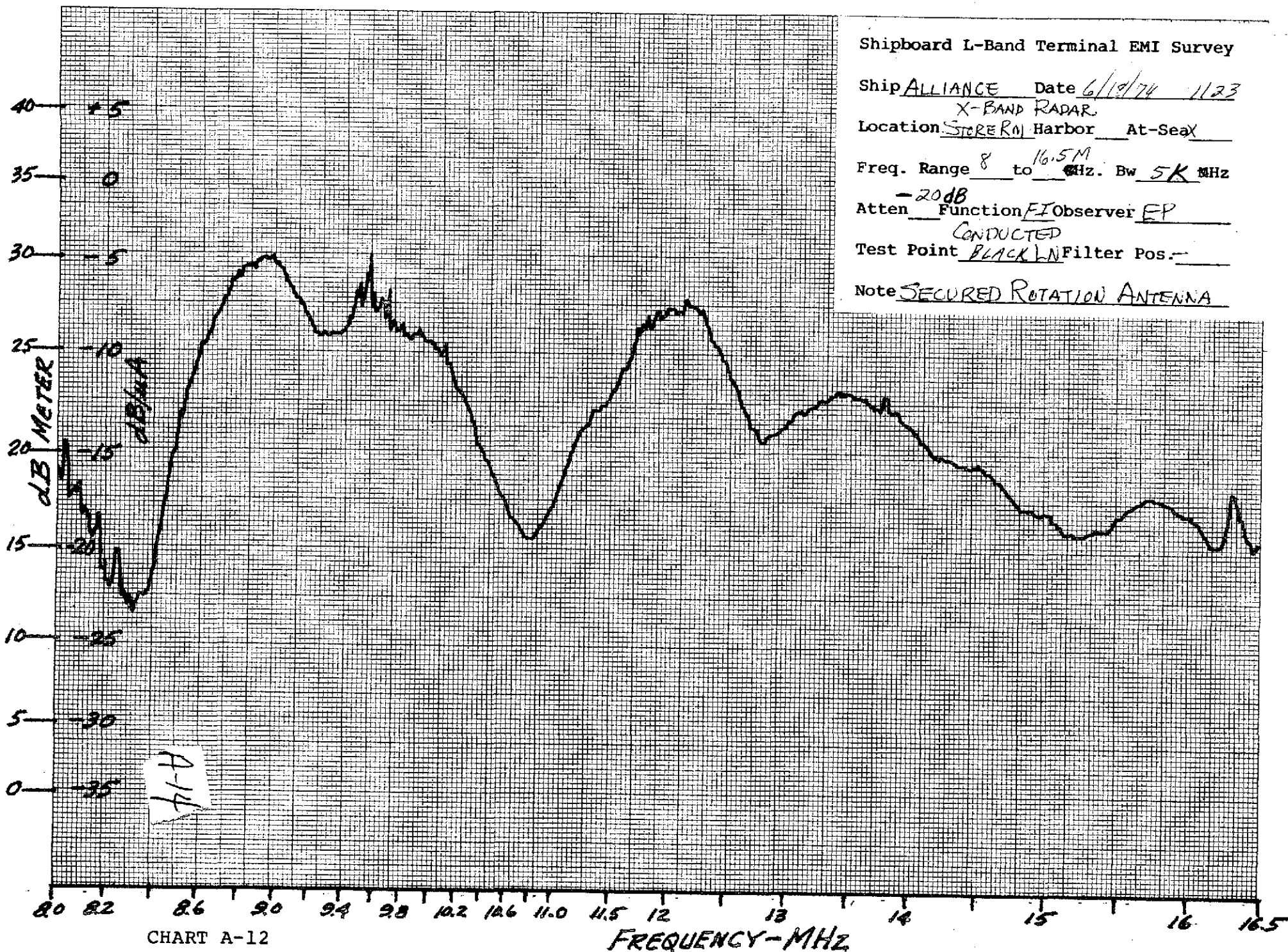
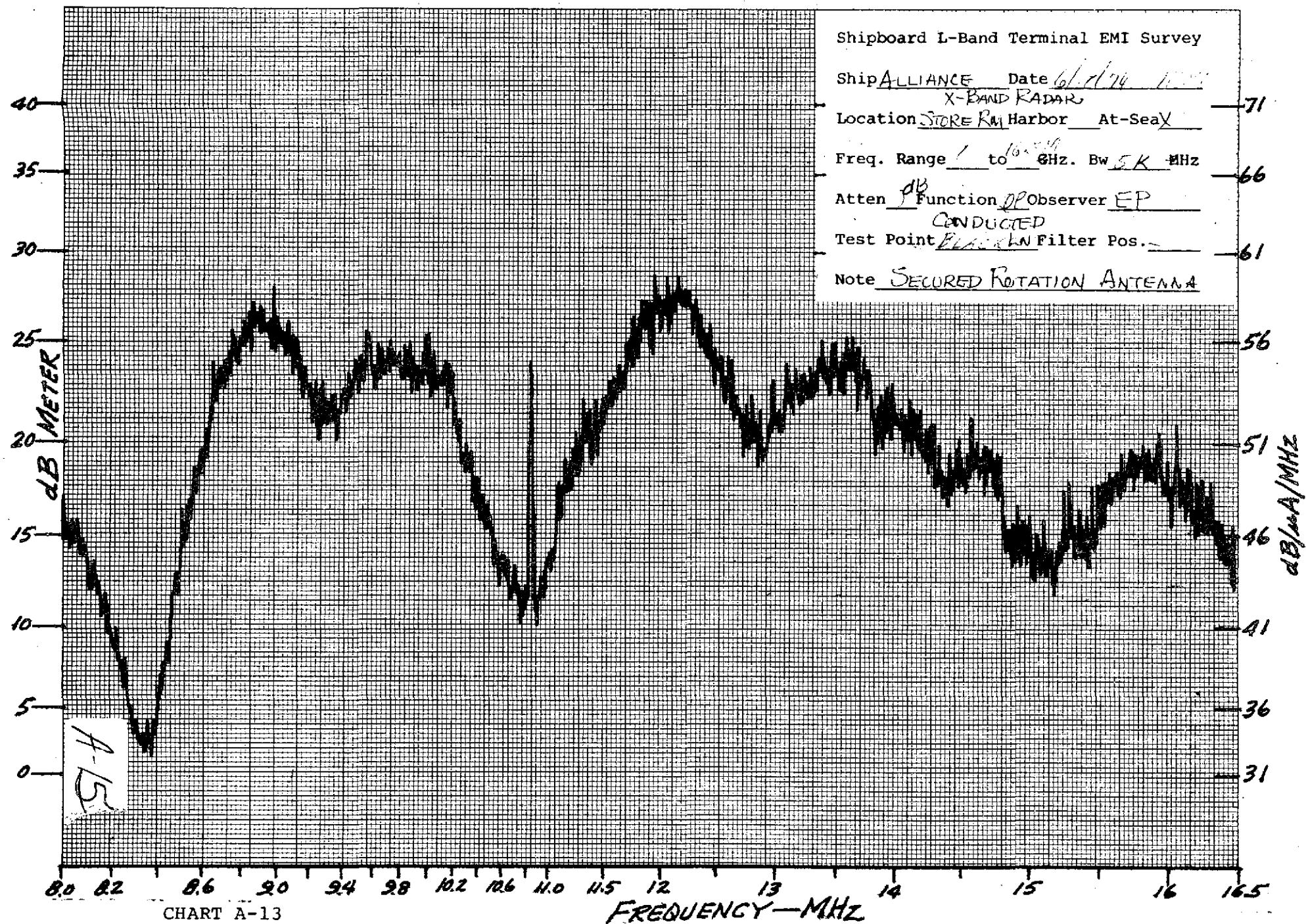


CHART A-12



Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 1131

X-BAND RADAR

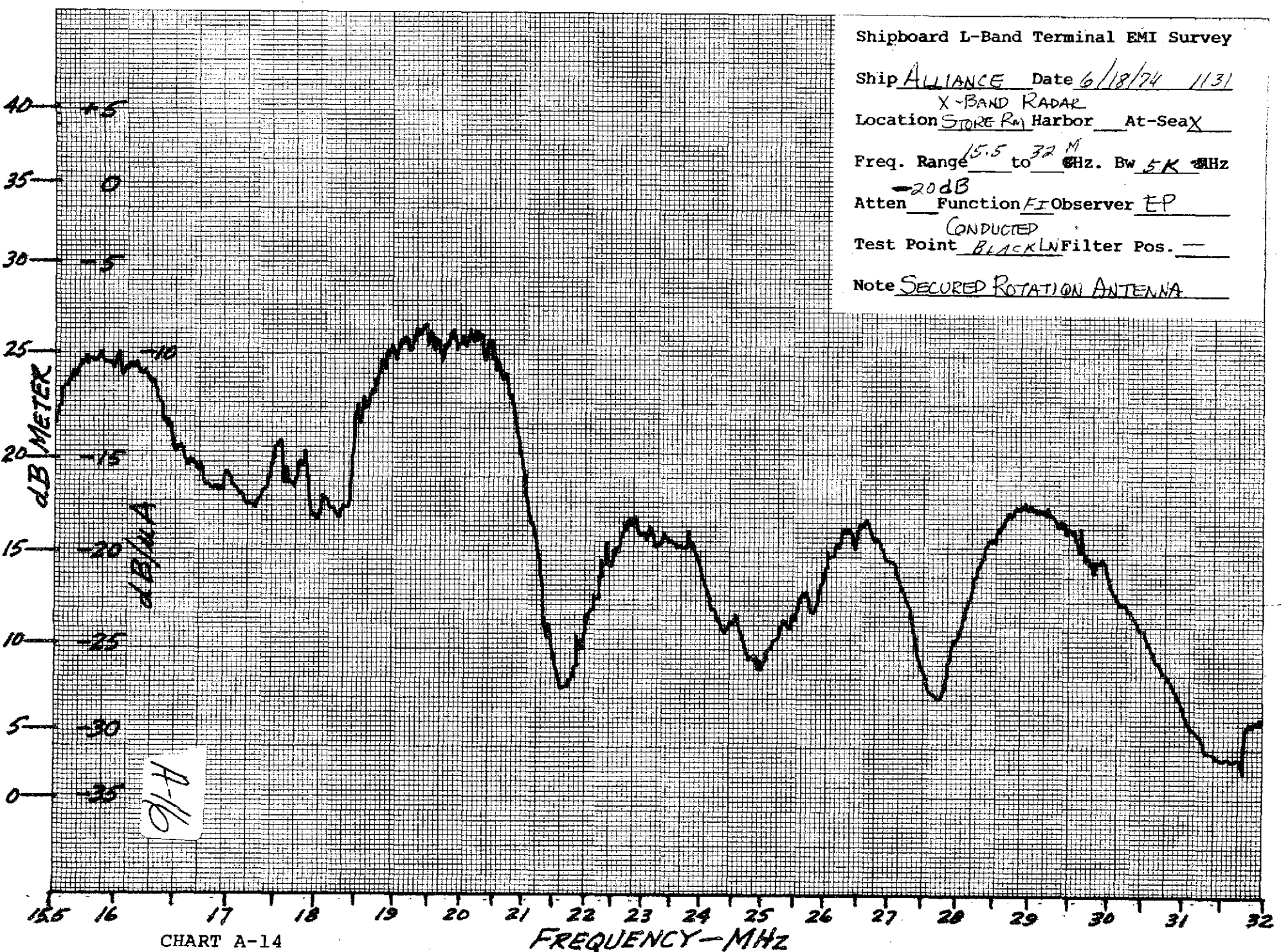
Location STORE RM Harbor At-Sea X

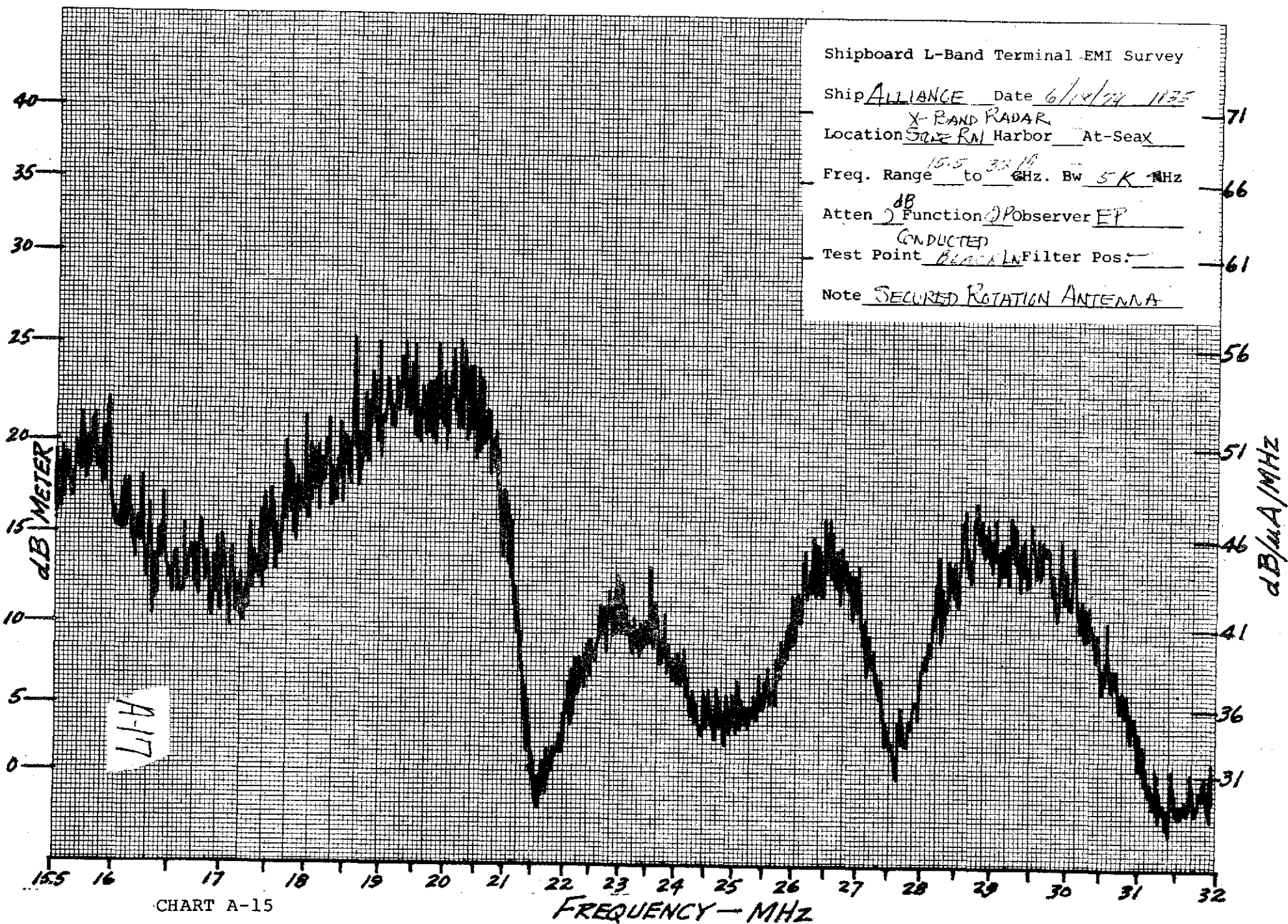
Freq. Range 15.5 to 32 M GHz. Bw 5K MHz

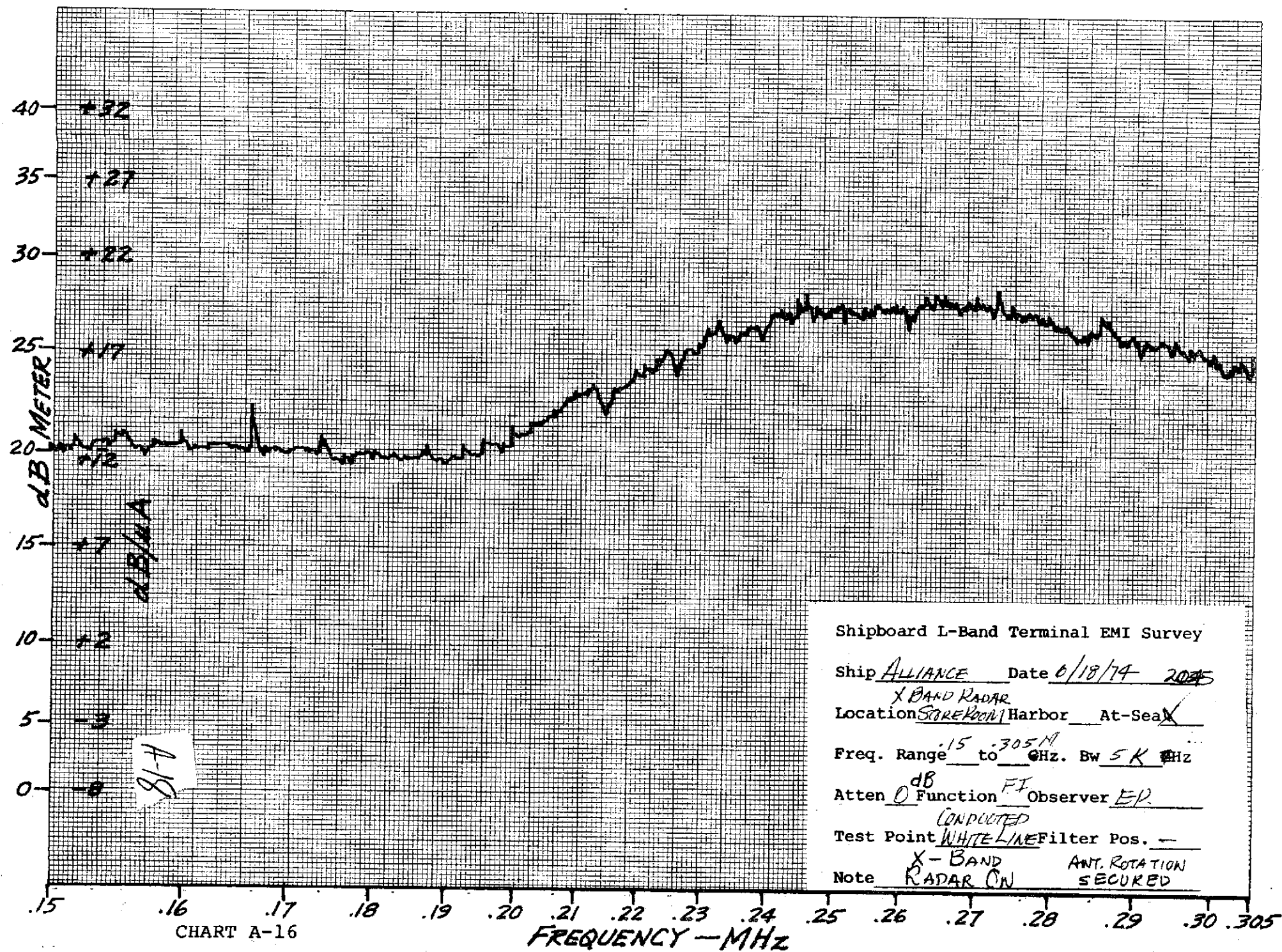
Atten -20dB Function FI Observer EP

Test Point CONDUCTED BLACK LN Filter Pos. ---

Note SECURED ROTATION ANTENNA







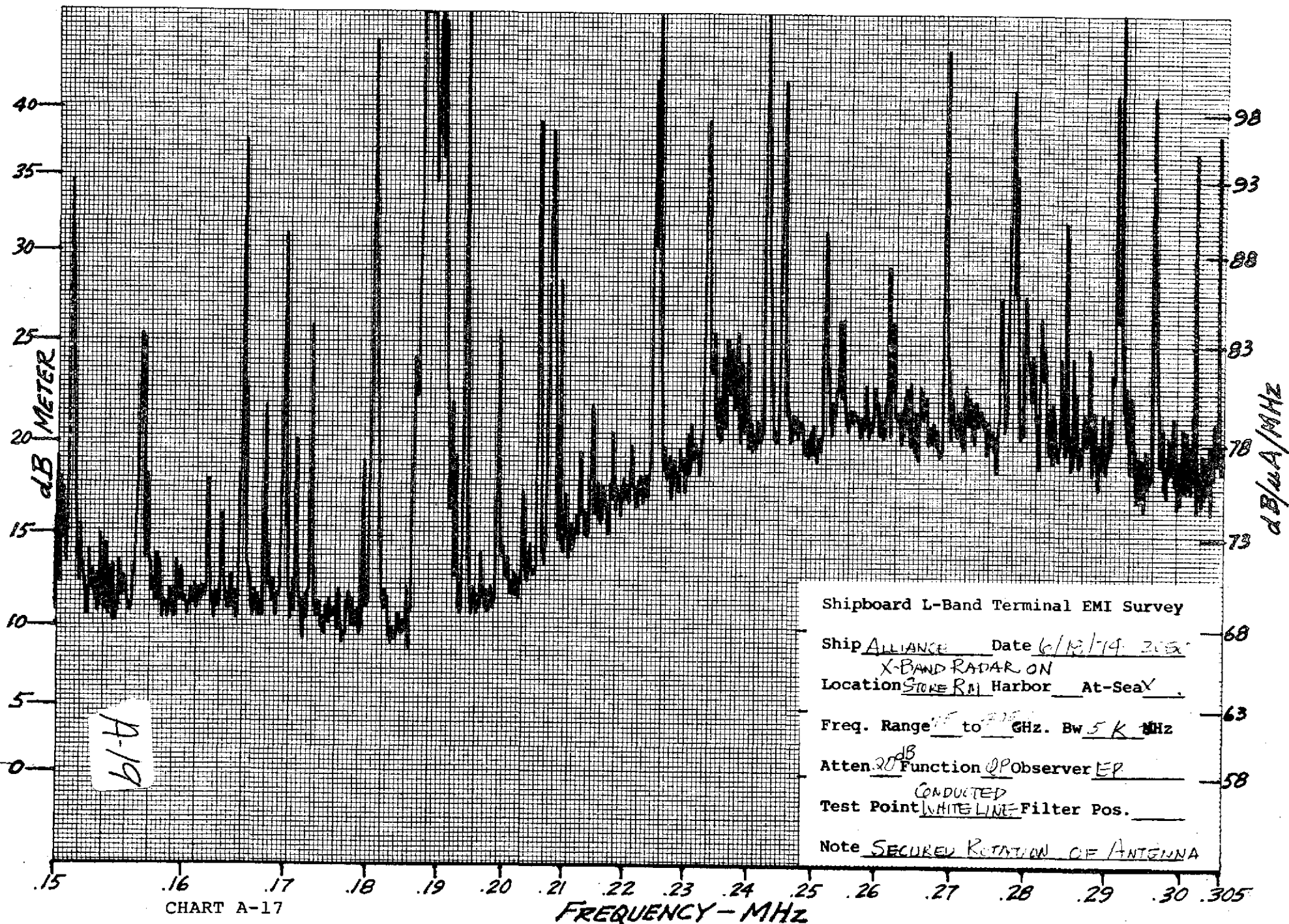
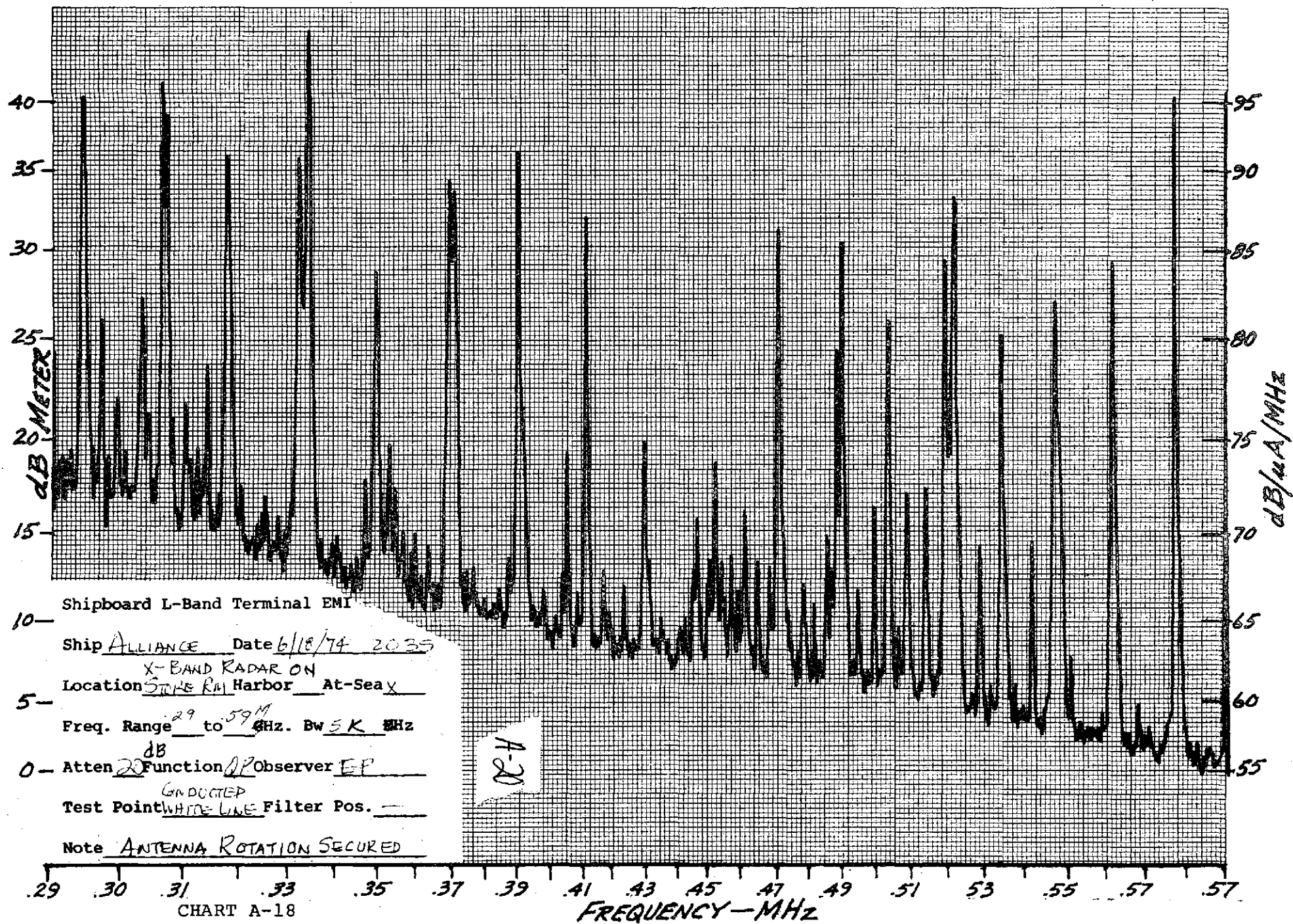


CHART A-17



Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 11/18/74 2040

X-BAND RADAR ON
Location SCORE RM Harbor At-Sea

Freq. Range 29 to 59 ^MGHz. Bw 5K ^MHz

Atten 0 ^{dB} Function F1 Observer E.P.

CONDUCTED
Test Point WHITE LWE Filter Pos. —

Note ANTENNA ROTATION SECURED

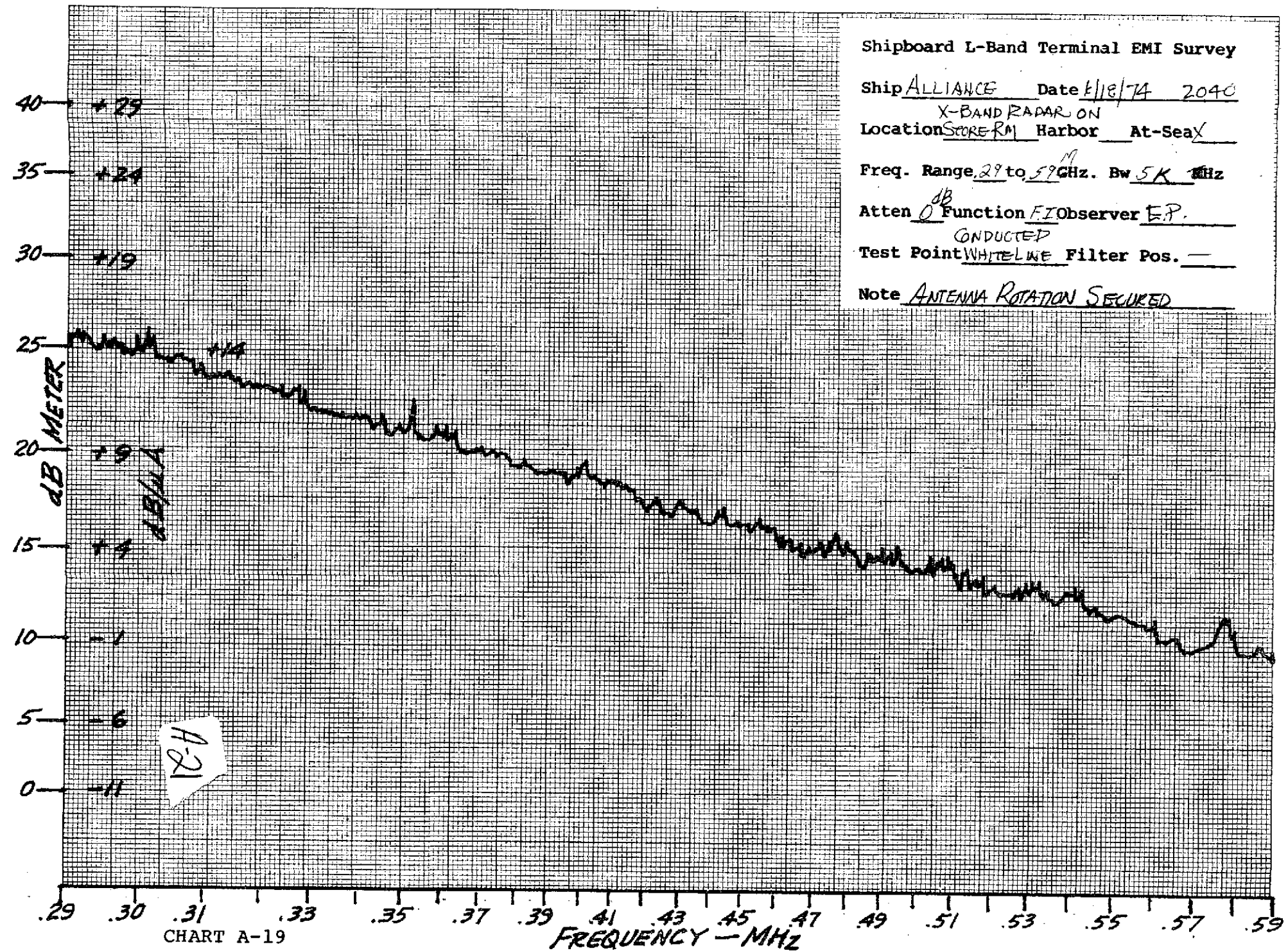


CHART A-19

FREQUENCY - MHz

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 2045

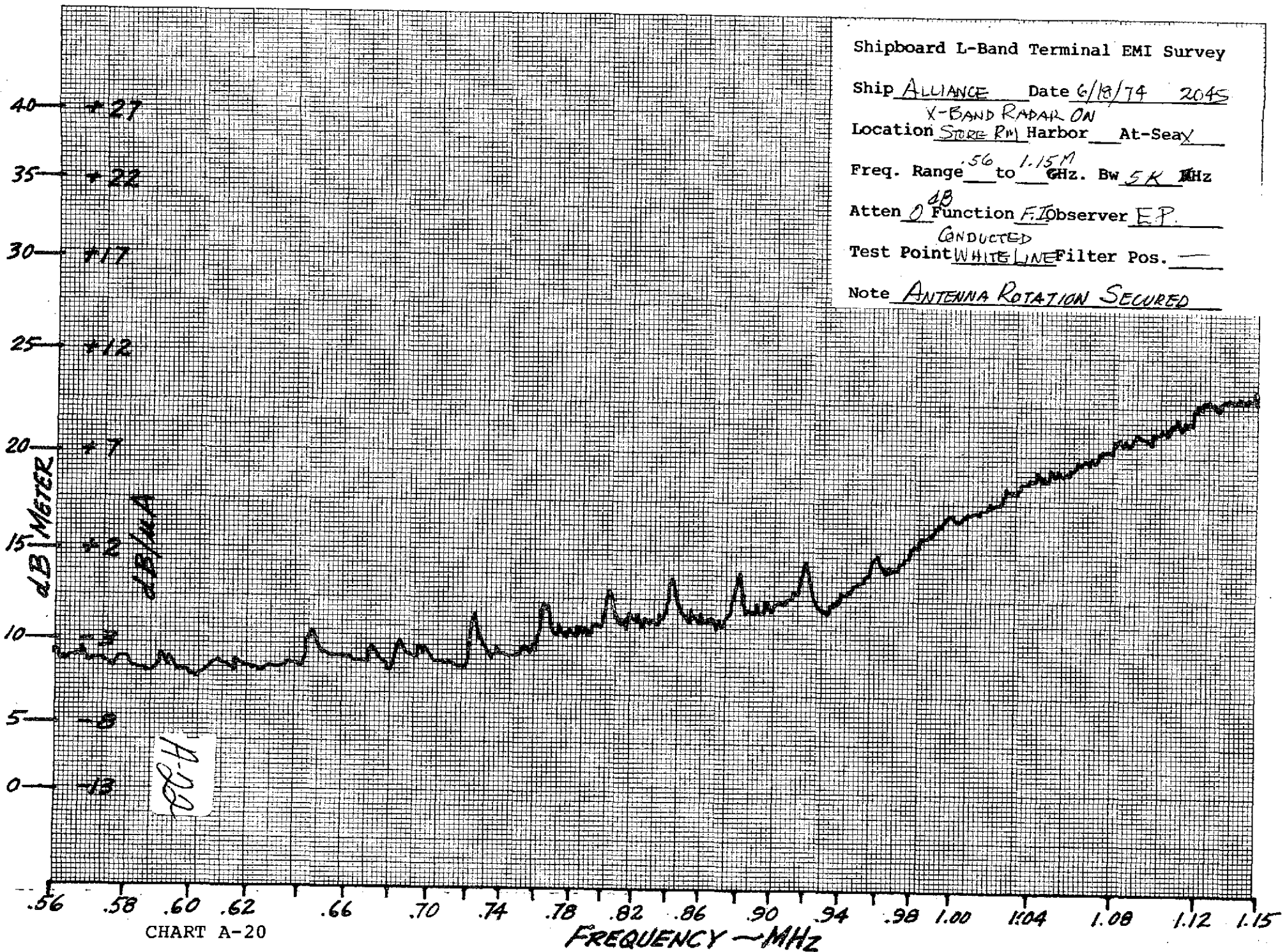
X-BAND RADAR ON
Location STORE RM Harbor At-Sea X

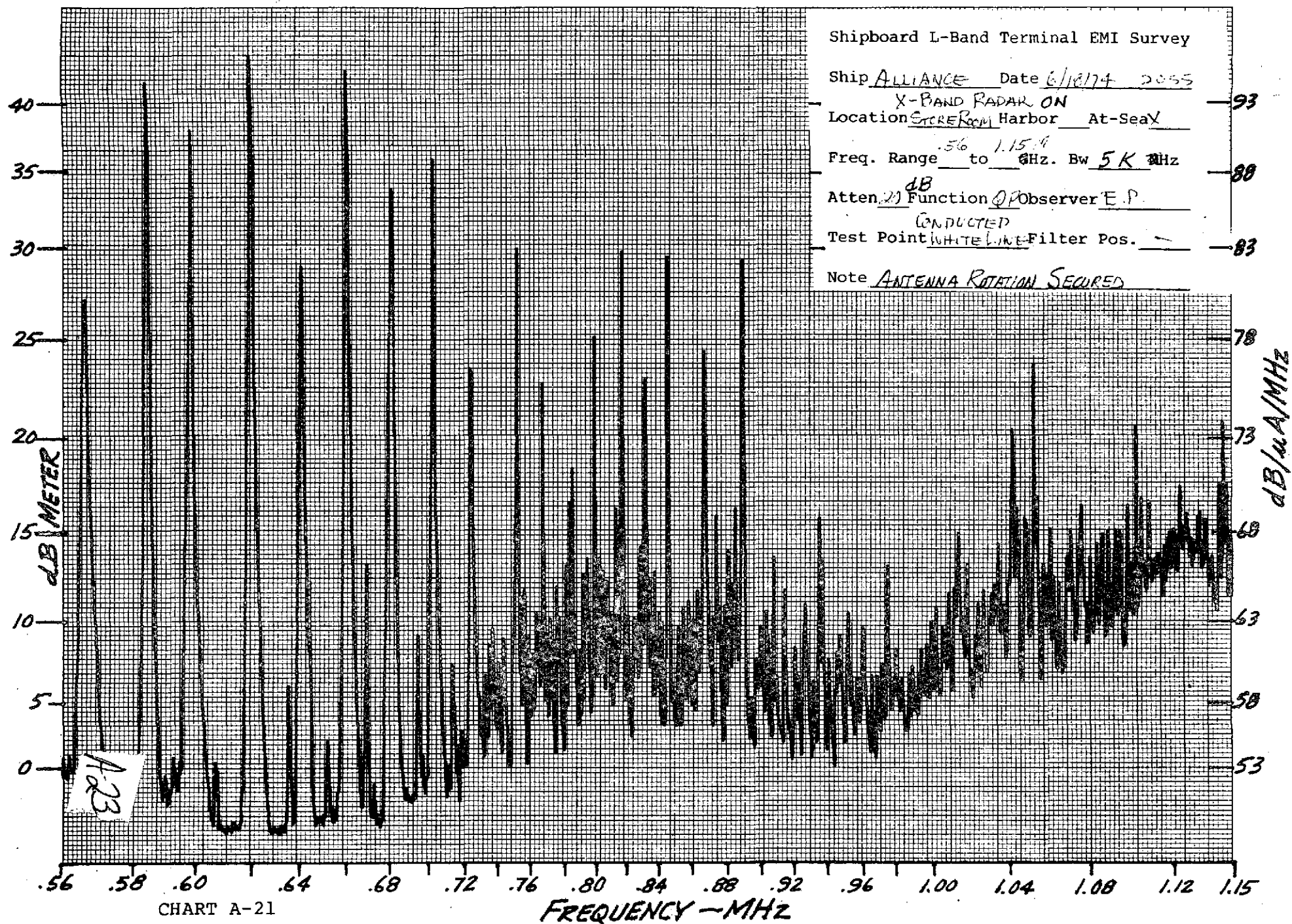
Freq. Range .56 to 1.15 GHz. Bw 5K MHz

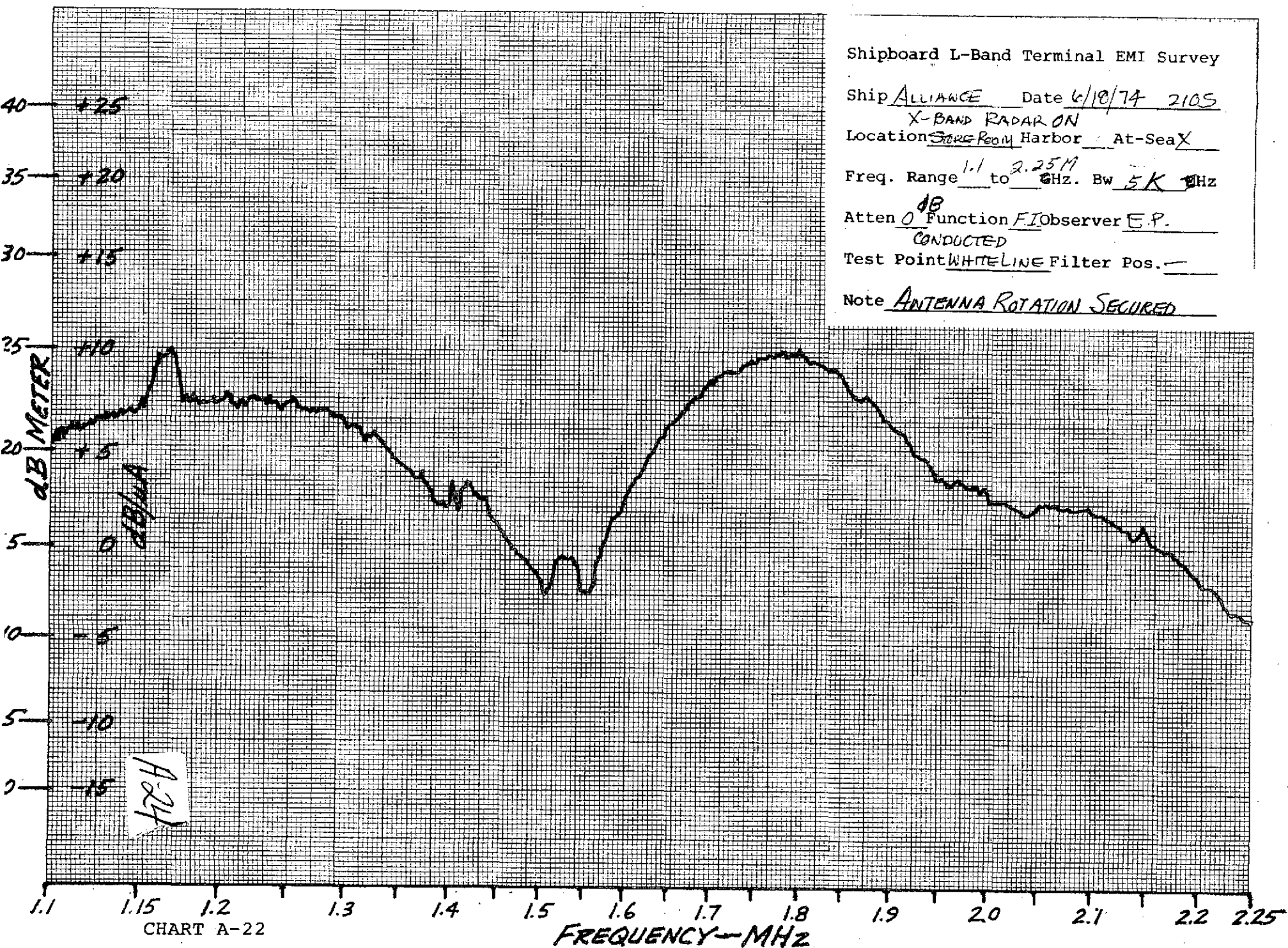
Atten 0 ^{dB} Function F Observer EP

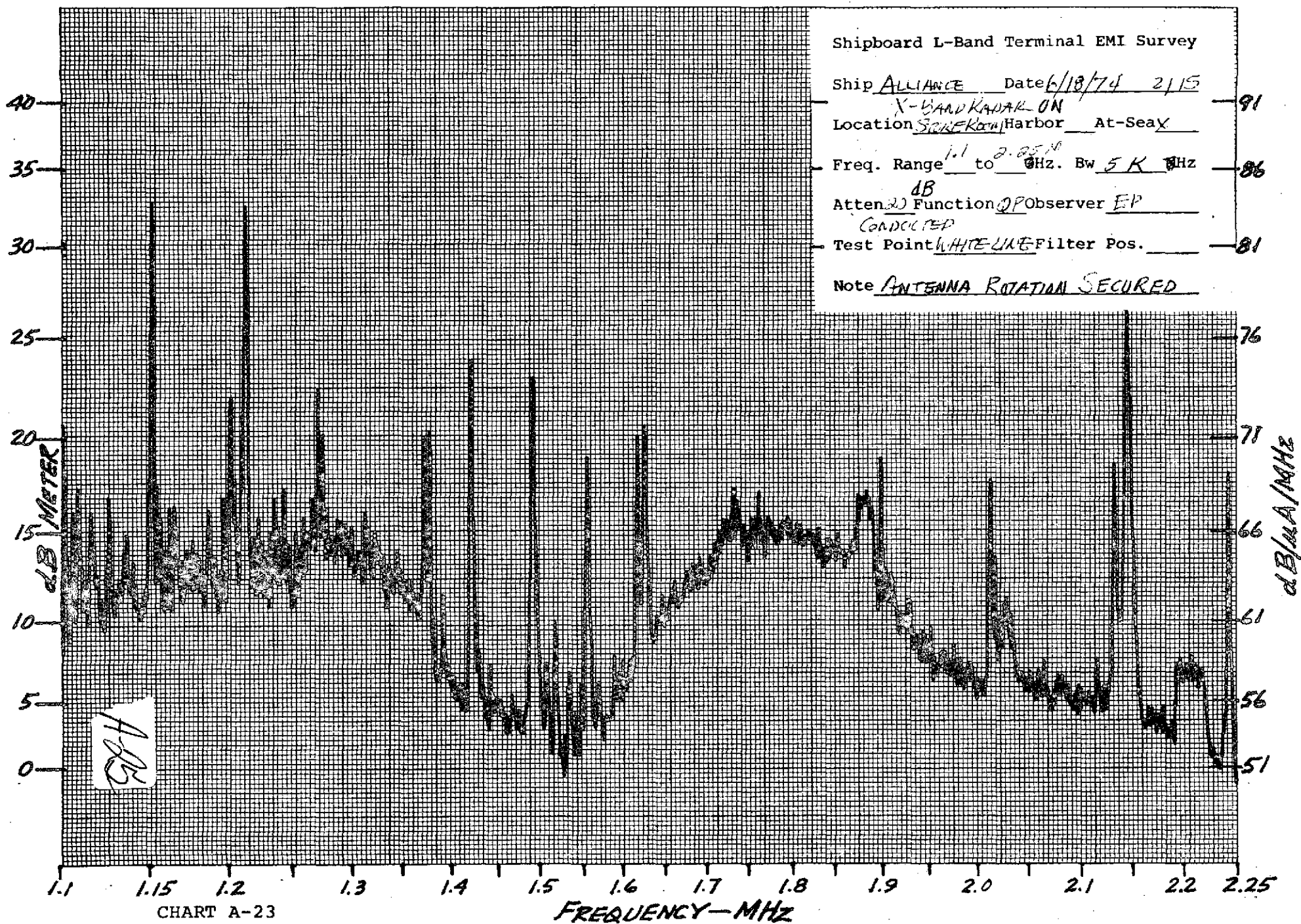
Test Point CONDUCTED WHITE LINE Filter Pos. —

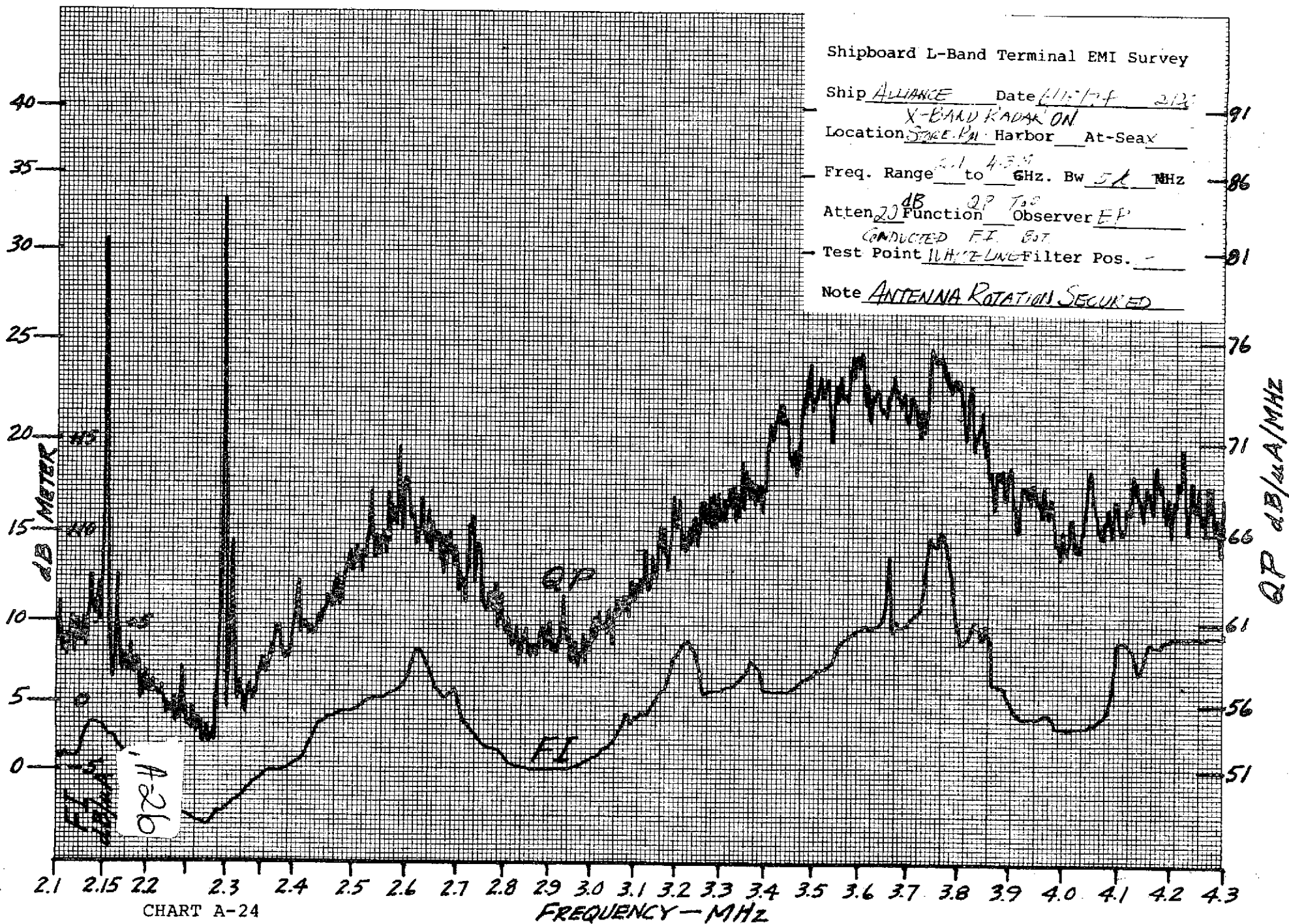
Note ANTENNA ROTATION SECURED

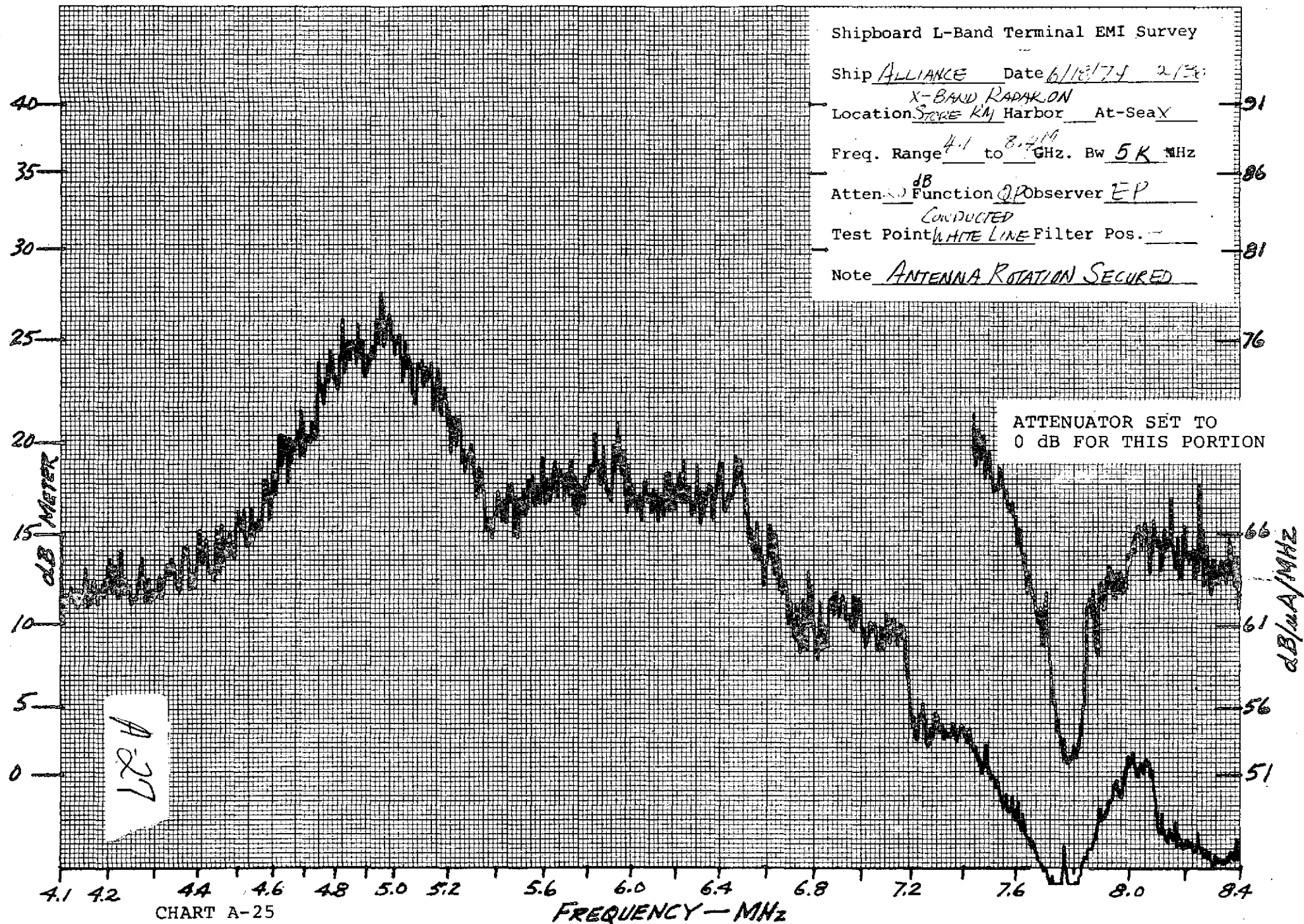












Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 2140

X-BAND RADAR ON

Location STORERM Harbor At-Sea X

Freq. Range 4.1 to 8.419 GHz. Bw 5 K MHz

Atten 0 ^{dB} Function FI Observer EP

Test Point CONDUCTED WHITE LINE Filter Pos.

Note ANTENNA ROTATION SECURED

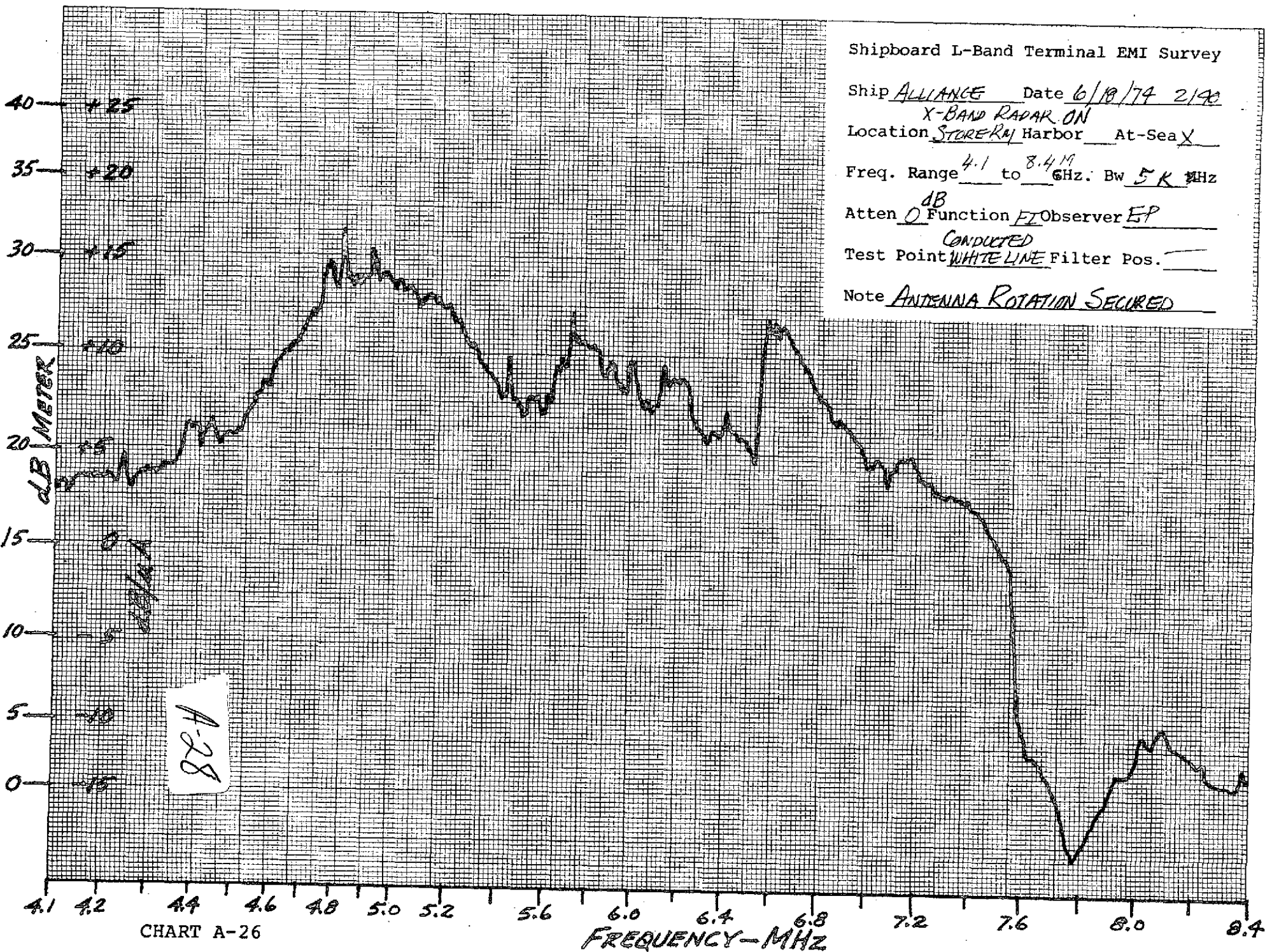


CHART A-26

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 2150

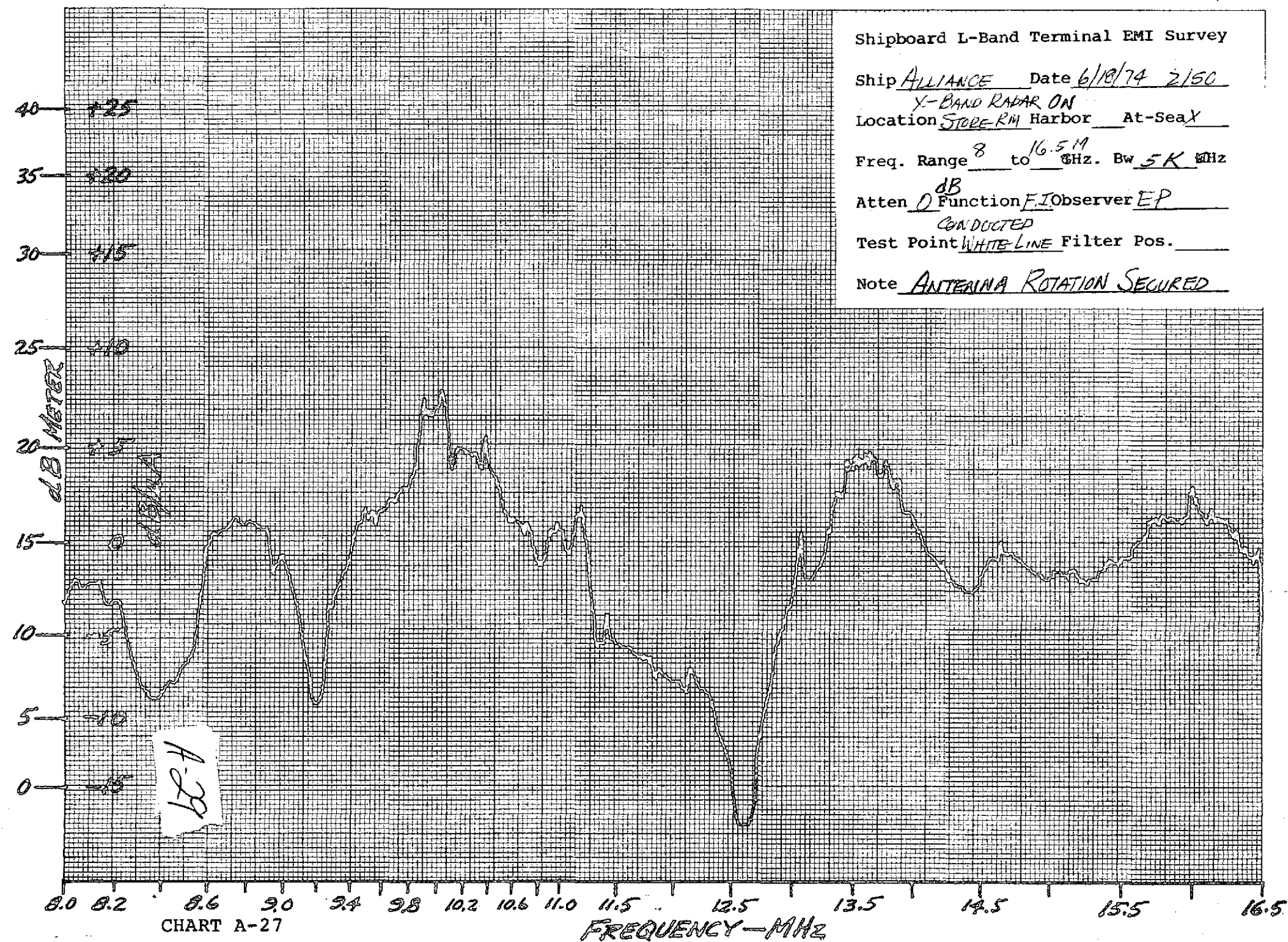
X-BAND RADAR ON
Location STORE RM Harbor At-Sea X

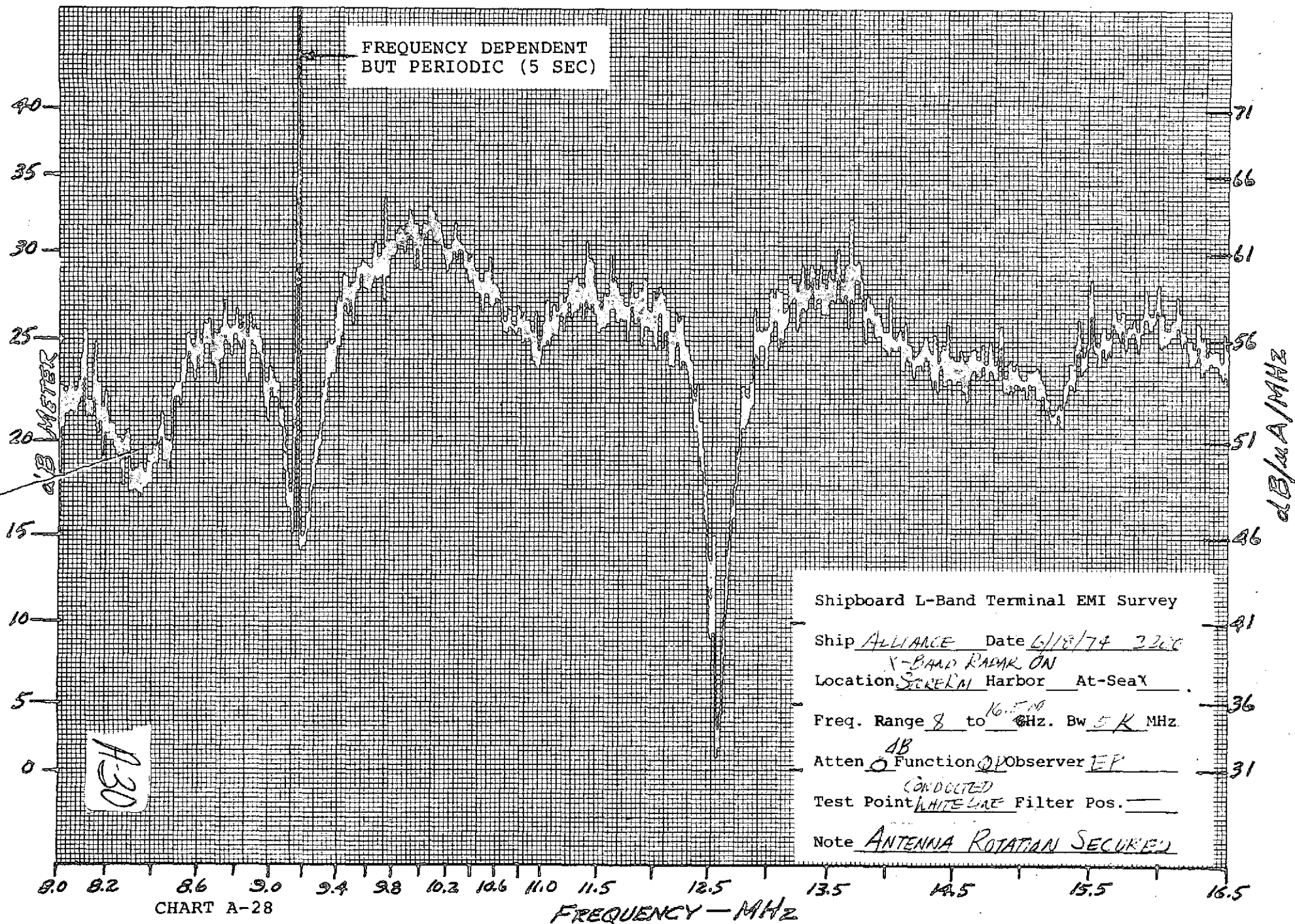
Freq. Range 8 to 16.5 M GHz. Bw 5 K Hz

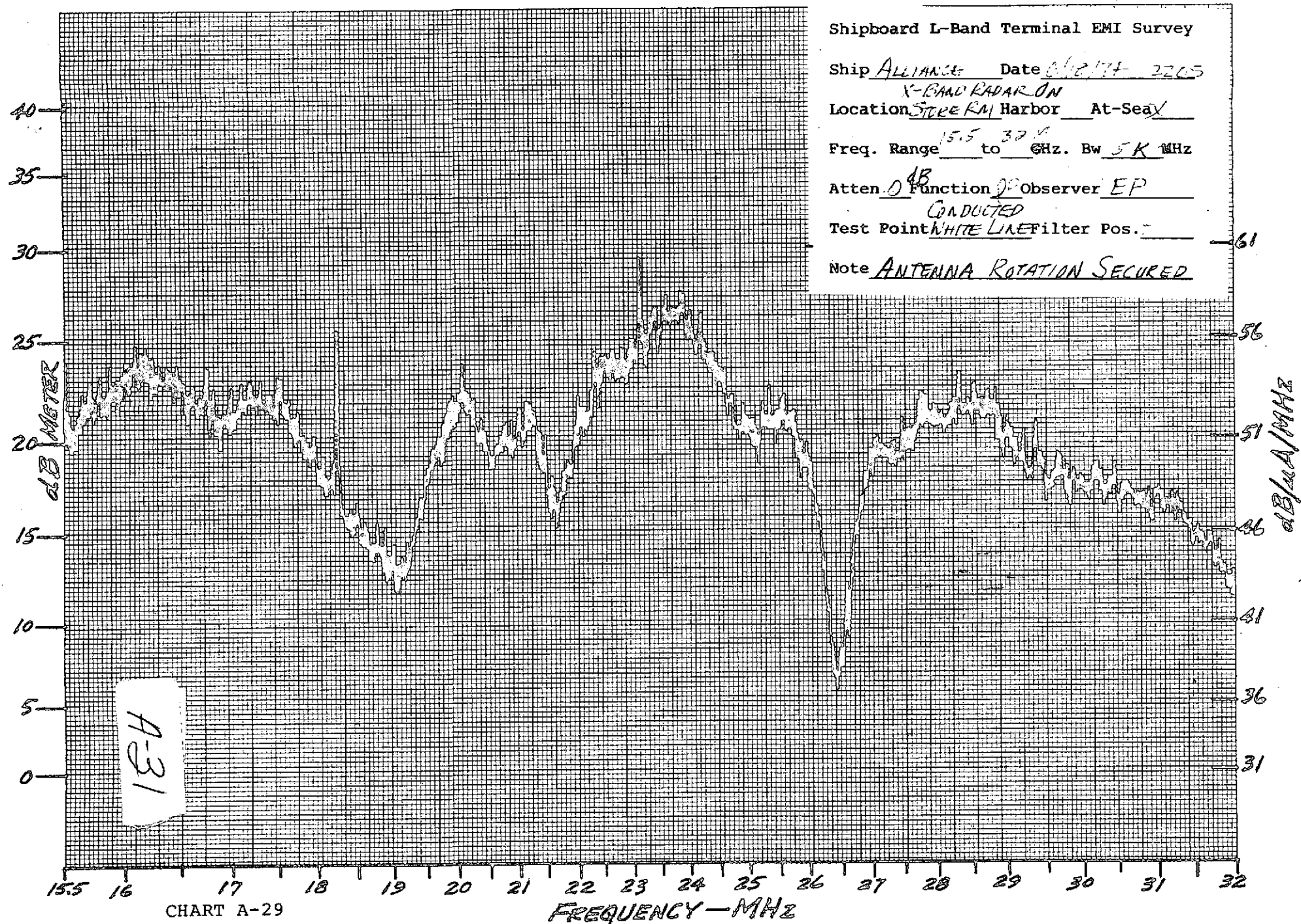
Atten dB Function F.I Observer EP

CONDUCTED
Test Point WHITE LINE Filter Pos.

Note ANTENNA ROTATION SECURED







Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 2210

X-BAND RADAR ON

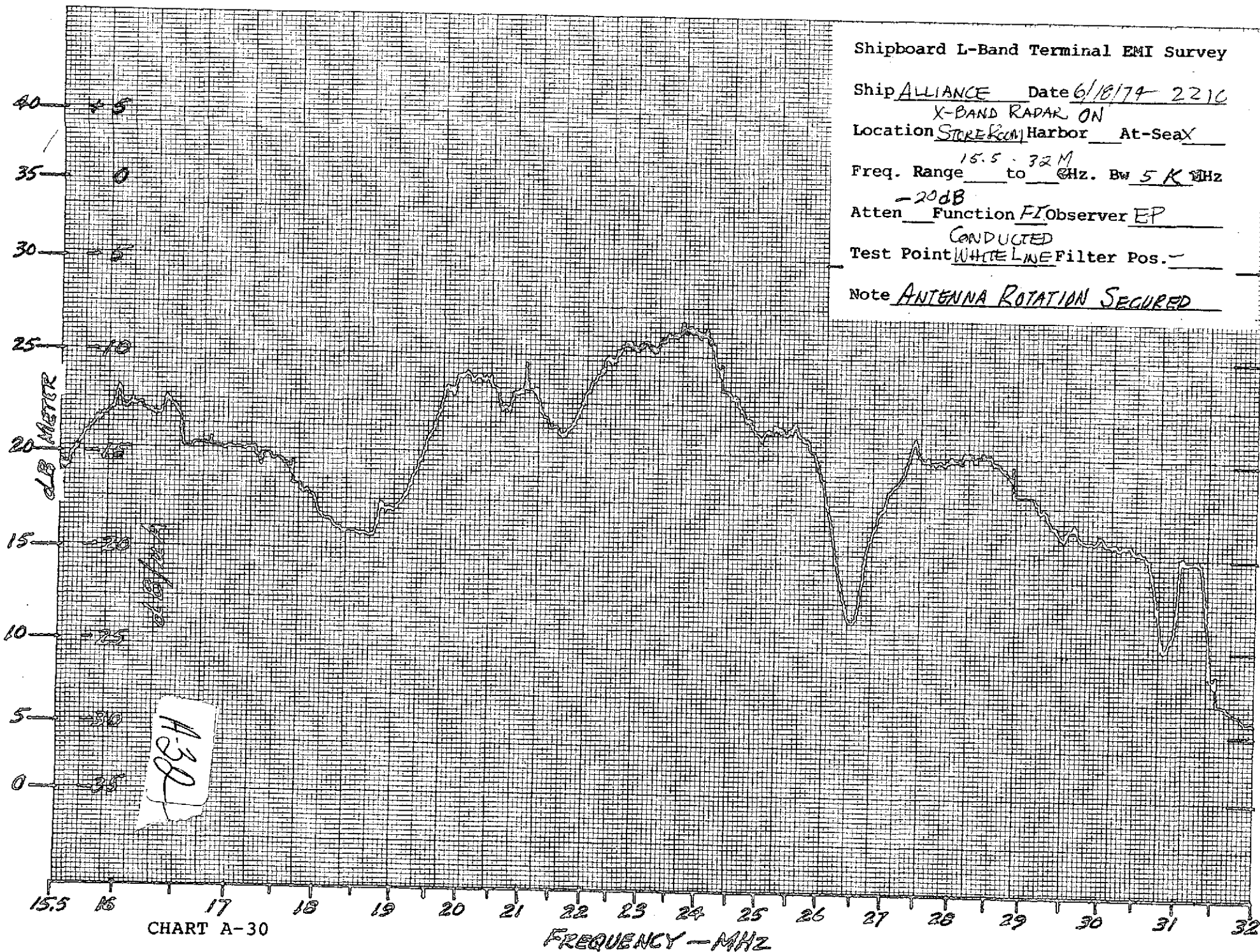
Location STOKERON Harbor At-Sea X

Freq. Range 15.5 - 32 M to GHz. Bw 5 K Hz

Atten -20dB Function FI Observer EP

Test Point CONDUCTED WHITE LINE Filter Pos. -

Note ANTENNA ROTATION SECURED



Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 2035S-BAND RADAR ONLocation STORAGE RM Harbor At-Sea ✓Freq. Range 15 to 30.5 MHz. Bw 5 KHzAtten 0 dB Function F1 Observer EP.Test Point T1 Filter Pos. —

ANTENNA ROTATION SECURED

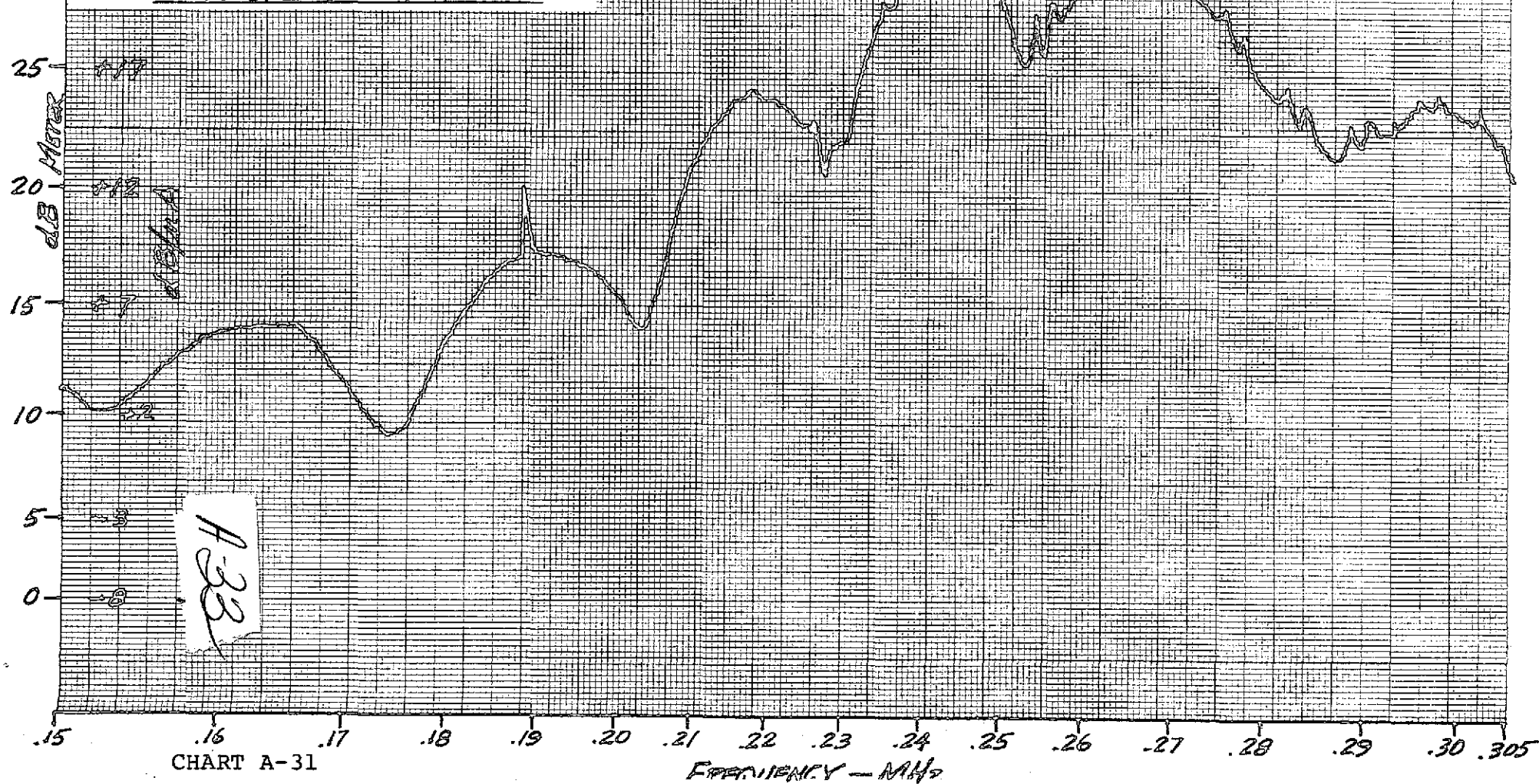
Note CONDUCTED EMISSION, RADAR ON

CHART A-31

FREQUENCY - MHz

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/13/74 182

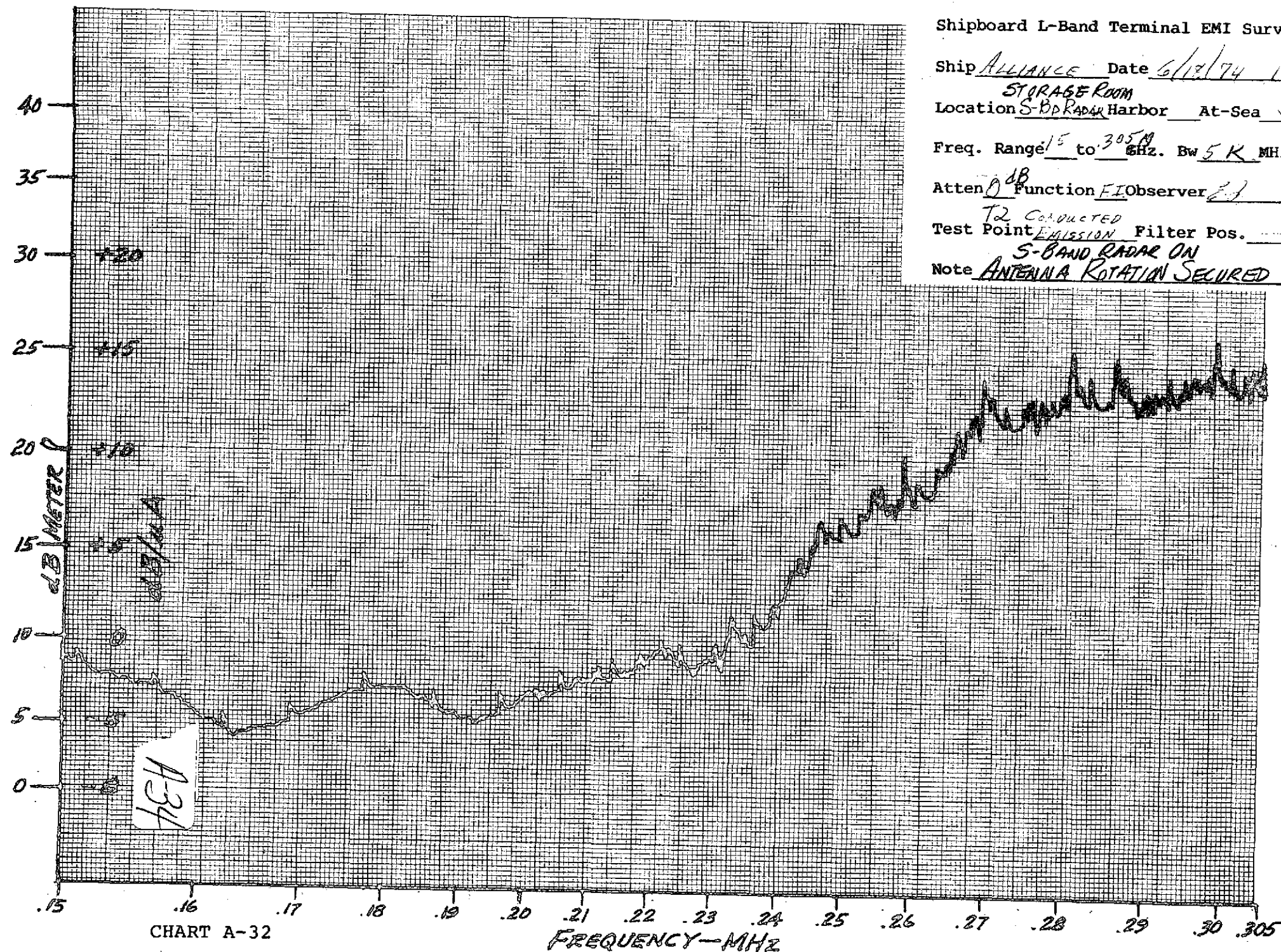
Location STORAGE ROOM
S-BD RADAR Harbor At-Sea ☒

Freq. Range 15 to 305 MHz. Bw 5 K MHz

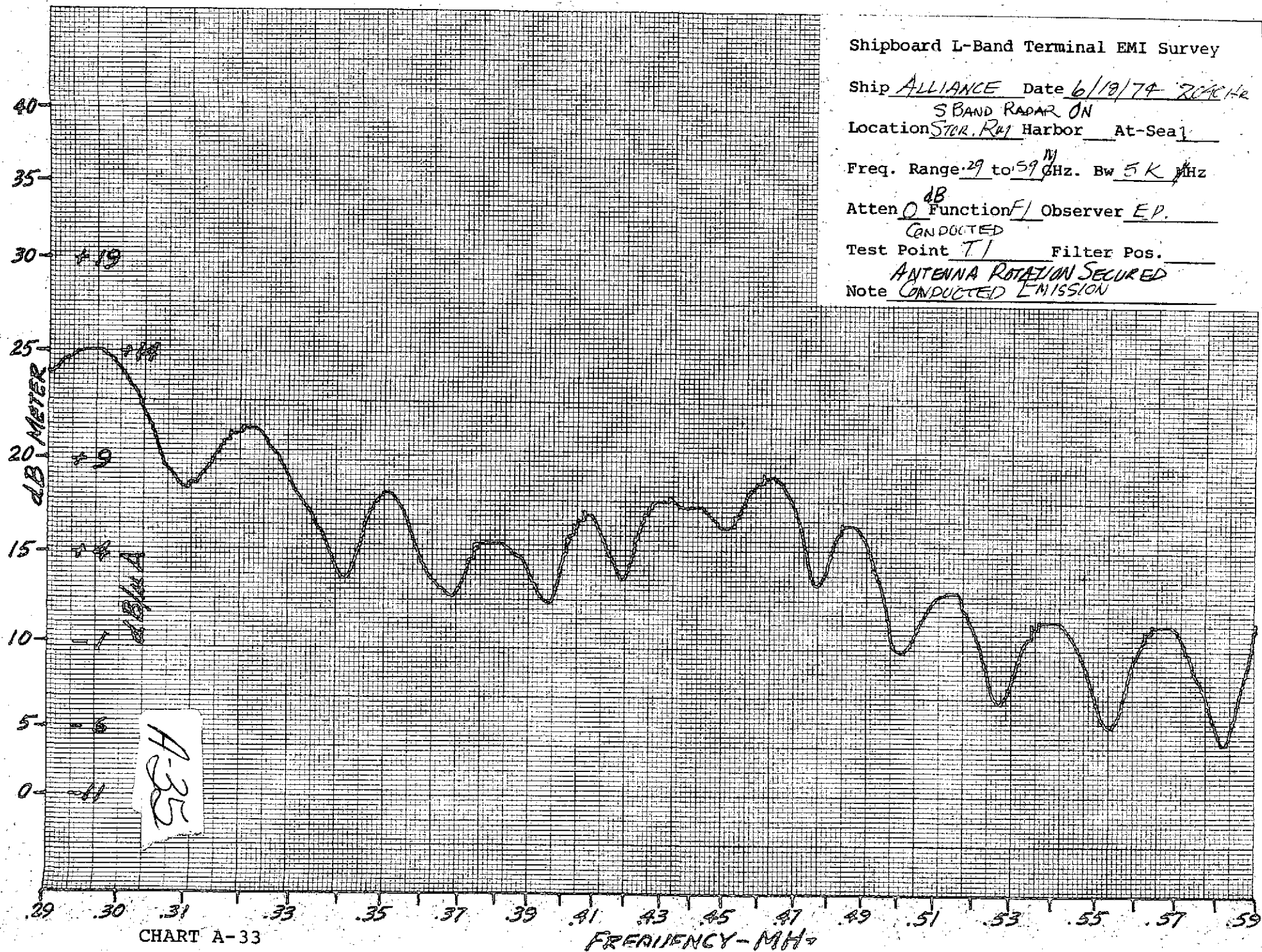
Atten 0 dB Function F Observer ED

Test Point T2 CONDUCTED Filter Pos. EMISSION

Note S-BAND RADAR ON
ANTENNA ROTATION SECURED



Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 ZORKERS BAND RADAR ON
Location STOR. RM Harbor At-Sea 1Freq. Range .29 to .59 ^MGHz. Bw 5 K MHzAtten 0 ^{dB} Function F1 Observer EP.CONDUCTED
Test Point T1 Filter Pos. ANTENNA ROTATION SECURED
Note CONDUCTED EMISSION

9

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/1/74
RADAR ON - ANTENNA SECURED
Location SEA Harbor At-Sea 1 75

Freq. Range 1 to 7.6 GHz. Bw 5K MHz

Atten 0 dB Function QF Observer ED 70

Test Point T2 Filter Pos. 1

ALL 4 RESOURCES IN QF WERE
Note TIME DEPENDENT - NOT EMI 65

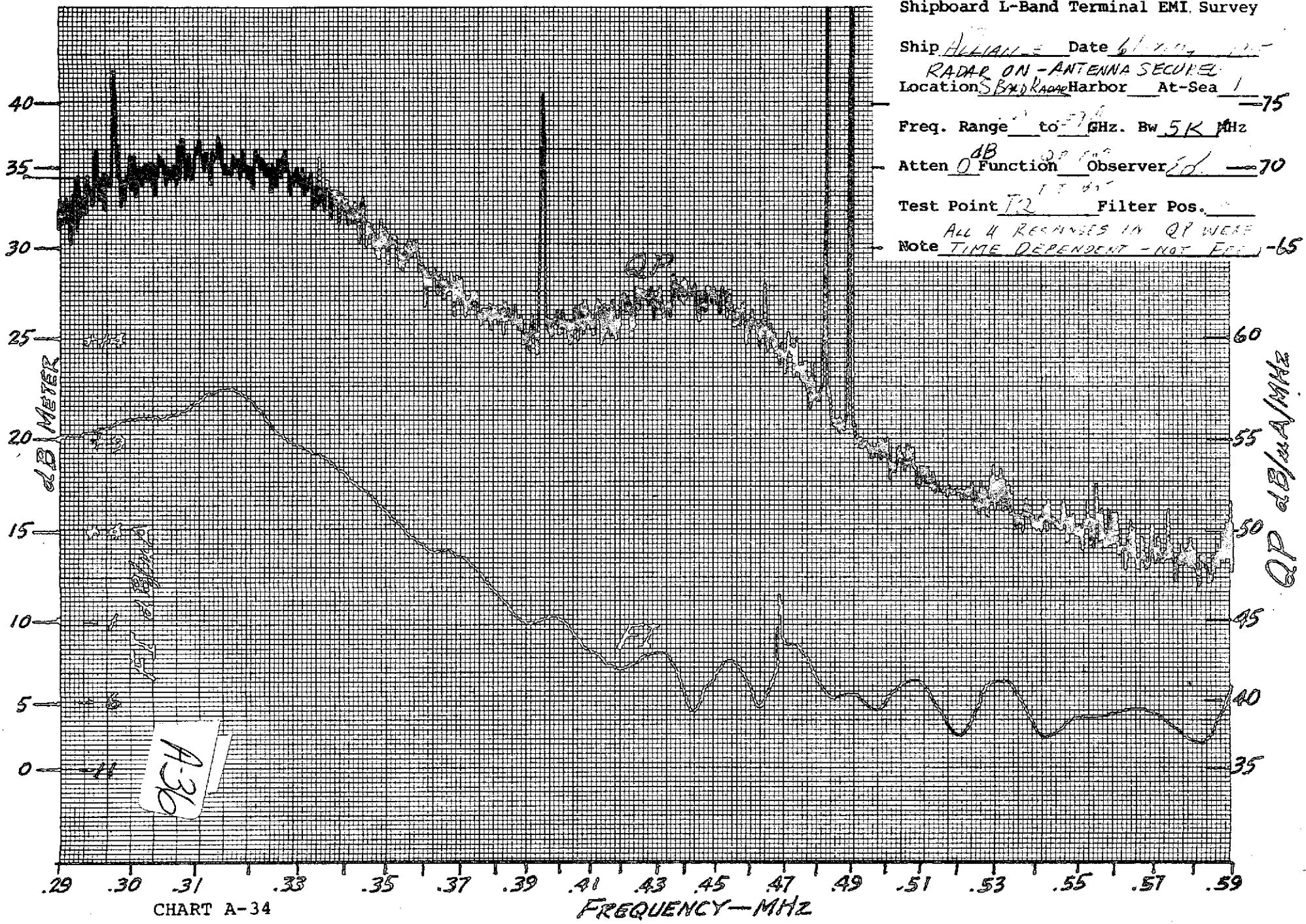


CHART A-34

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 1970

STORAGE ROOM

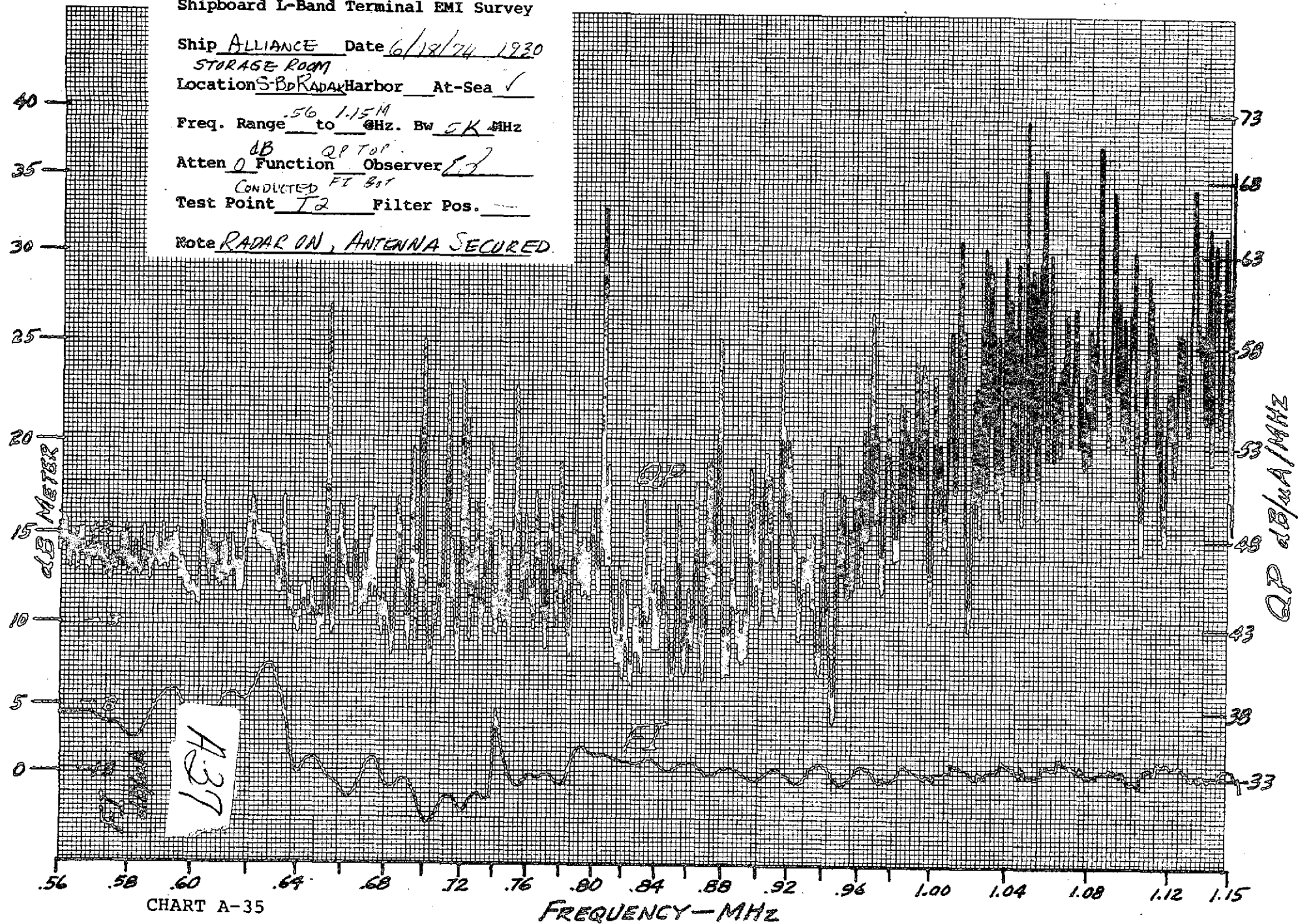
Location S-Bd RADAR Harbor At-Sea ☒Freq. Range .56 to 1.15 MHz. Bw 5K MHzAtten 0B QP TOP
Function Observer ELCONDUCTED FT 811
Test Point T2 Filter Pos. ---Note RADAR ON, ANTENNA SECURED.

CHART A-35

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/1/76 1976

Location STORAGE ROOM
POKADAK Harbor At-Sea ✓ -71

Freq. Range 1.1 to 2.25 MHz. Bw 5K Hz

Atten dB Function DP TOP Observer ECJ -66

Test Point CONDUCTED FE 31
T2 Filter Pos. _____

Note RADAR ON, ANTENNA SECURED -61

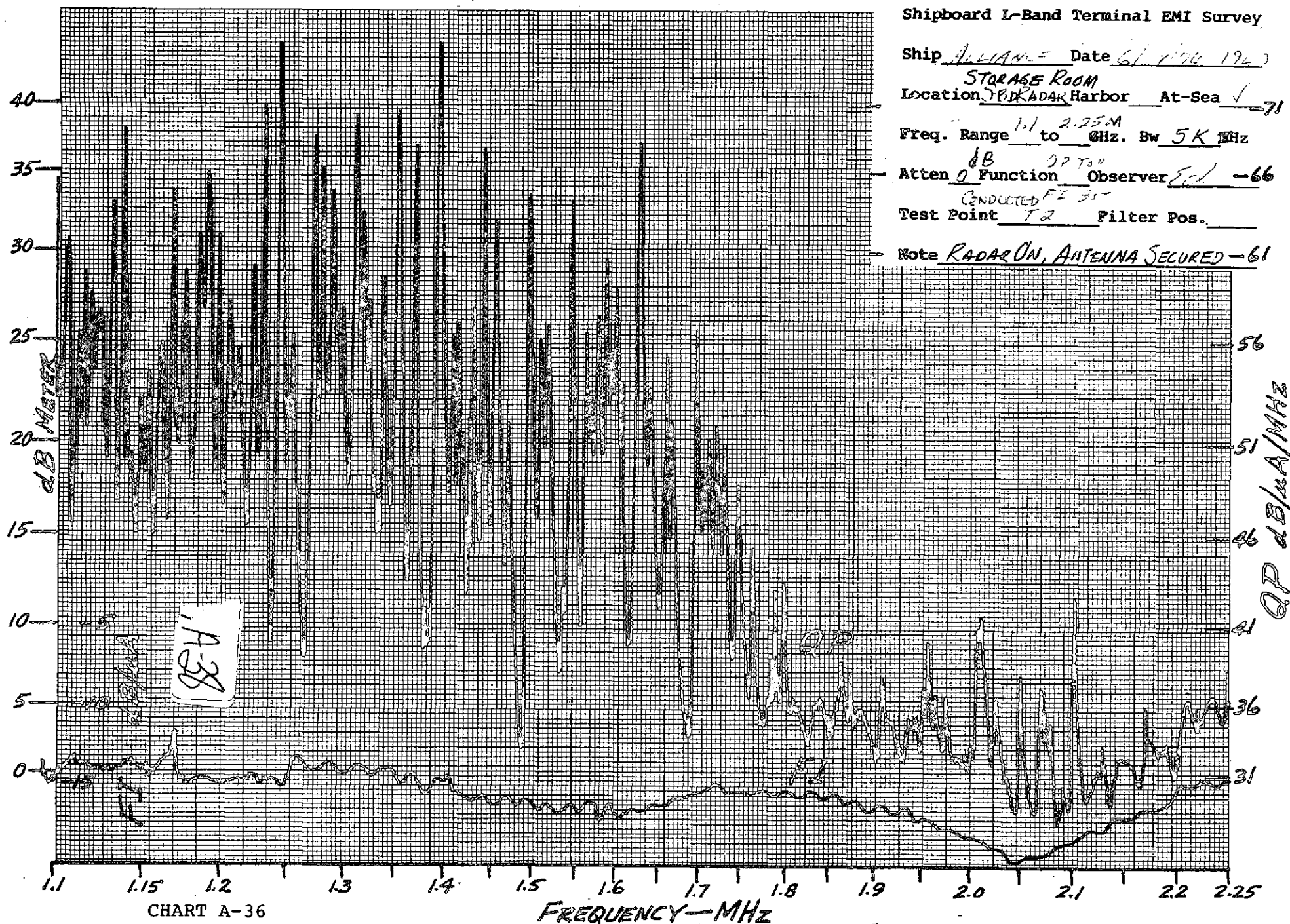


CHART A-36

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/12/74 1974
STORAGE ROOM
Location 500 KADAK Harbor At-Sea ☒
Freq. Range 2.1 to 4.34 GHz. Bw 5K GHz
Atten QP -20 dB QP TOP
Function FI Observer ED
FI 0 dB CONDUCTED FI DIST
Test Point T2 Filter Pos. —
Note RADAR ON - ANTENNA SECURED

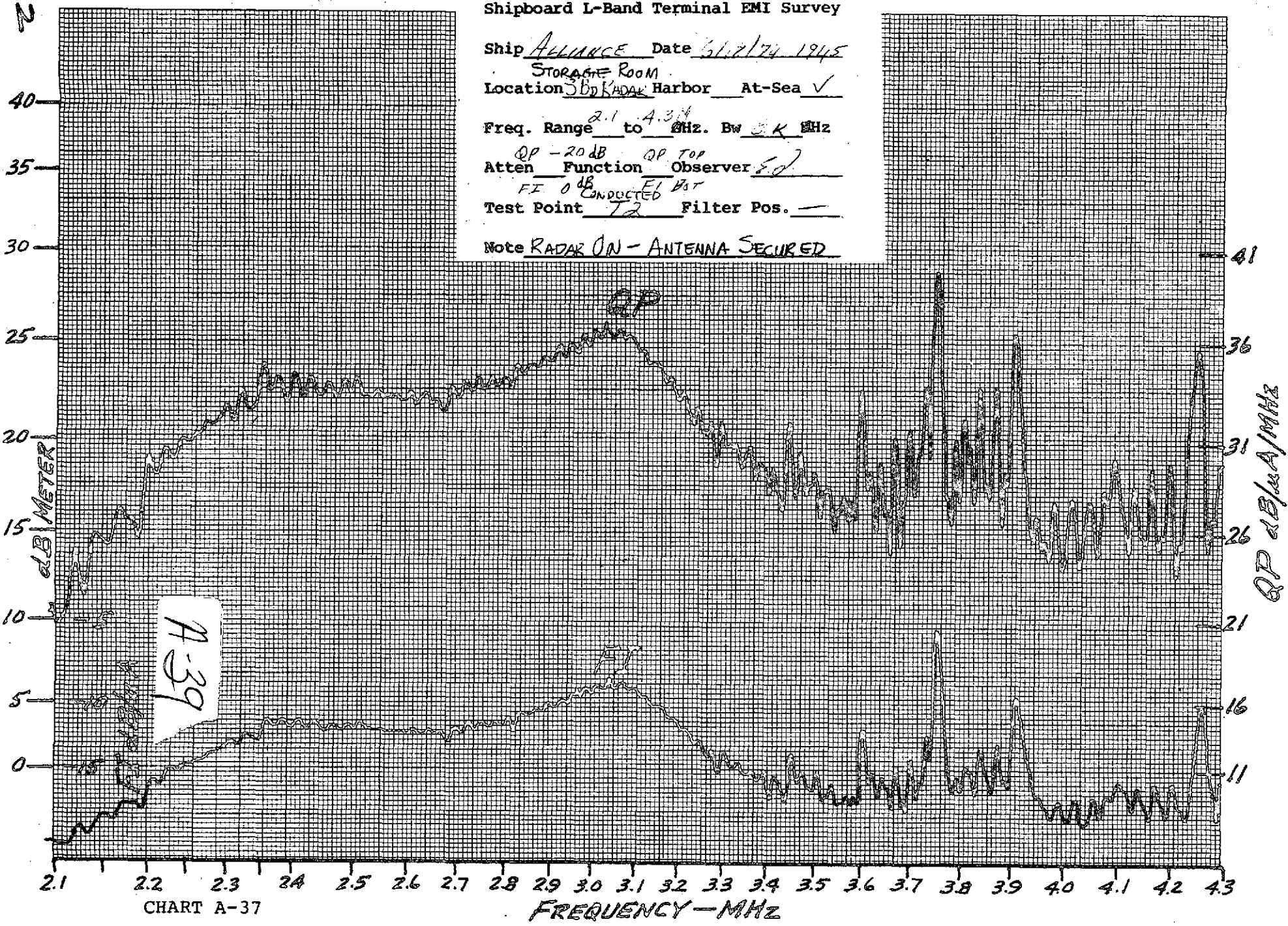


CHART A-37

Shipboard L-Band Terminal EMI Survey

Ship A-44 Date 6/17/74 231Location STORAGE ROOM
SPD RADAR Harbor At-Sea ☒Freq. Range 4.1 to 8.4 GHz. Bw 5 K HzAtten -20 dB Function F.T. Observer ELTest Point CONDUCTED T2 Filter Pos. ---Note RADAR ON - ANTENNA SECUREDFOREIGN
BROADCAST
STATION

40

35

30

25

20

15

10

5

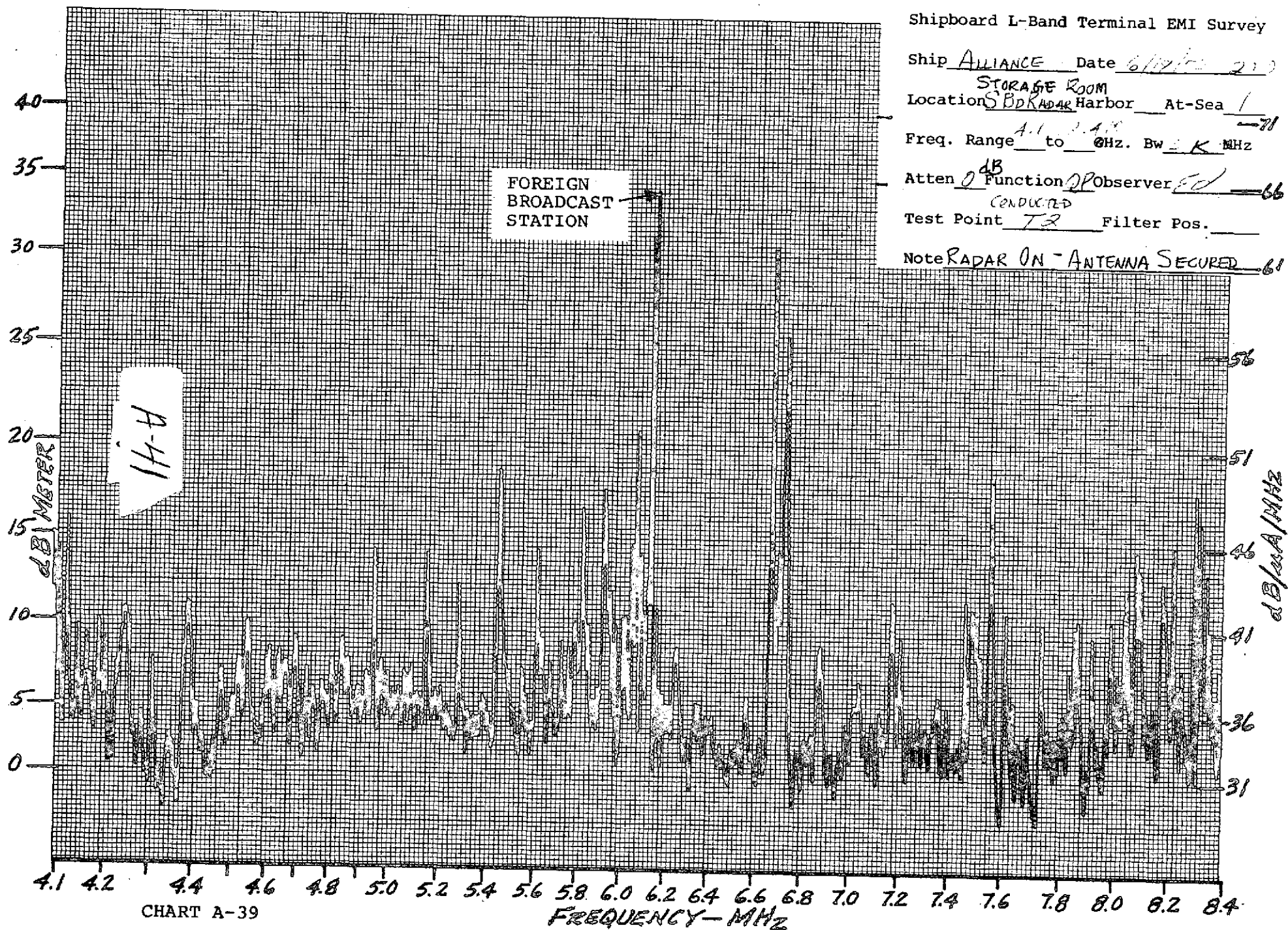
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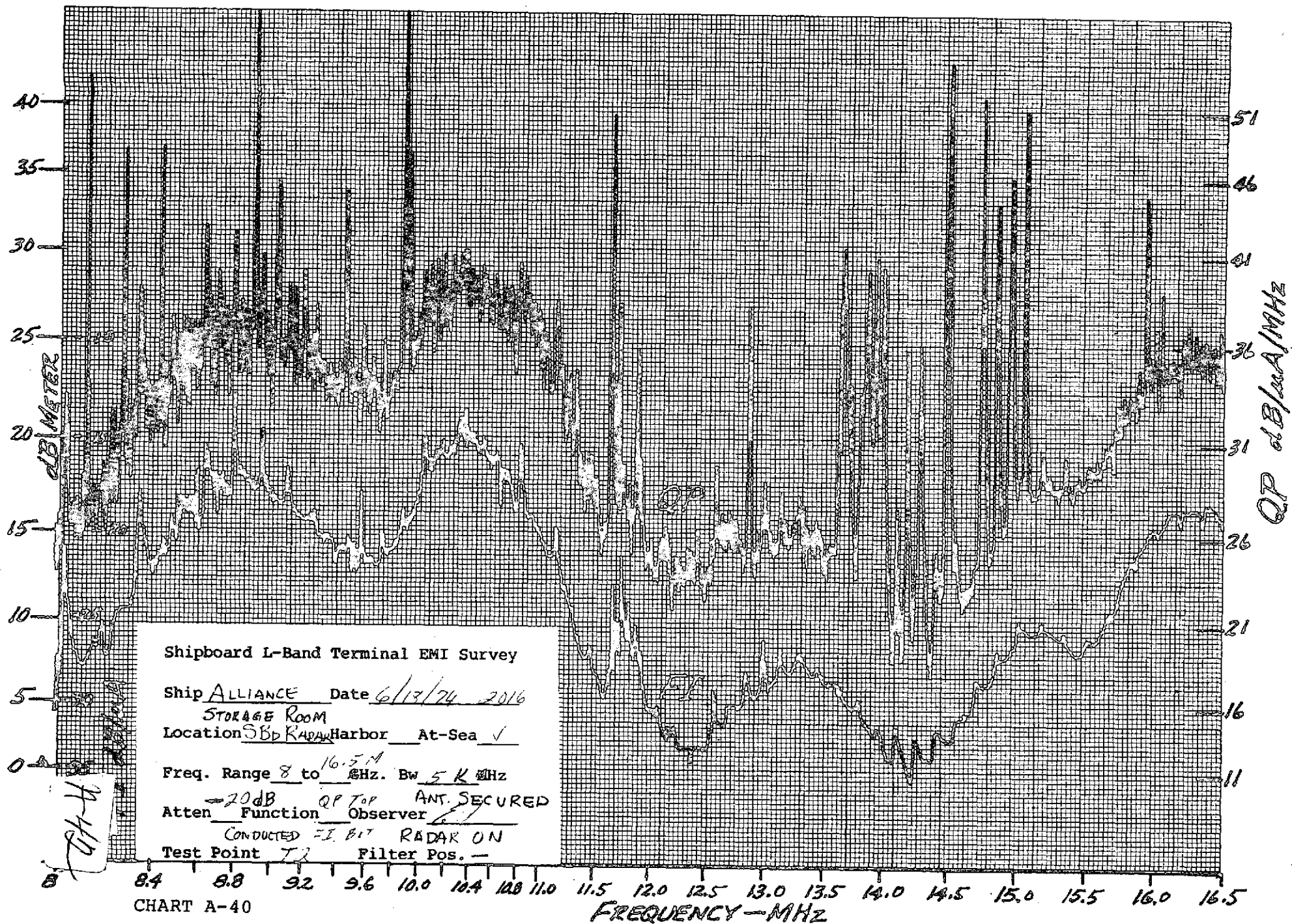
dB METER

A-44

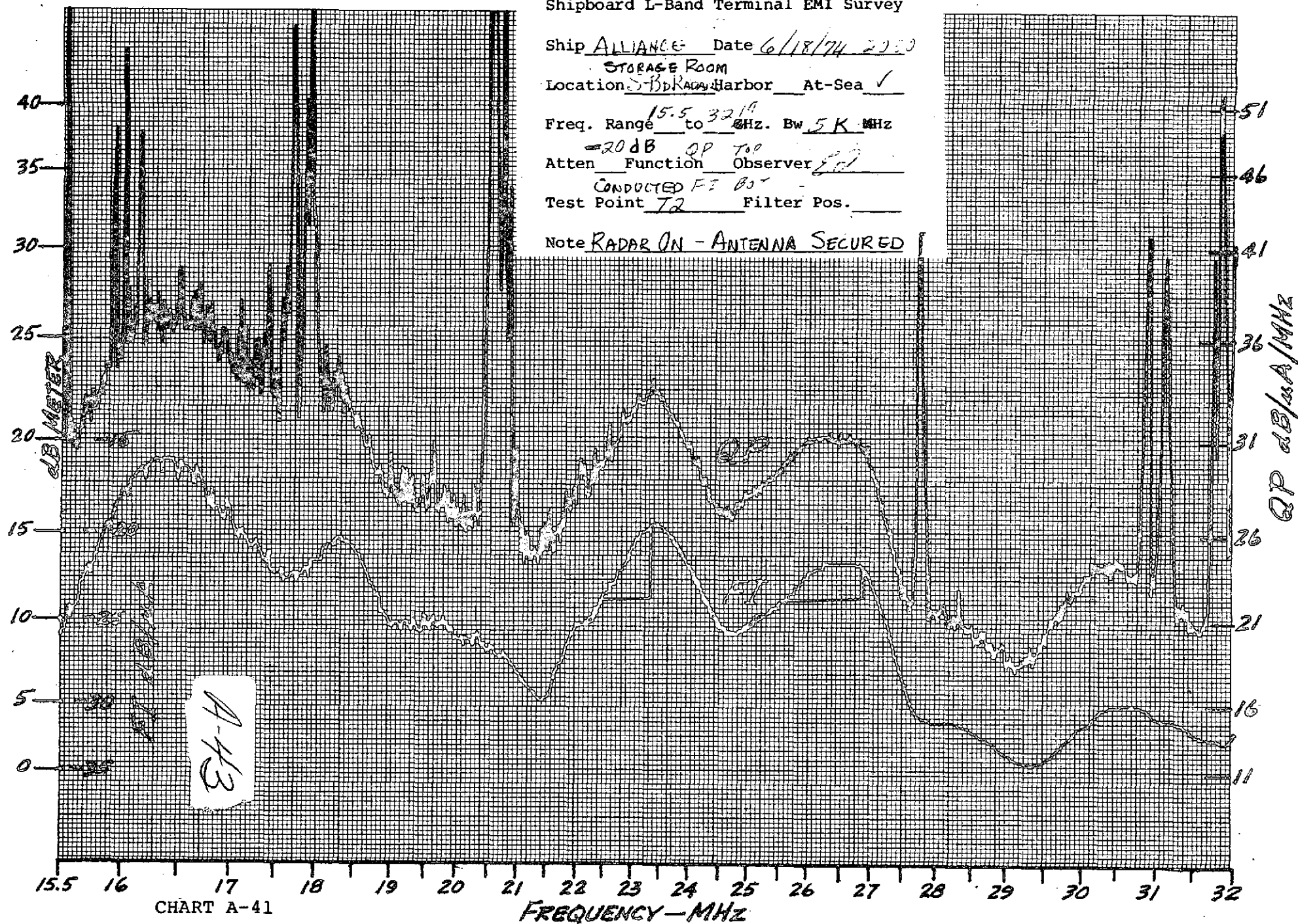
CHART A-38

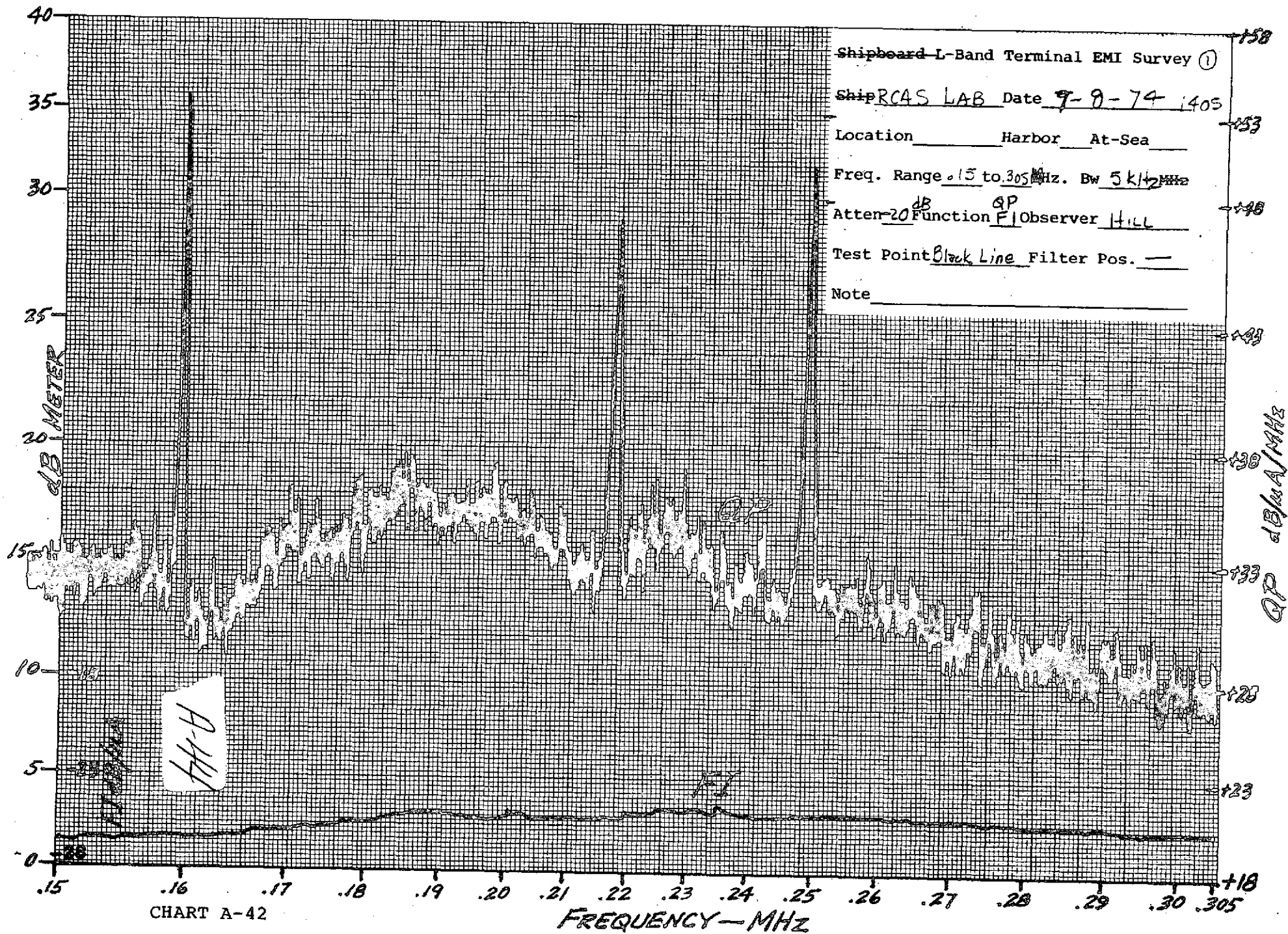
4.1 4.2 4.4 4.6 4.8 5.0 5.2 5.4 5.6 5.8 6.0 6.2 6.4 6.6 6.8 7.0 7.2 7.4 7.6 7.8 8.0 8.2 8.4
FREQUENCY—MHz

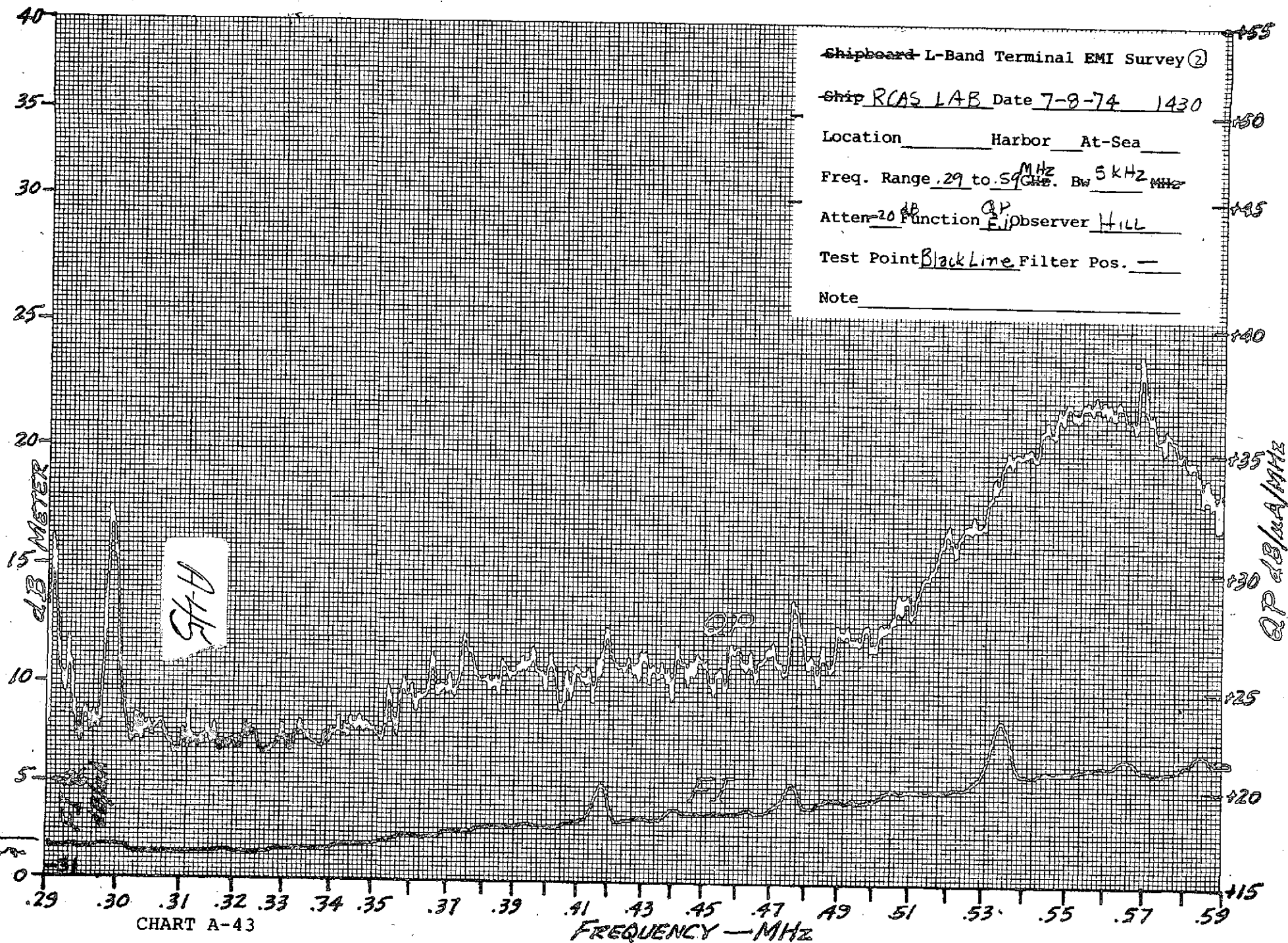




Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 2000Location STORAGE ROOM
BDRADAR Harbor At-Sea ☒Freq. Range 15.5 to 32.15 GHz. Bw 5 K MHzAtten -20 dB OP TOP
Function Observer EDCONDUCTED FE BS
Test Point T2 Filter Pos. Note RADAR ON - ANTENNA SECURED





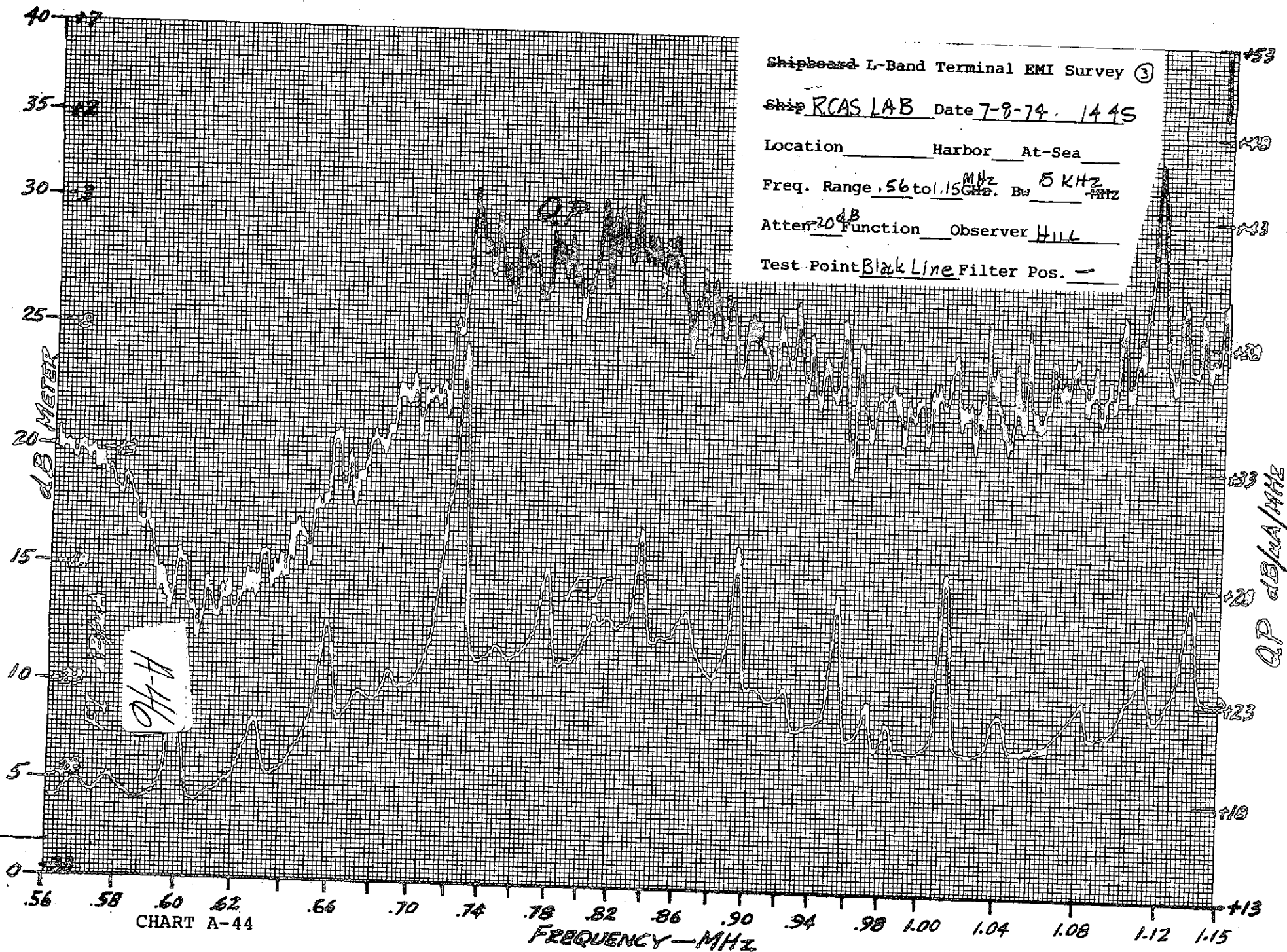
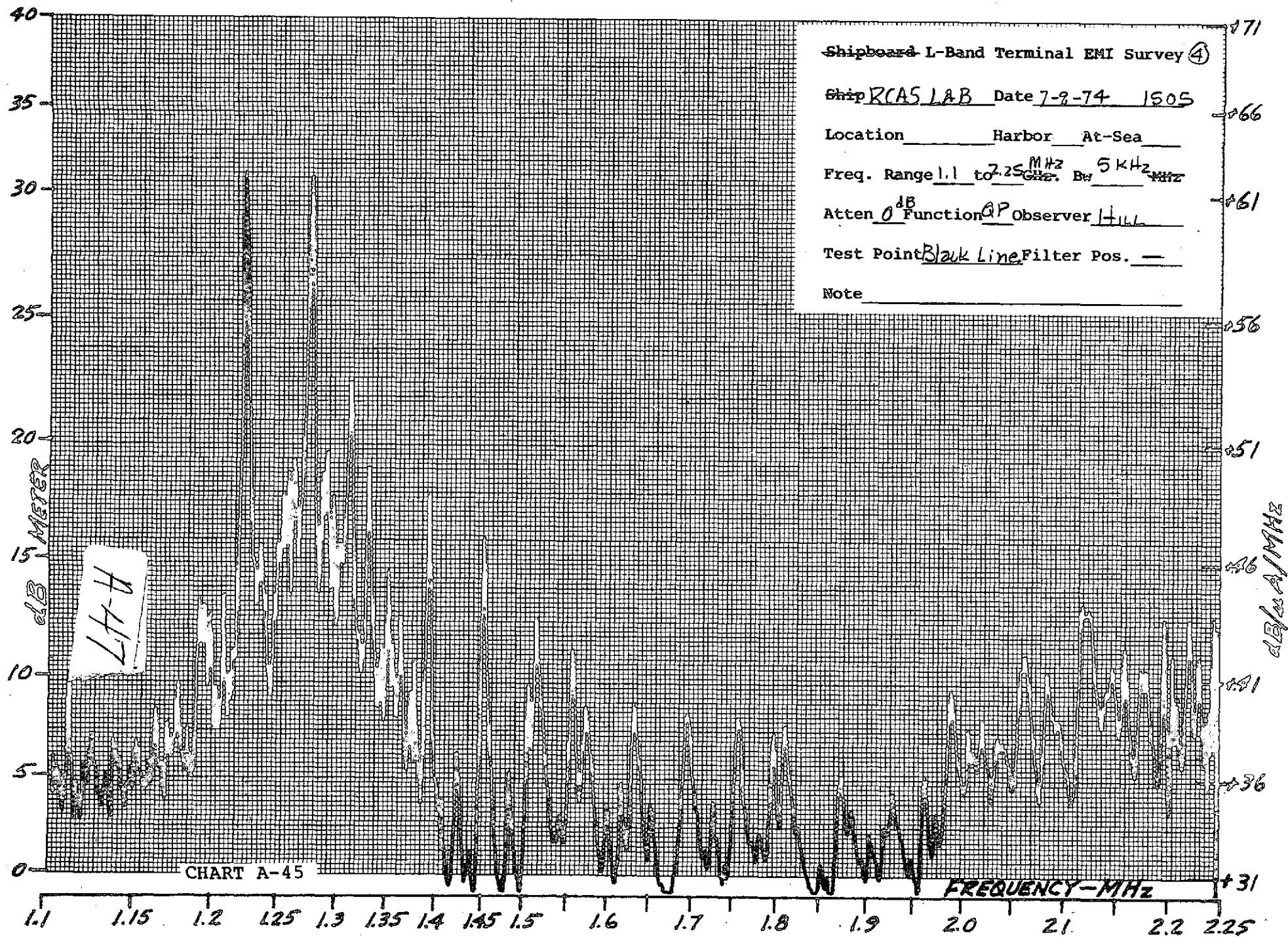
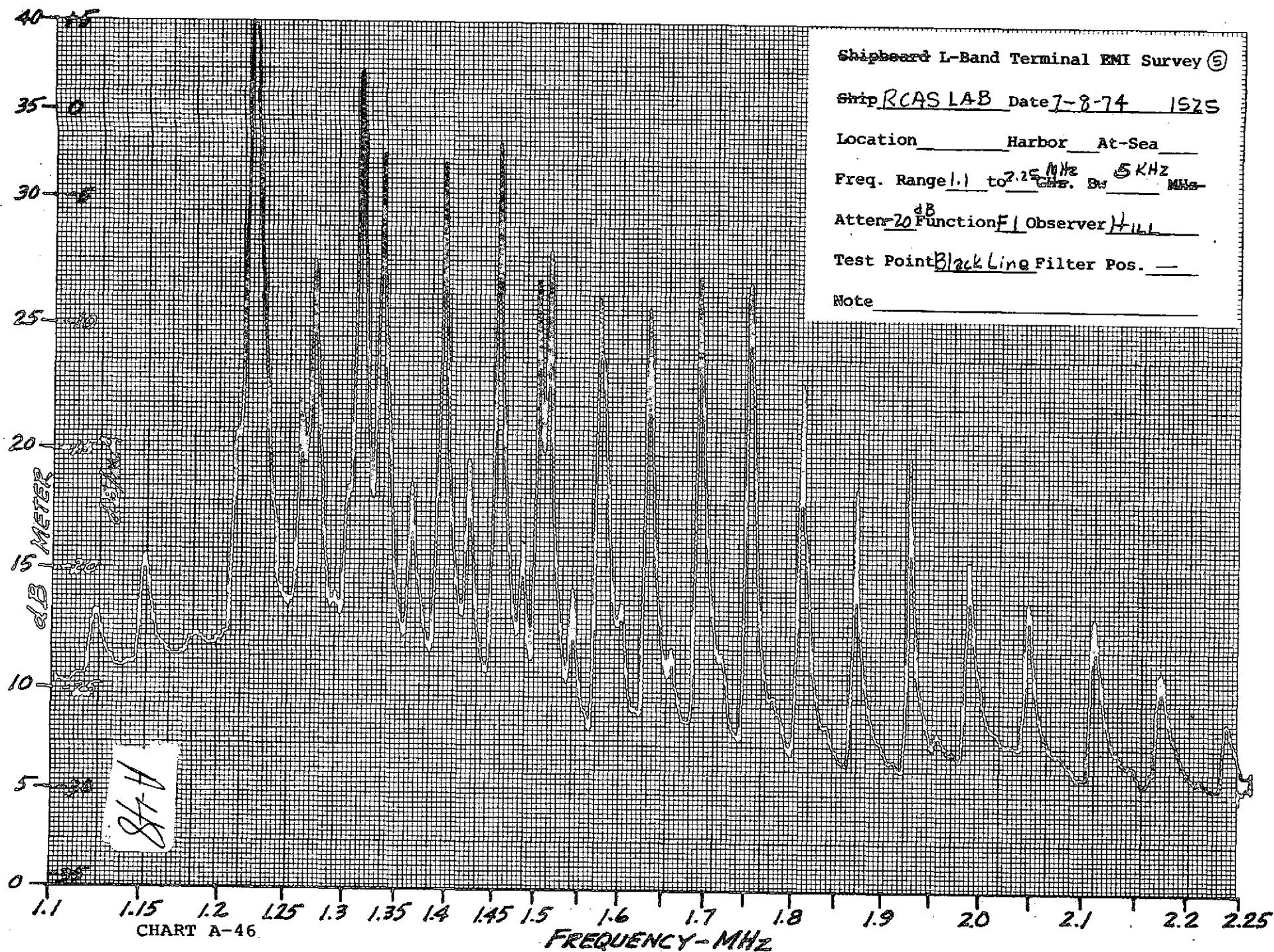
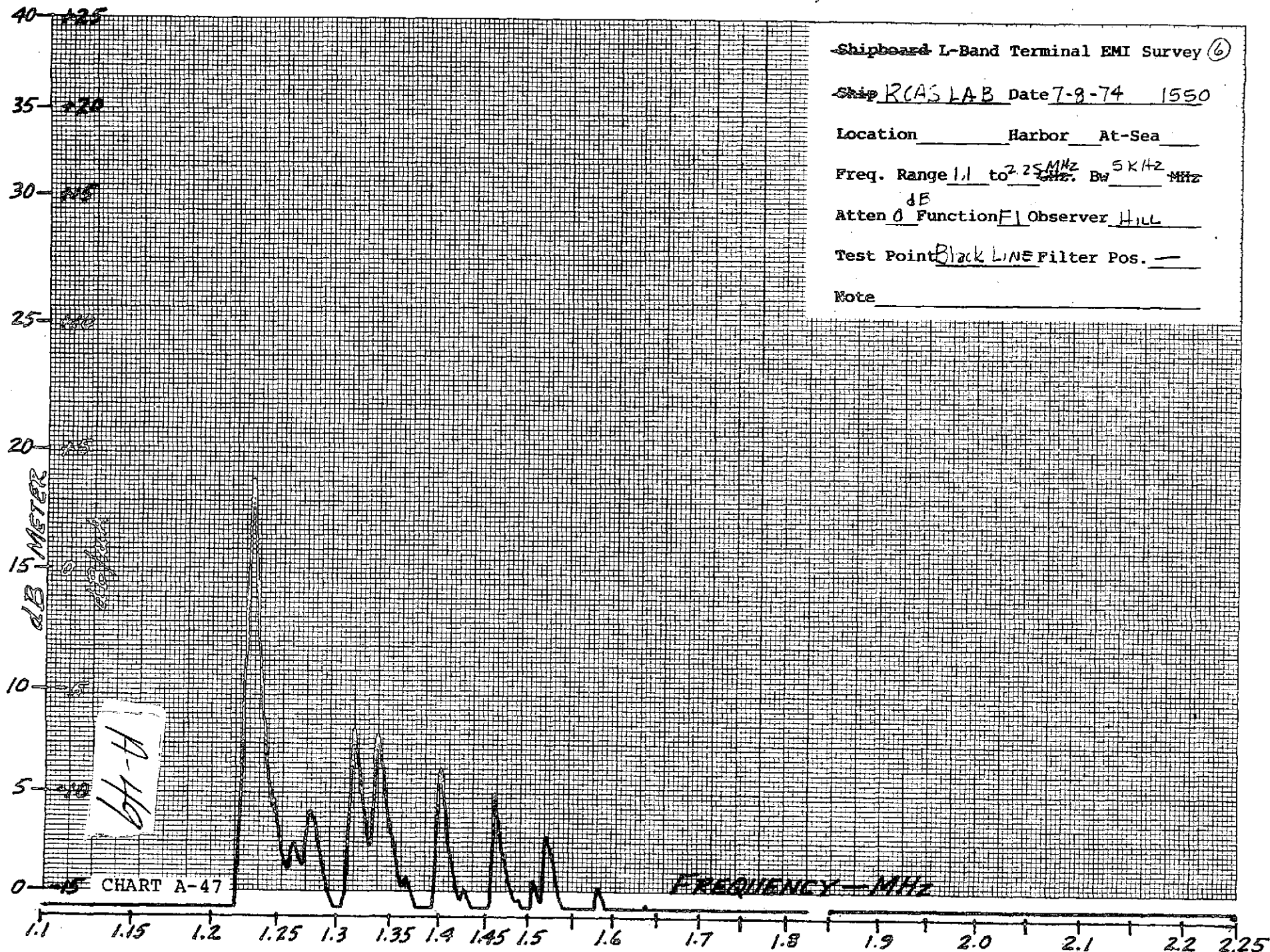
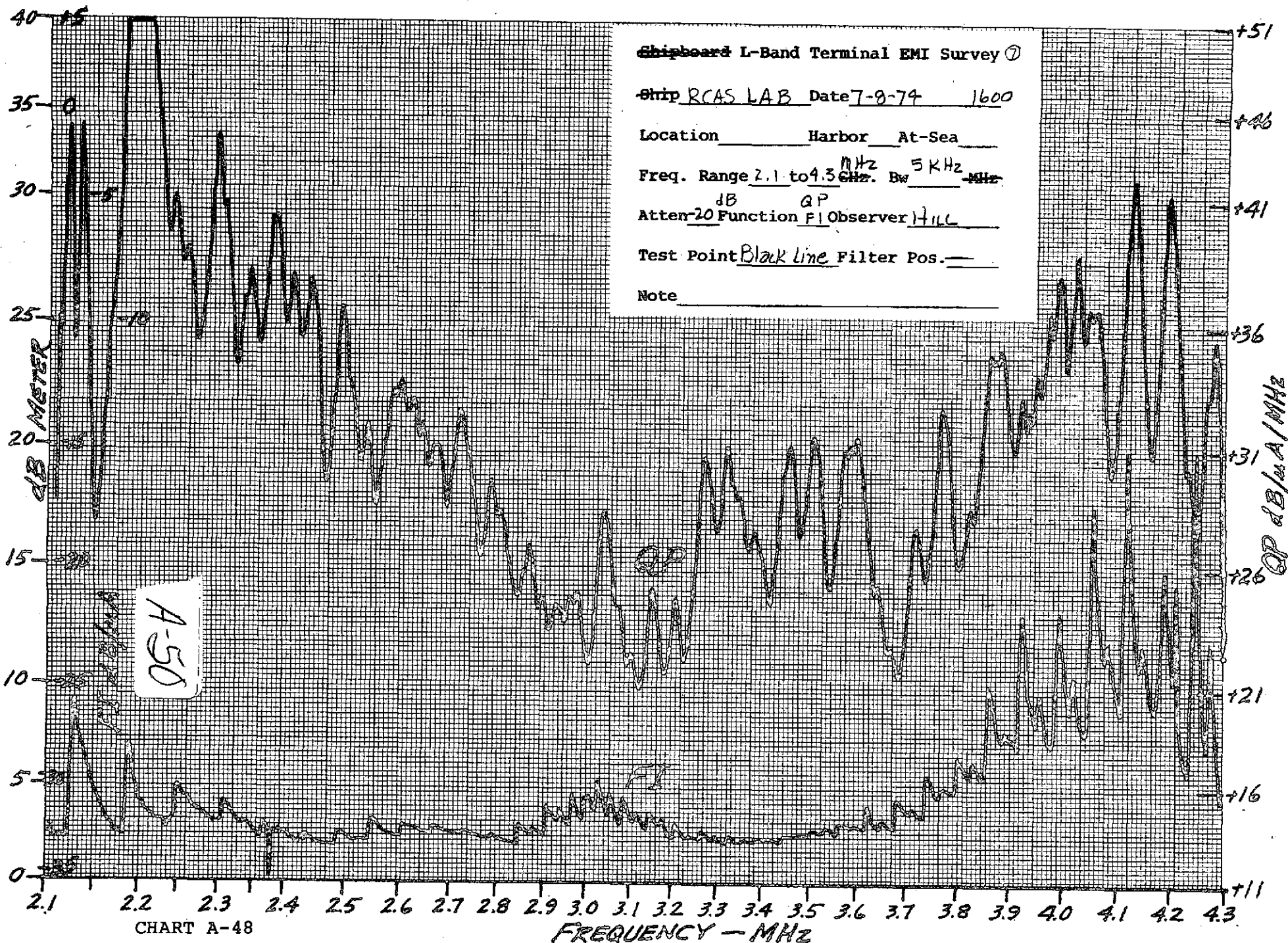


CHART A-44









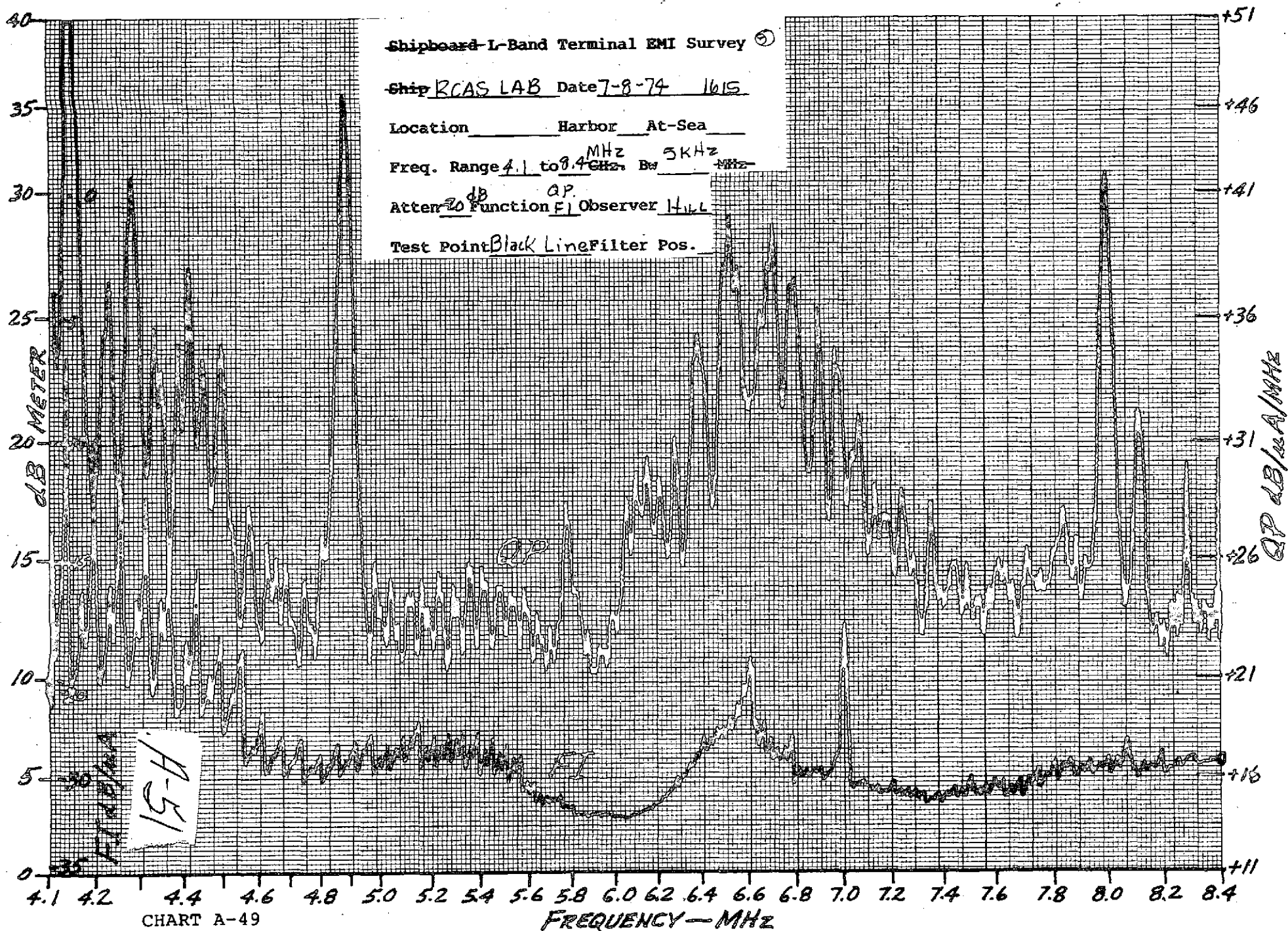
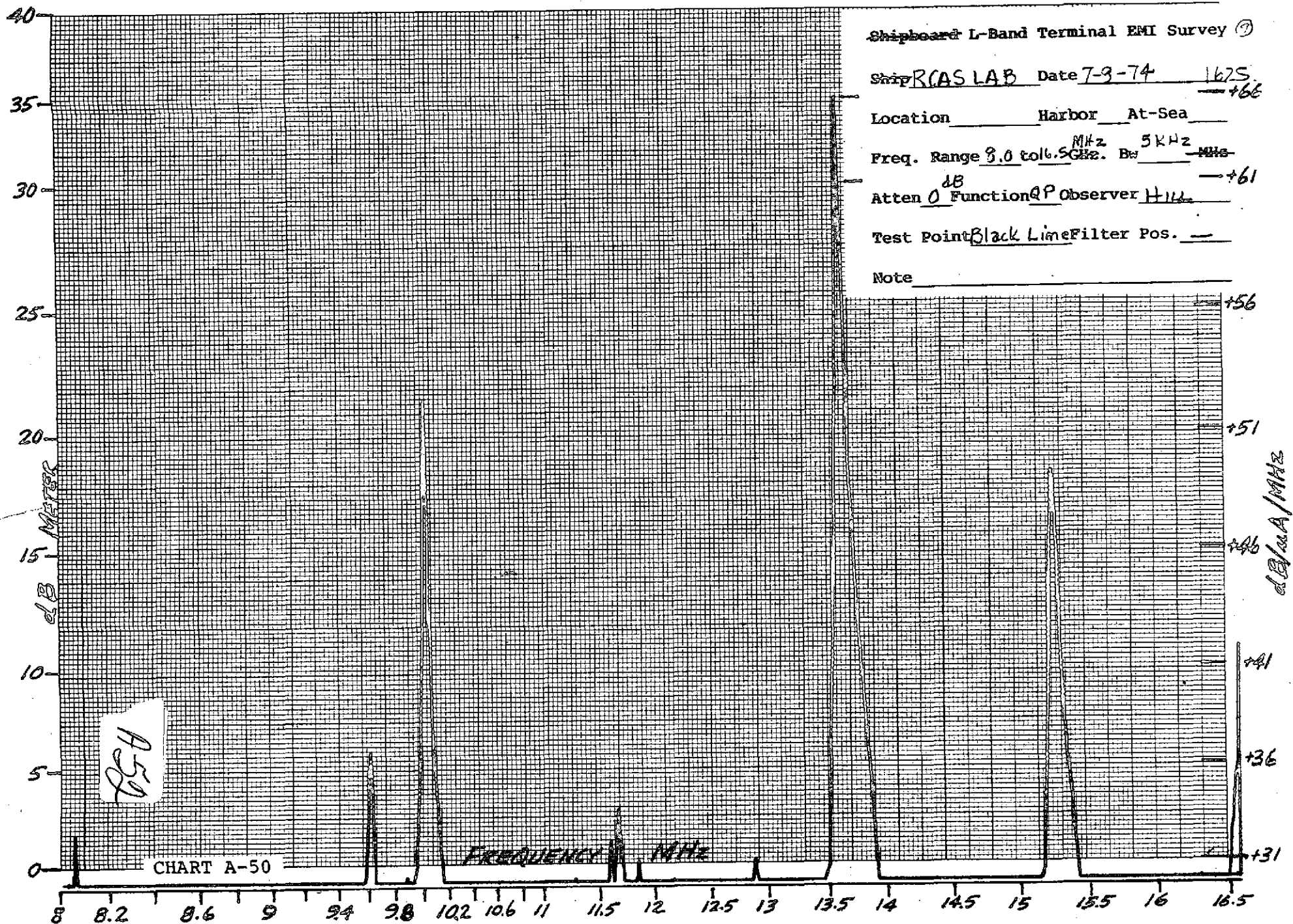
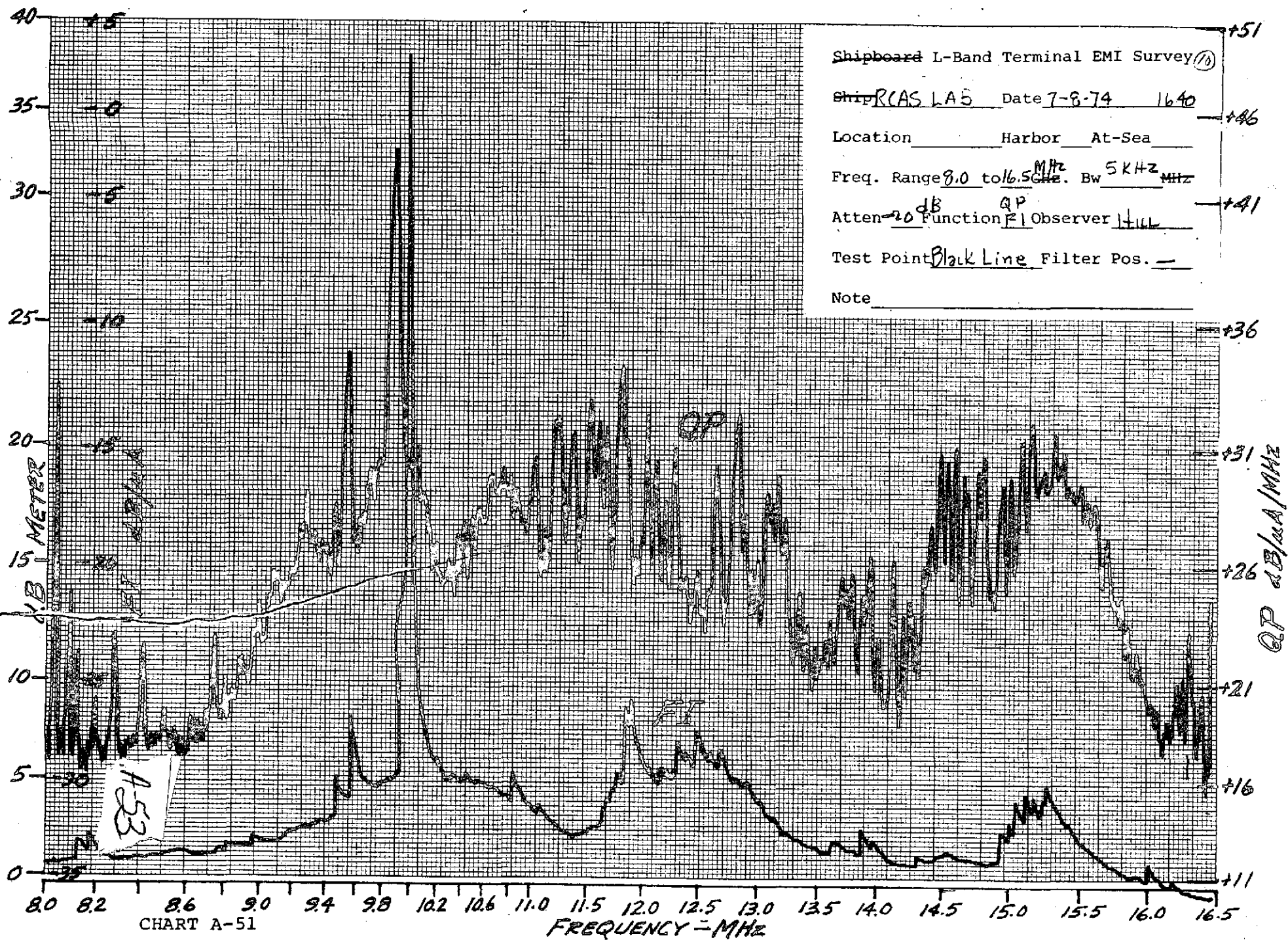
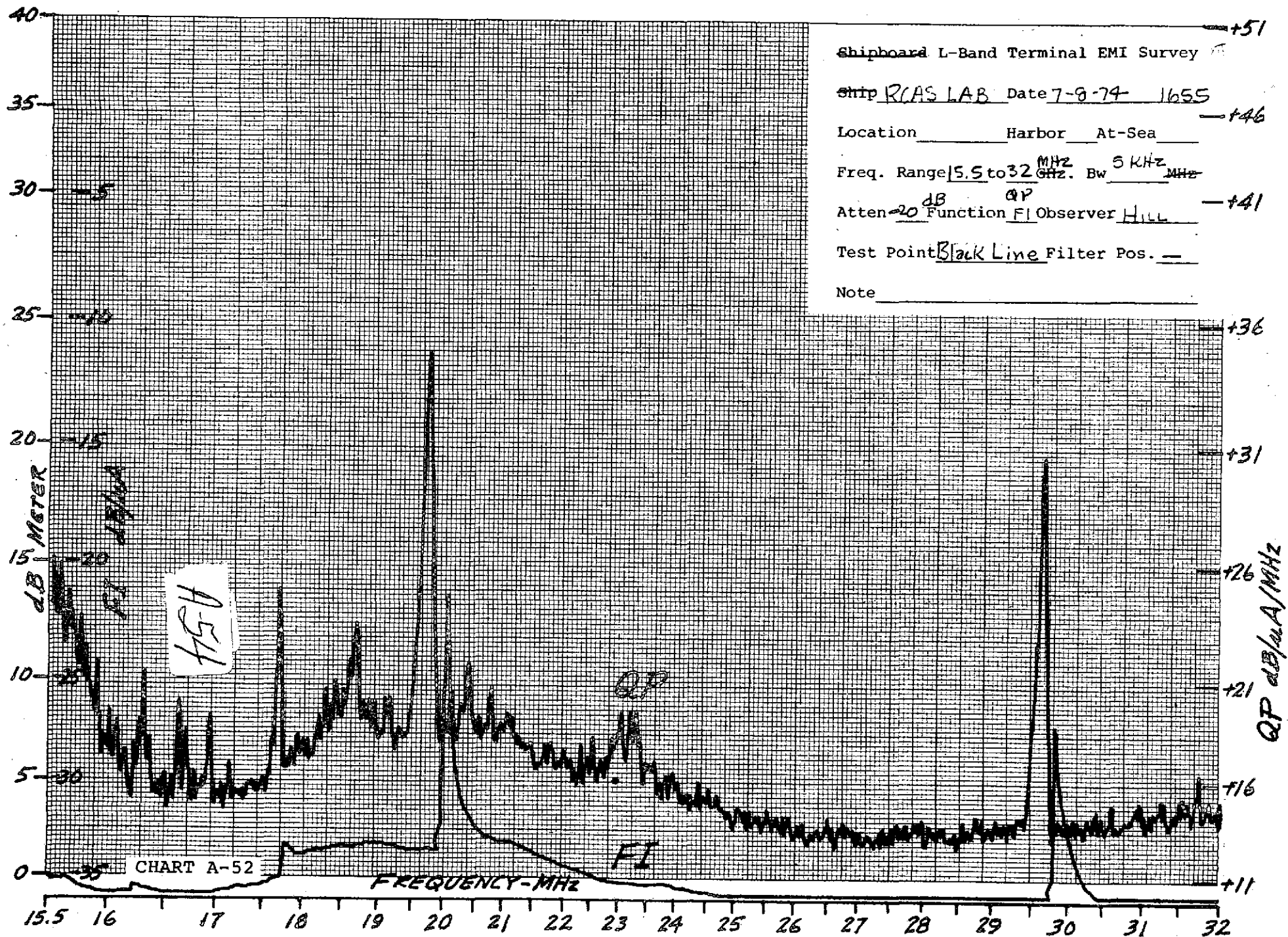
~~Shipboard~~ L-Band Terminal EMI Survey ⑤Ship RCAS LAB Date 7-8-74 1615Location Harbor At-Sea At-SeaFreq. Range 4.1 to 8.4 MHz Bw 5 KHzAtten 20 dB AP
Function F1 Observer HILLTest Point Black Line Filter Pos. AP

CHART A-49

FREQUENCY - MHz







#21101

CALIBRATING ENGINEER: L. WOLF

DATE: 5-26-61

CURRENT PROBE 91550-1

SERIAL NO. 345-131

STODDART AIRCRAFT RADIO CO., INC.

FIGURE 6. CURRENT PROBE
S REFERENCE
TRANSFER IMPEDANCE TO ONE OHM

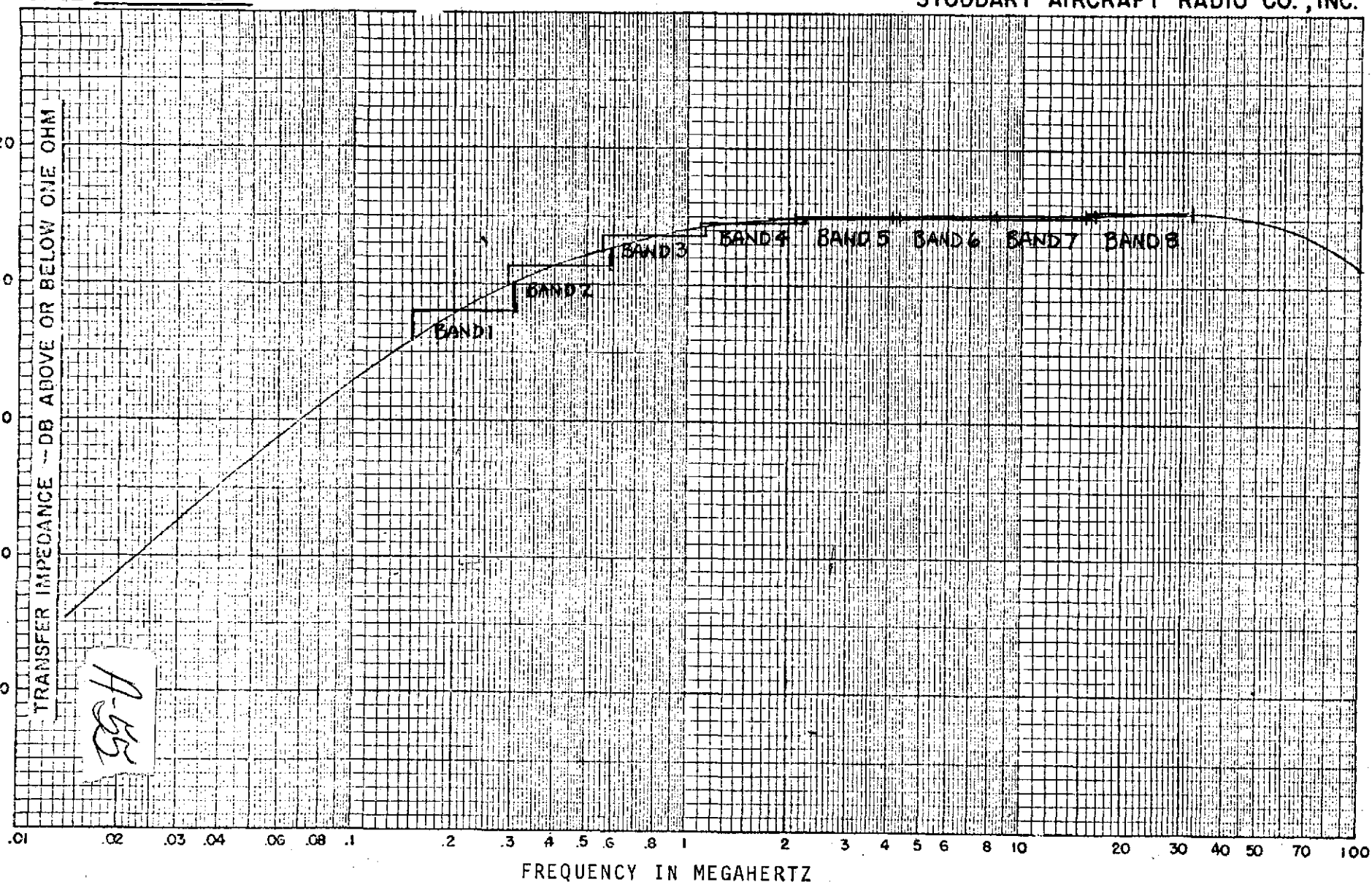


CHART A-53 CURRENT PROBE CALIBRATION

Spectrum Display A-1

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/26/74 1138

Center Freq. 50 MHz, Bandwidth 100 KHz

Scan Width 10 MHz/div, Log Ref Level -30 dBm

S-BAND RADAR POWER LINE

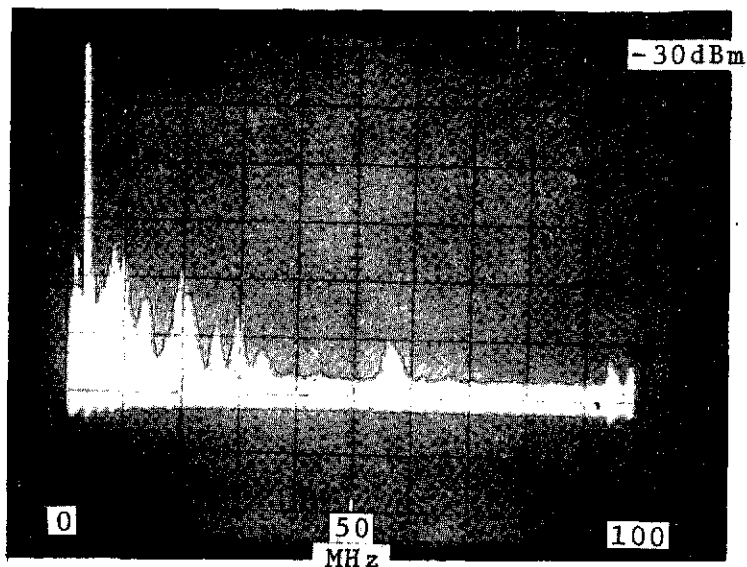
Test Point T2 LINE Filter Pos. —

STORAGE ROOM

Location Harbor SAVANNAH At-Sea —

BOTH RADARS ON

Date — Note — Observer HILL/PAWELL



NOTE: This data must be adjusted for the current probe transfer impedance. See comments on first page of Appendix A. The vertical scale on the spectrum display is 10 dB per major division.

Spectrum Display A-2

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/26/74 1135

Center Freq. 50 MHz, Bandwidth 100 KHz

Scan Width 10 MHz/div, Log Ref Level -30 dBm

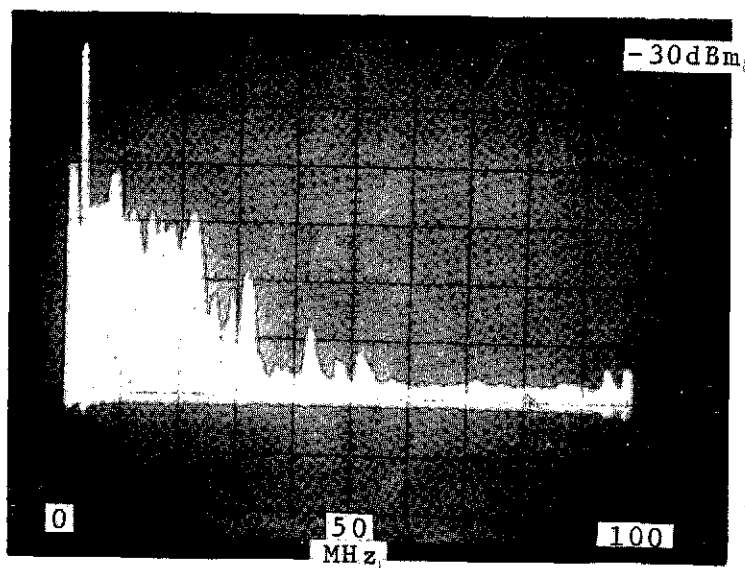
X-BAND RADAR POWER LINE

Test Point BLACK LINE Filter Pos. —

STORAGE ROOM

Location Harbor SAVANNAH At-Sea —

Date — Note BOTH RADARS ON Observer HILL/PAWELL



A-56

Spectrum Display A-3

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/26/74 1140

Center Freq. 70 MHz, Bandwidth 100 KHz

Scan Width 5 MHz/div, Log Ref Level -50dBm

3-BAND RADAR POWER LINE

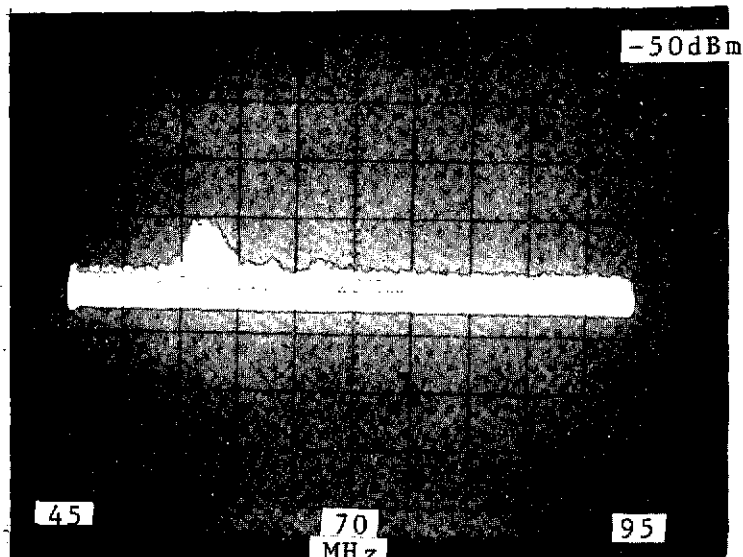
Test Point I2 LINE Filter Pos. ---

STORAGE ROOM

Location Harbor SAVANNAH At-Sea

BOTH RADARS ON

Date --- Note --- Observer HU/PWELL



NOTE: This data must be adjusted for the current probe transfer impedance. See comments on first page of Appendix A. The vertical scale on the spectrum display is 10 dB per major division.

Spectrum Display A-4

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/20/74 1130

Center Freq. 70 MHz, Bandwidth 100 KHz

Scan Width 5 MHz/div, Log Ref Level -50dBm

ON X-BAND RADAR POWER LINE

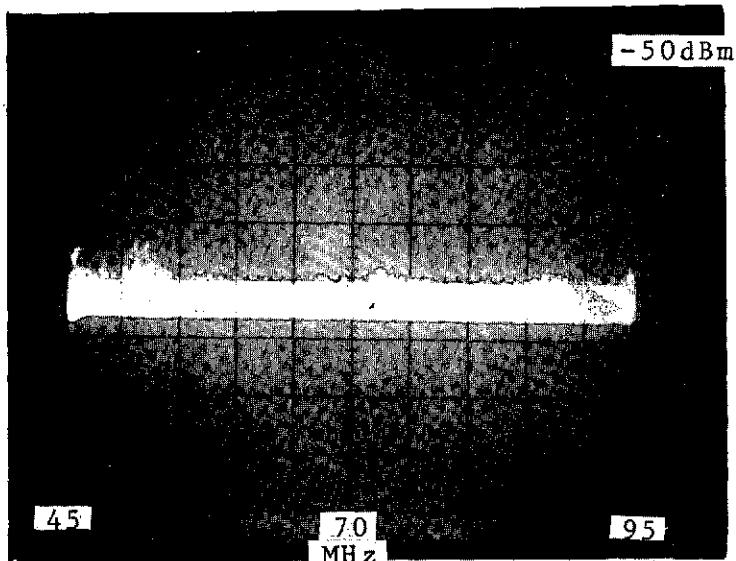
Test Point BLACK LINE Filter Pos. ---

STORAGE ROOM

Location Harbor SAVANNAH At-Sea

BOTH RADARS ON

Date --- Note --- Observer HU/PWELL



A-57

APPENDIX B, FIELD INTENSITY

Chart B-1, Adjustment Factor for Model 1010 Horn
Chart B-2, Adjustment Factor for Log Spiral Conical Antenna
Chart B-3, Radars Off, Out-of-Band, Storage Room LCS
Chart B-4, Radars off, In-Band, Storage Room Horn
Chart B-5, S-Band Radar On, Out-of-Band, Storage Room LCS
Chart B-6, S-Band Radar On, In-Band, Storage Room Horn
Chart B-7, X-Band Radar On, Out-of-Band, Storage Room LCS
Chart B-8, X-Band Radar On, In-Band, Storage Room Horn
Chart B-9, Radars On, Out-of-Band, Storage Room LCS
Chart B-10, Radars On, Out-of-Band, Mast, Aft LCS
Chart B-11, Radars On, Out-of-Band, Mast, Starboard LCS
Chart B-12, Out-of-Band, Bridge Traffic Dish
Chart B-13, Out-of-Band, Dock Area LCS
Chart B-14, Out-of-Band, Downtown Philadelphia LCS
Chart B-15, On-Band, Ben Franklin Bridge Traffic Dish
Chart B-16, Adjustment Factor for HP Spectrum Analyzer
Spectrum Display, B-1, S-Band Radar, Radar Mast
Spectrum Display, B-2, X-Band Radar, Radar Mast

Comments on the Use of These Charts and Spectrum Displays

Charts B-1 and B-2 are calibration charts giving the adjustment factors for the horn antenna or the log-spiral conical antenna with various connecting cables as used in taking the data recorded on Charts B-3 through B-11 and B-13 and B-14. Charts B-12 and B-15 were made using the 1.2 meter diameter L-band Dish Antenna and are for comparative information

APPENDIX B, Continued

only because the dish antenna has only been calibrated in the maritime satellite L-band.

On each chart the ordinate scale on the left represents the instrument meter scale in dB/ μ v. To this must be added the proper attenuator setting of 0 dB or 20 dB as noted on the chart label. However, this is not true dB/ μ v because the NM-65T can only be calibrated at one frequency when the data is taken with an X-Y recorder. Because of gain variation with frequency, an adjustment must be made which is a function of frequency. This adjustment in addition to antenna factor, cable loss, and bandwidth adjustments are incorporated in Charts B-1 and B-2.

Example of use of Chart B-1

Chart B-1 is intended for use with Charts B-4, B-6, and B-8 which involve the model 1010 horn antenna for "in-band" measurements from 1.3 to 1.9 GHz. As an example of the use of Chart B-1 to convert values shown on the charts to broadband field intensity (from the DP trace) in dB/ μ v/m/MHz, read Chart B-6 at 1.6 GHz.

Meter reading	49.5 dB/ μ v
Attenuator reading	<u>20.0 dB</u>
	69.5 dB/ μ v
DP Antenna Factor (from Chart B-1)	<u>8.0</u>
Broadband field intensity	77.5 dB/ μ v/m/MHz

APPENDIX B, Continued

Example of use of Chart B-2

Chart B-2 is intended for use with Charts B-3, B-5, B-7, B-9, B-10, B-11, B-13, and B-14 which involve the use of the log-spiral conical antenna for measurements in the frequency range of 1.0 to 10 GHz. The upper curve is for the log-spiral conical antenna with a 15 meter length of RG-214/U cable. The lower curve is for the log-spiral conical antenna with either the 3 meter length of RG-9/U cable or the 12 meter length of Foam Wellflex cable.

As an example of the use of Chart B-2 to convert values from the FI trace shown on the charts to narrowband field intensity in dB/ μ V/m read Chart B-9 at 1.15 GHz.

Meter reading	8 dB/ μ V
Attenuator reading	<u>0 dB</u>
	8 dB/ μ V
F.I. Factor from Chart B-2	<u>30 dB/m</u>
	38 dB/ μ V/m

To convert values from the DP trace on the charts to broadband field intensity in dB/ μ V/m/MHz read Chart B-10 at 5.1 GHz.

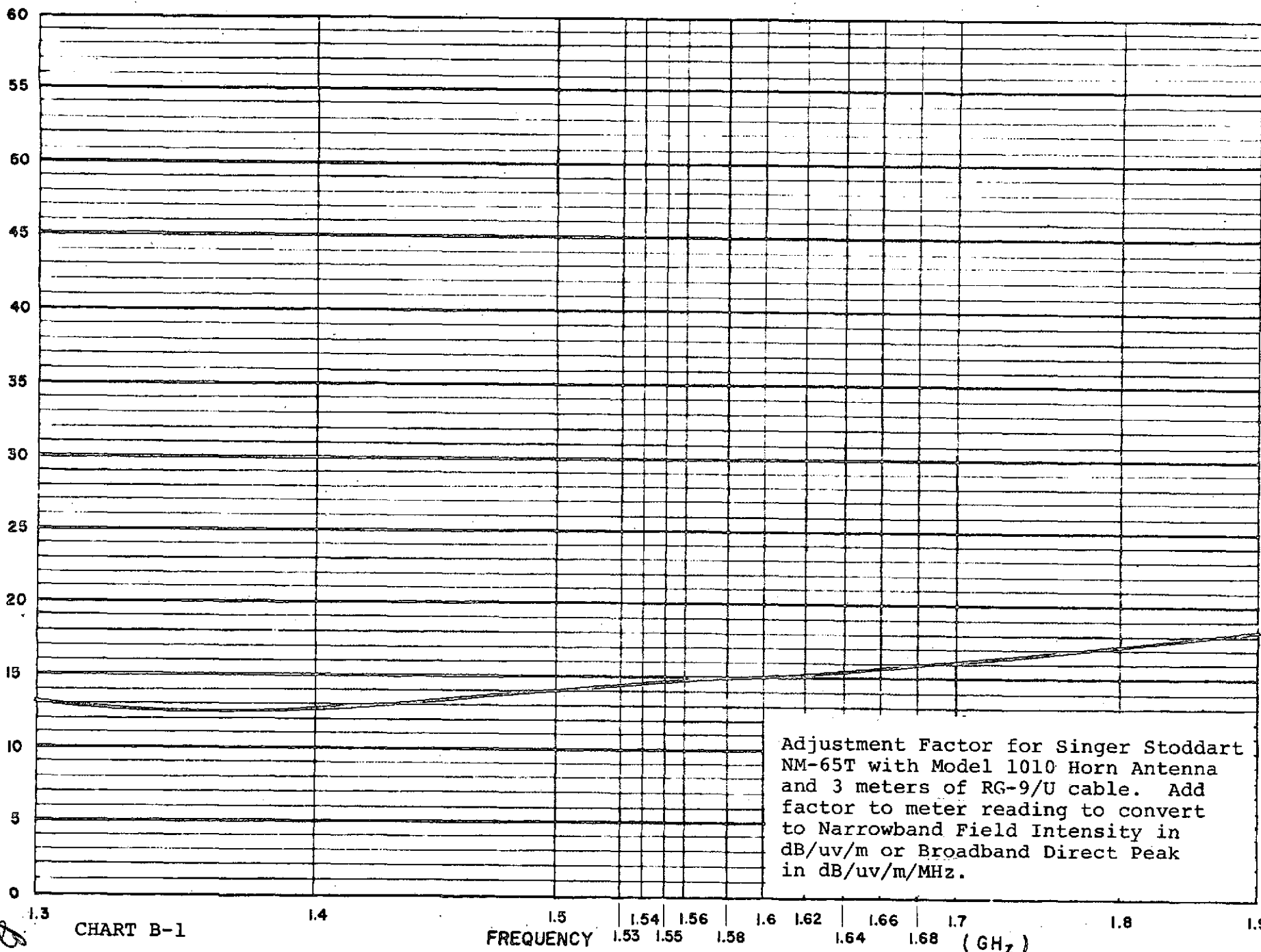
Meter reading	42 dB/ μ V
Attenuator reading	<u>0 dB</u>
	42 dB/ μ V
DP Antenna Factor from Chart B-2	<u>44 dB/m/MHz</u>
	86 dB/ μ V/m/MHz

APPENDIX B, Continued

Data Conversion from Spectrum Display

The spectrum analyzer data as read out on the spectrum display photographs must be adjusted for antenna factor and cable loss, and normalized for bandwidth. This is accomplished with the use of Chart B-16 which incorporates these adjustments as well as the conversion from dBm to dB/ μ v. Simply find the adjustment factor on Chart B-16 for the frequency of interest and add this to the signal value taken from the spectrum display photograph

FIELD INTENSITY ANTENNA FACTOR FOR dB/uv/m



DIRECT PEAK ANTENNA FACTOR FOR dB/uv/m/MHz

Adjustment Factor for Singer Stoddart NM-65T with Model 1010 Horn Antenna and 3 meters of RG-9/U cable. Add factor to meter reading to convert to Narrowband Field Intensity in dB/uv/m or Broadband Direct Peak in dB/uv/m/MHz.

CHART B-1

FREQUENCY

(GHz)

FIELD INTENSITY ANTENNA FACTOR FOR dB/uv/m

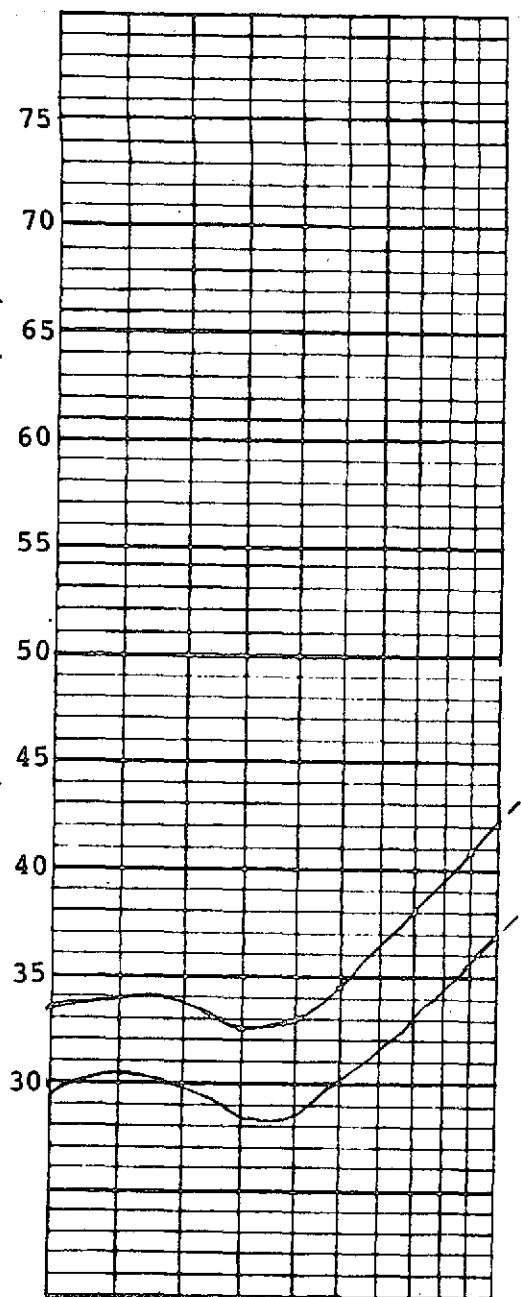


CHART B-2

15m RG-214/U Cable

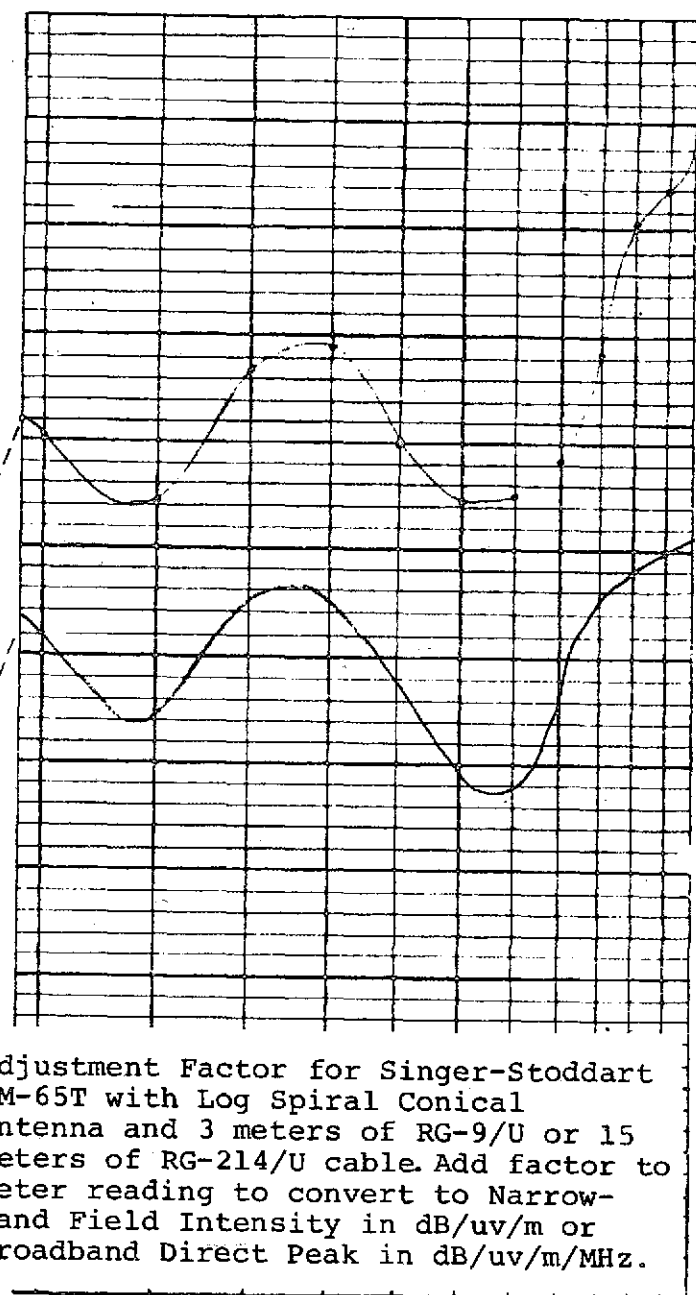
3m RG-9/U Cable

12m Foam Wellflex Cable

FREQUENCY (GHz)

Adjustment Factor for Singer-Stoddart NM-65T with Log Spiral Conical Antenna and 3 meters of RG-9/U or 15 meters of RG-214/U cable. Add factor to meter reading to convert to Narrowband Field Intensity in dB/uv/m or Broadband Direct Peak in dB/uv/m/MHz.

DIRECT PEAK ANTENNA FACTOR FOR dB/uv/m/MHz



9-9

dB/uv

60

55

50

45

40

35

30

25

20

15

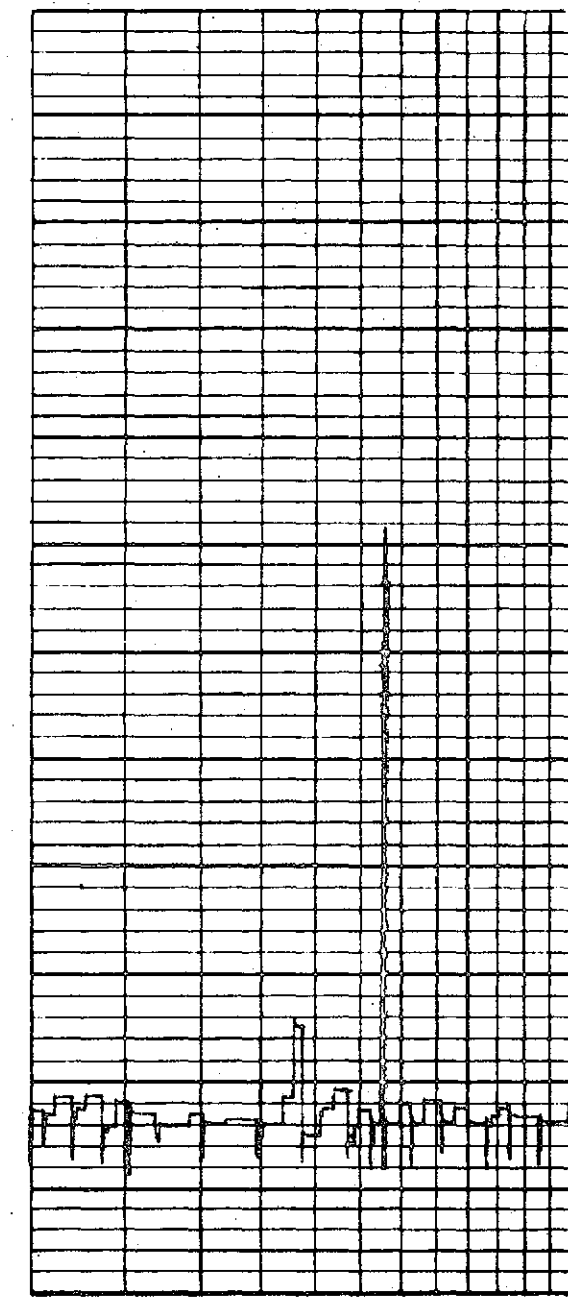
10

5

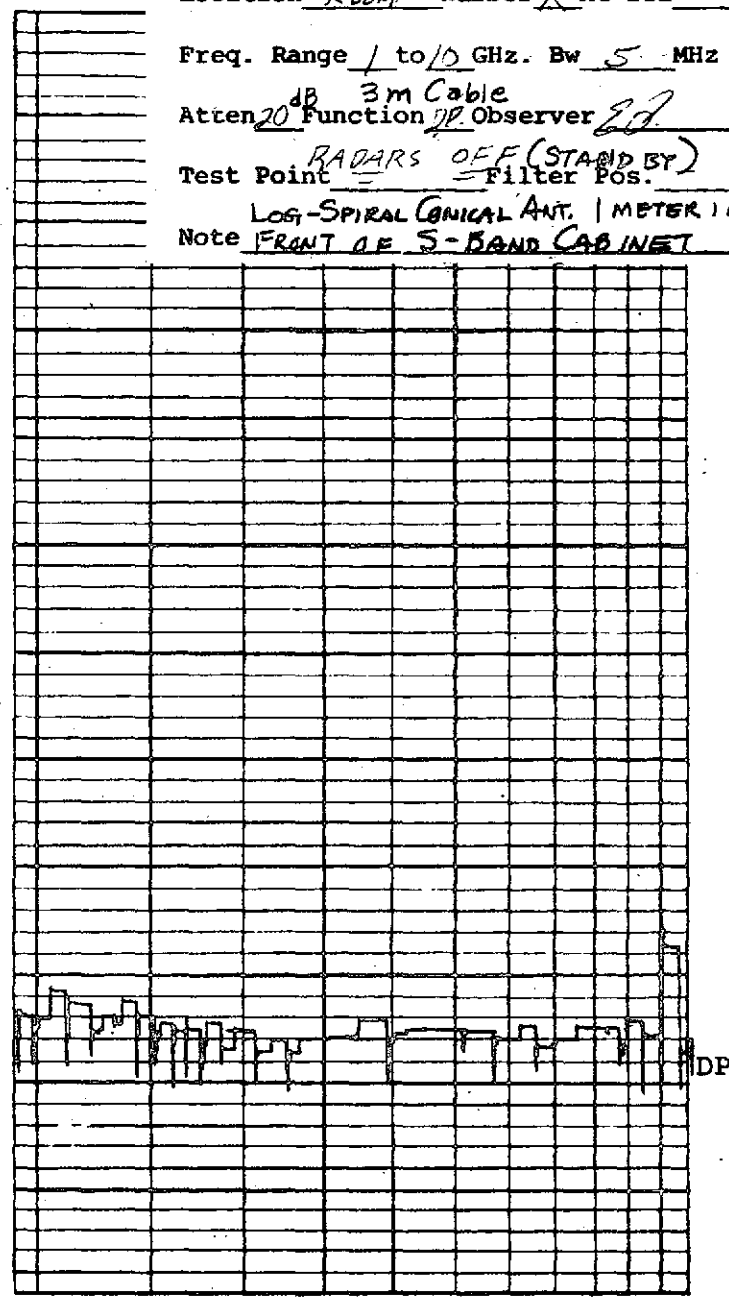
0



CHART B-3



FREQUENCY (GHz)

Ship AM. ALLIANCE Date 6/13/74 1220Location STORAGE ROOM Harbor PT. ELIZABETH At-Sea XFreq. Range 1 to 10 GHz. Bw 5 MHzAtten 20 dB 3m Cable Function DP Observer EDTest Point RADARS OFF (STAND BY) Filter Pos. Filter Pos.Note LOG-SPIRAL CONICAL ANT. 1 METER IN FRONT OF S-BAND CABINET

DP

dB/uv

60

55

50

45

40

35

30

25

20

15

10

5

0

Shipboard L-Band Terminal EMI Survey

Ship AM. ALLIANCE Date 6/10/94 12

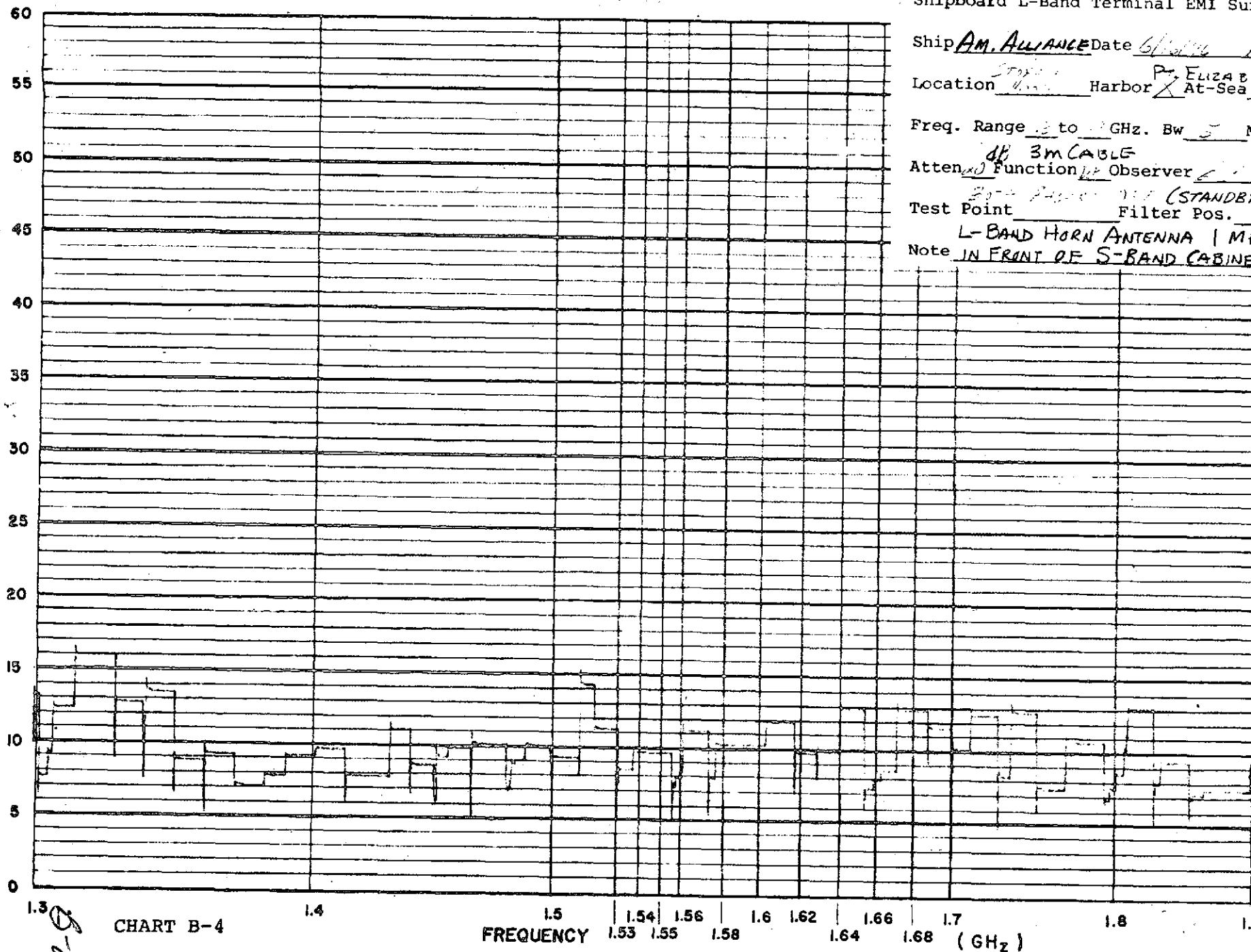
Location ST. JOHN'S Harbor X ELIZABETH At-Sea

Freq. Range 1.3 to 1.9 GHz. Bw 5 MHz

Atten 40 dB 3m CABLE Function LF Observer CE

Test Point 20-4 PHASE 117 (STANDBY) Filter Pos.

L-BAND HORN ANTENNA 1 METER
Note IN FRONT OF S-BAND CABINET



DP

dB/uv

60

55

50

45

40

35

30

25

20

15

10

5

0

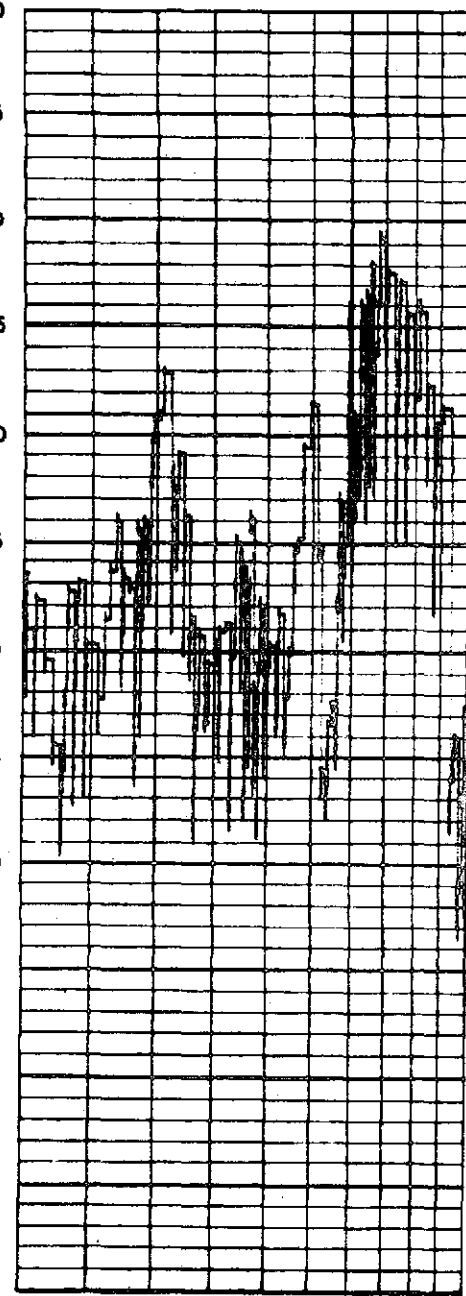
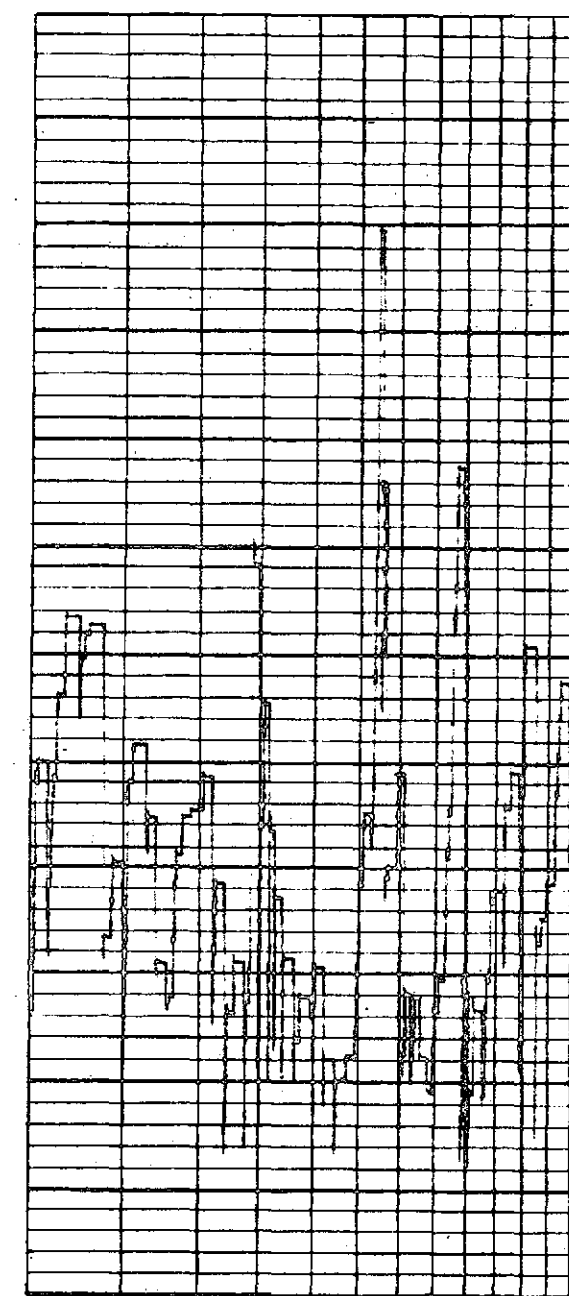
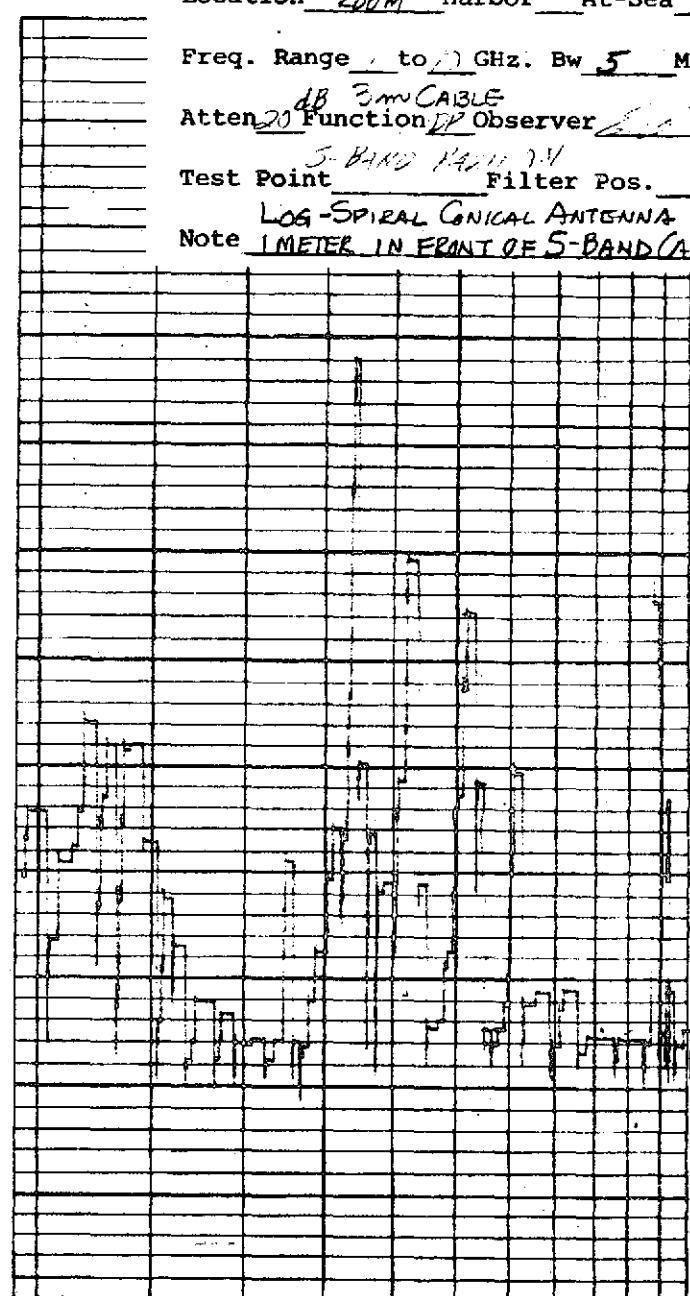


CHART B-5



FREQUENCY (GHz)



DP

Ship AM. F. LIAISON Date 2. 5. 61

Location STRAKE Harbor Pt. ELIZABETH
EDM At-Sea

Freq. Range to 20 GHz. Bw 5 MHz

Atten dB 3m CABLE Function DP Observer [Signature]

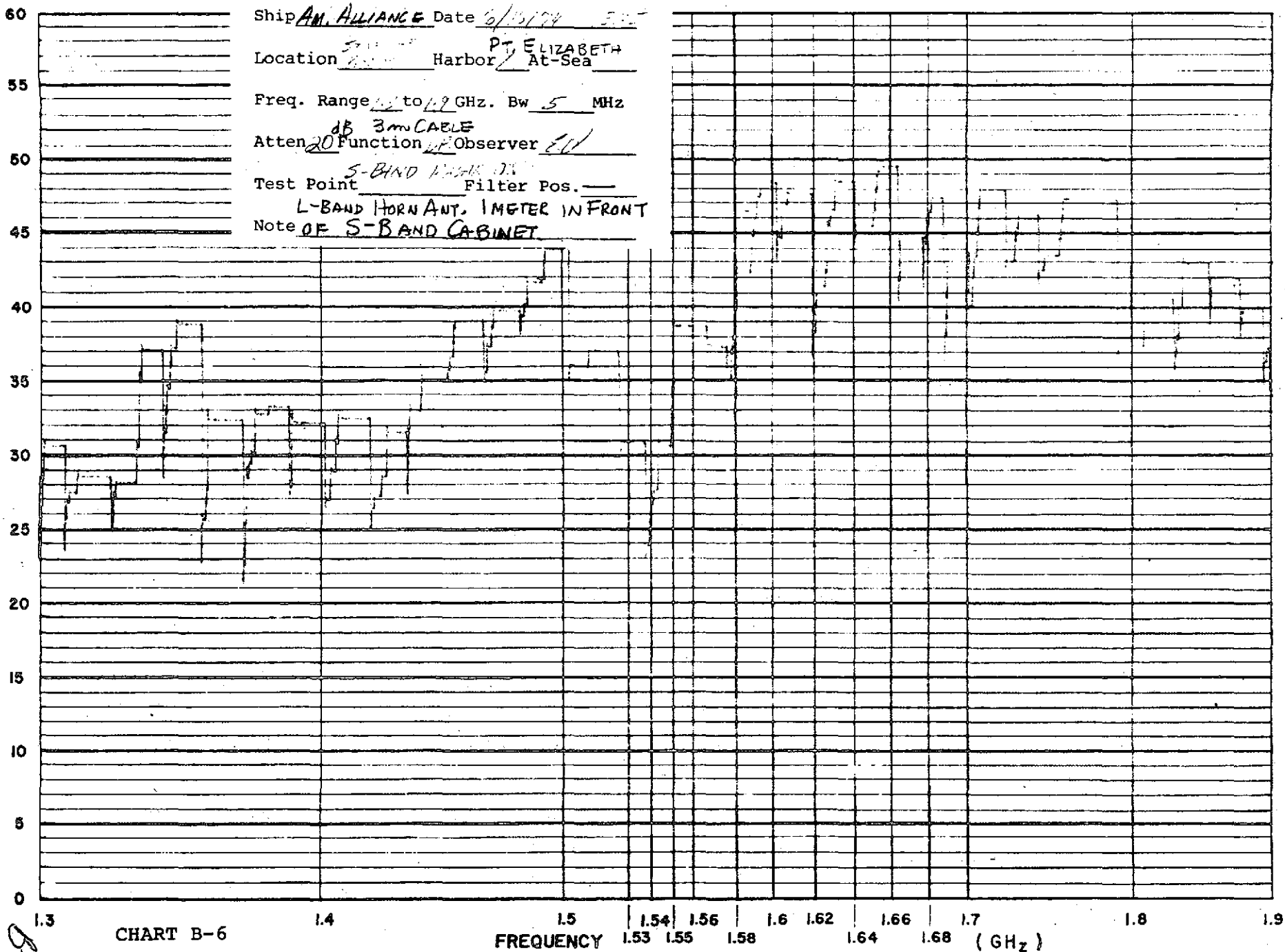
Test Point S-BAND 14211 JV Filter Pos. [Blank]

Note LOG-SPIRAL CONICAL ANTENNA
1 METER IN FRONT OF S-BAND CABINET

dB/uv

3 Shipboard L-Band Terminal EMI Survey

Ship AM. ALLIANCE Date 6/10/74 500
Location 500 Harbor PT. ELIZABETH At-Sea
Freq. Range 1.3 to 1.9 GHz. Bw 5 MHz
Atten dB 3m CABLE Function LF Observer EW
Test Point 5-BAND HORN ANT. Filter Pos. —
Note L-BAND HORN ANT. 1 METER IN FRONT
OF 5-BAND CABINET



dB/uv

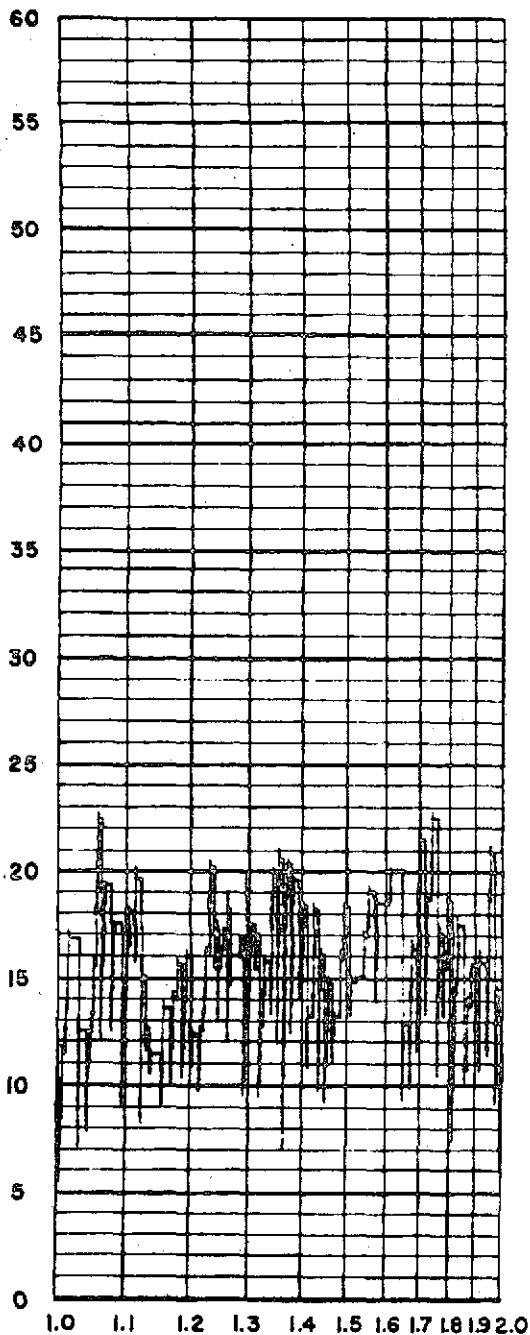
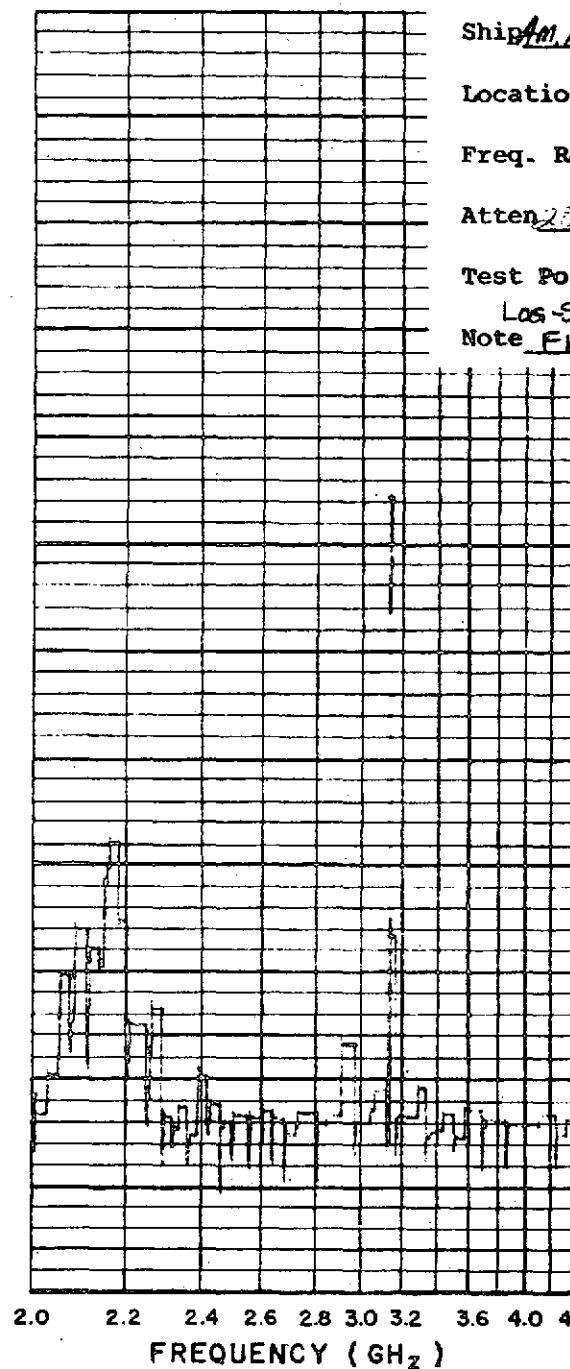


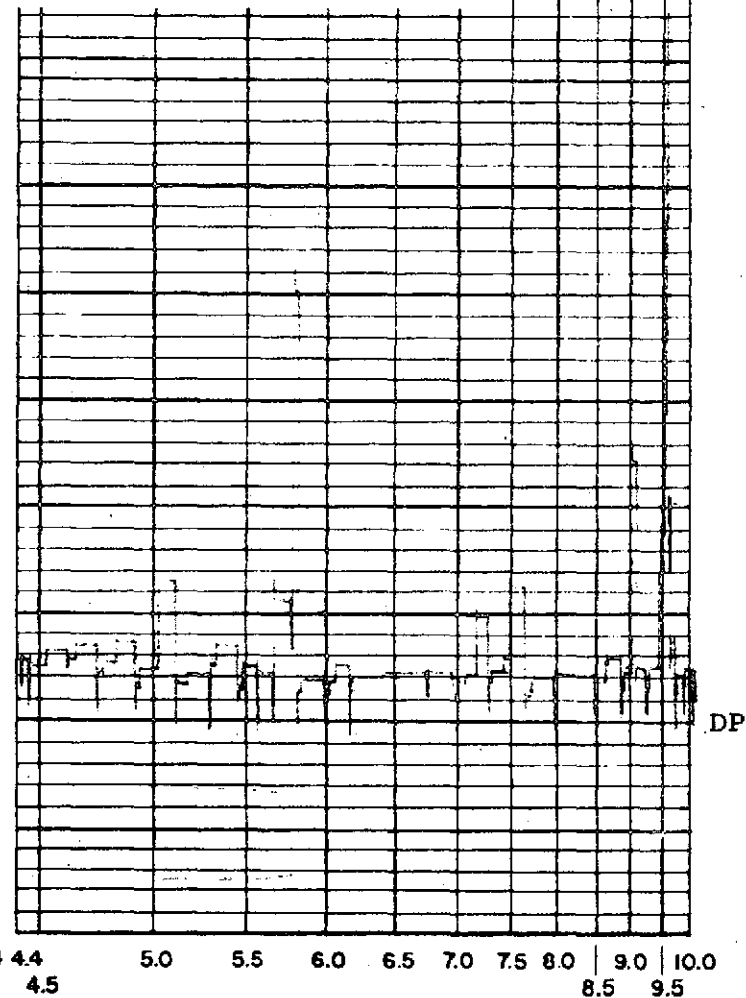
CHART B-7

B-11



Shipboard L-Band Terminal EMI Survey

Ship AM. ALLIANCE Date 6/1/73
 Location Harbor PT. ELIZABETH
 Harbor X At-Sea
 Freq. Range 1 to 10 GHz. Bw 5 MHz
 Atten 20 dB 3M CABLE Function OFF Observer JLB
 Test Point 1-5-10 Filter Pos. 30
 Note LOG SPIRAL CONICAL ANT. 1 METER IN FRONT OF X-BAND CABINET



DP

dB/uv

Shipboard L-Band Terminal EMI Survey

Ship AM. ALLIANCE Date 1/12

Location PT. ELIZABETH Harbor At-Sea

Freq. Range 1.3 to 1.9 GHz. Bw 5 MHz

Atten 0 dB 3m CABLE Function LINE Observer DP

Test Point X-BAND HORN ANT. 1METER IN FRONT Filter Pos. OF X-BAND CABINET

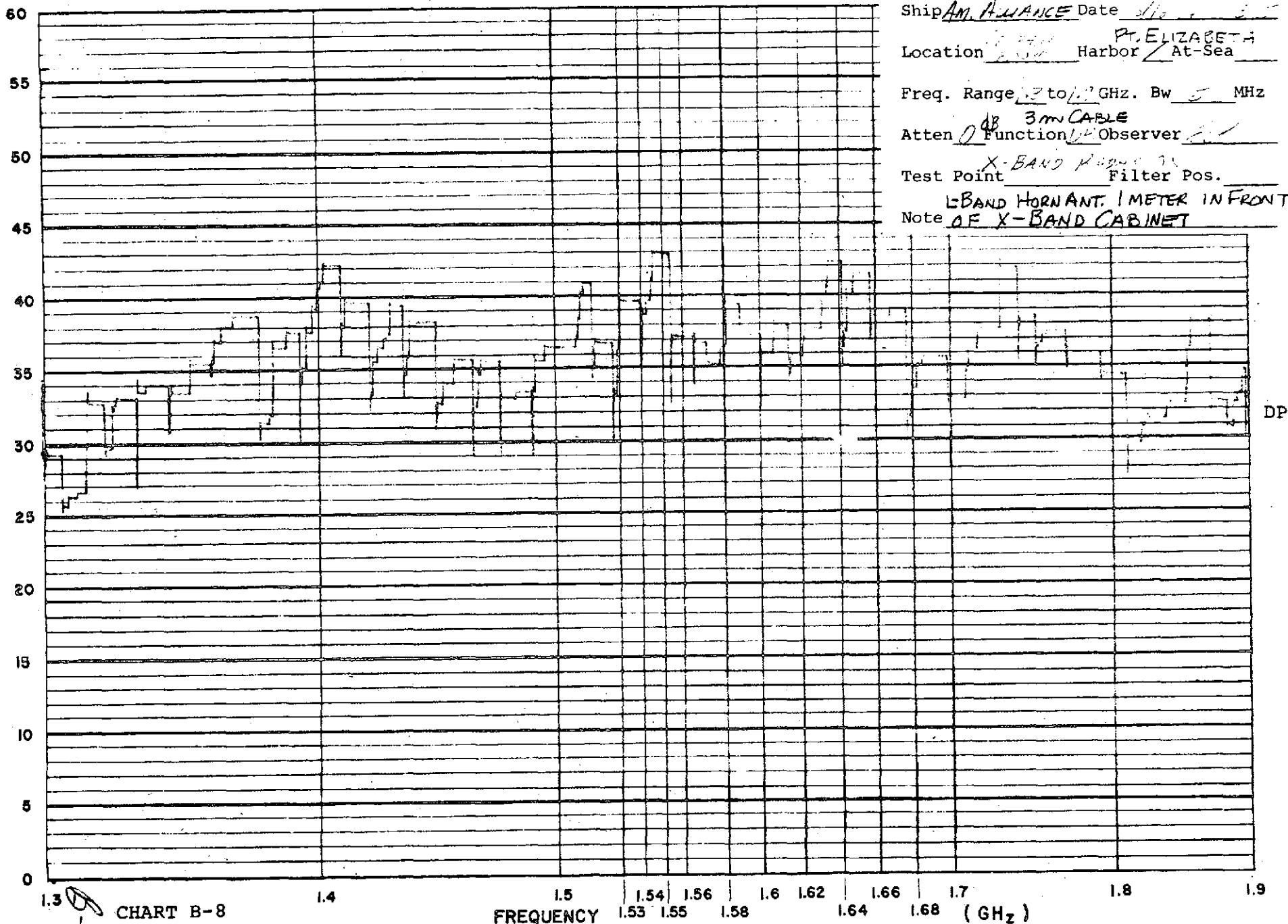


CHART B-8

FREQUENCY (GHz)

103 dB/uv
dB/uv

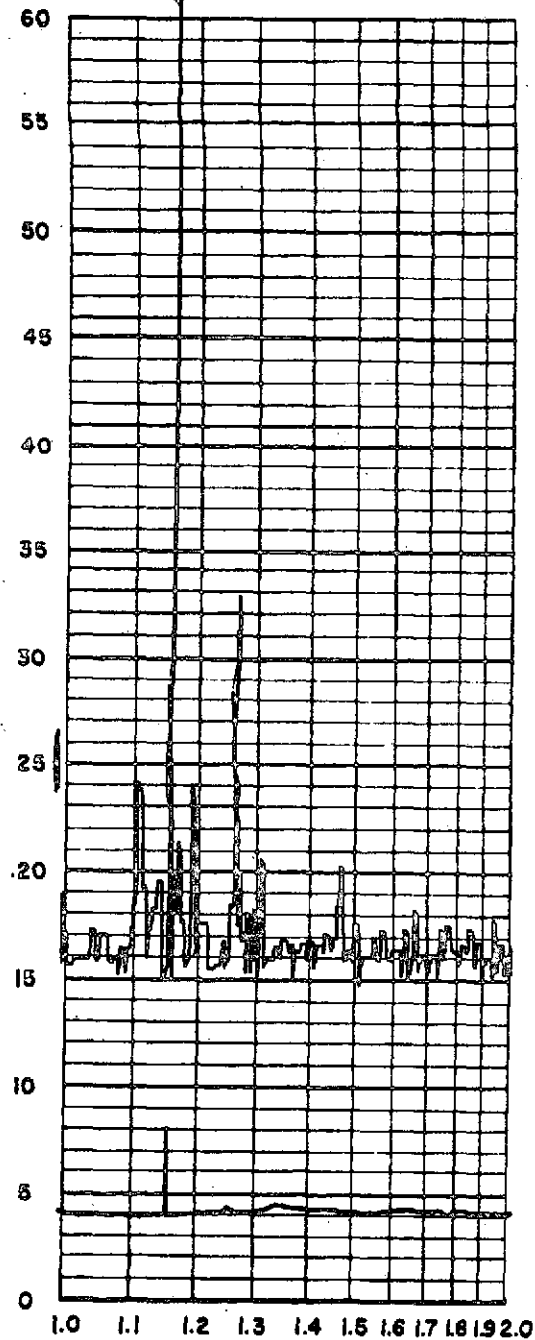
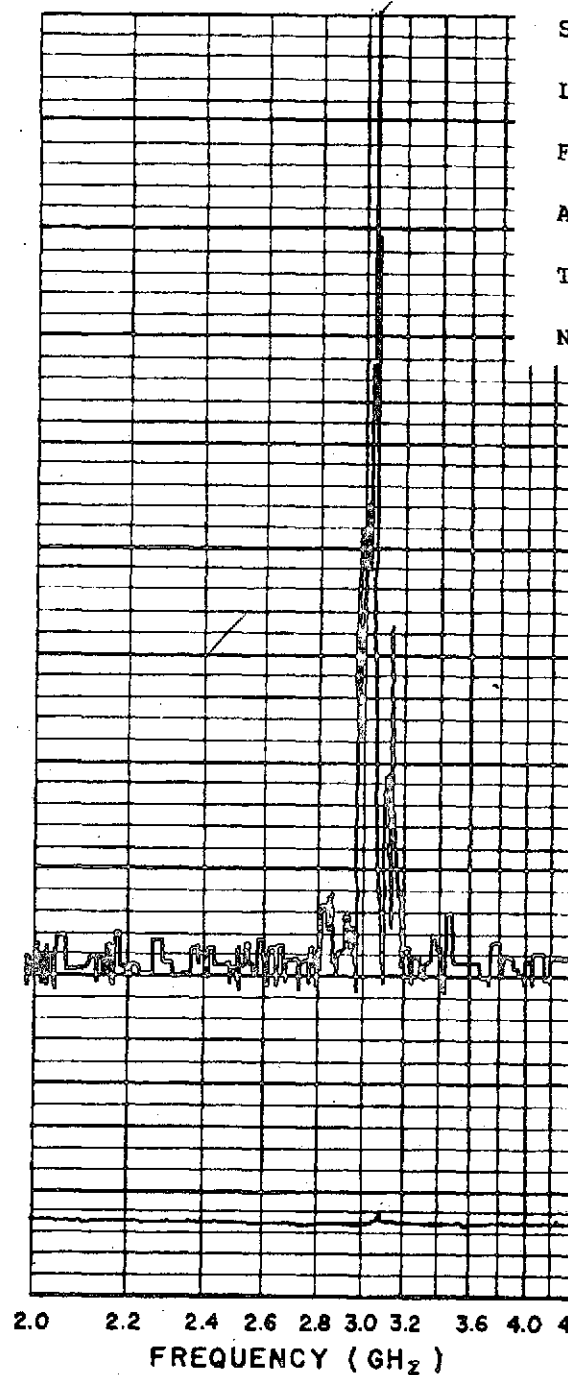


CHART B-9

91 dB/uv

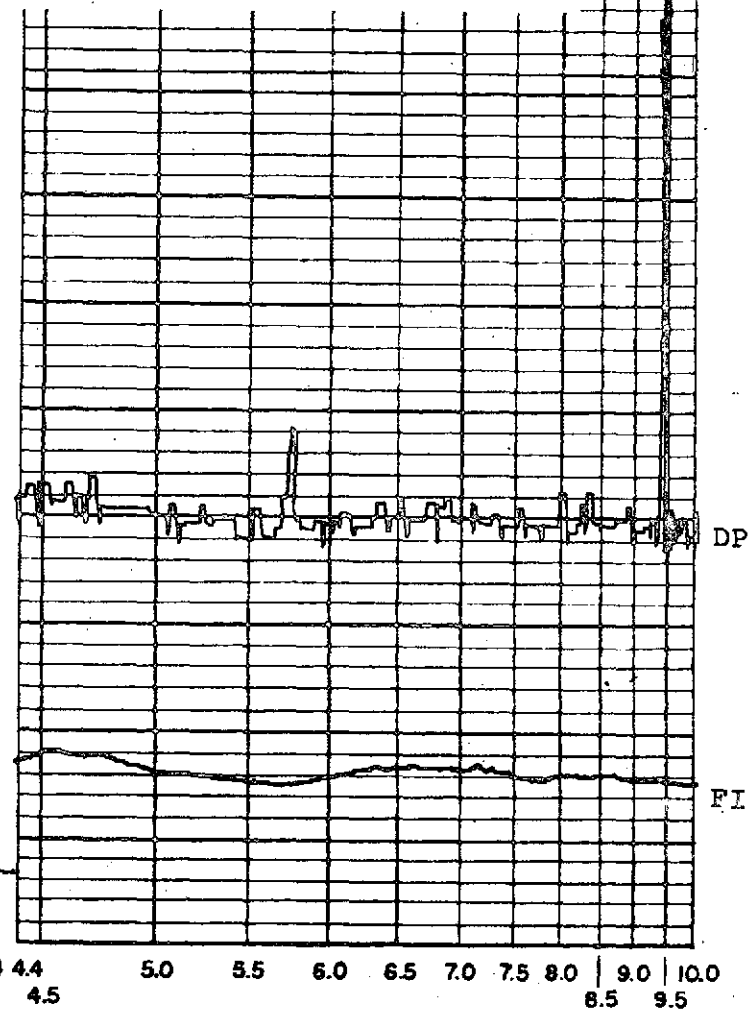


FREQUENCY (GHz)

Shipboard L-Band Terminal EMI Survey

84 dB/uv

Ship 141745 Date 1/2/74
Location 72° 56' N Harbor SAVANNAH At-Sea
Freq. Range to GHz. Bw 5 MHz
Atten 0 dB Function Observer J.H/E.P.
Test Point Filter Pos.
12m Low Loss Cable
Note



dB/uv

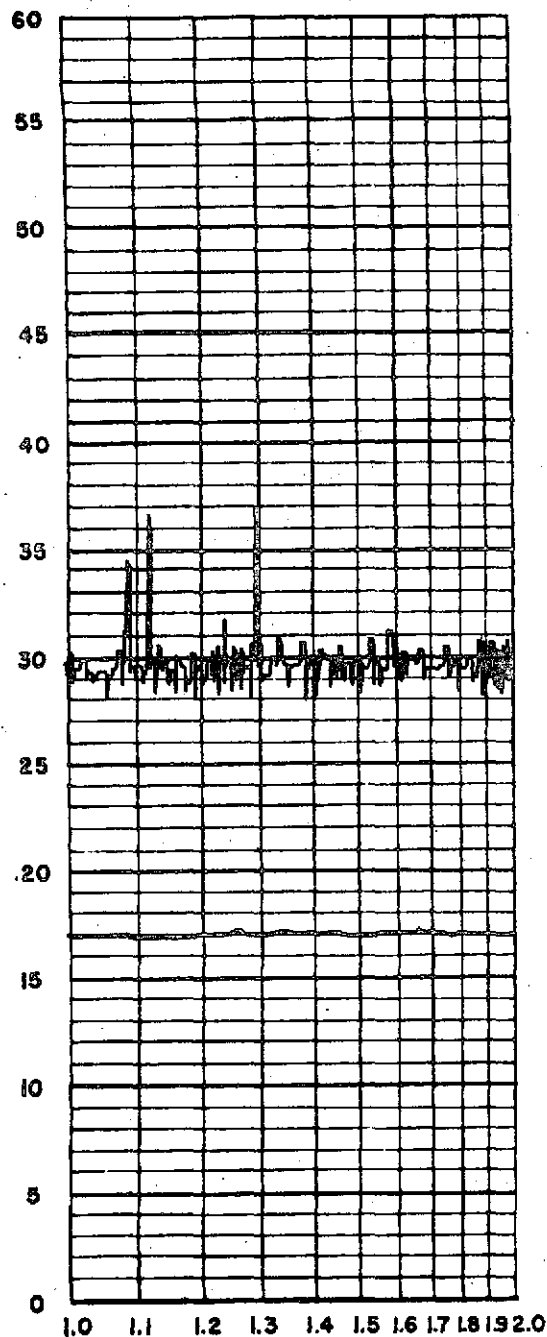
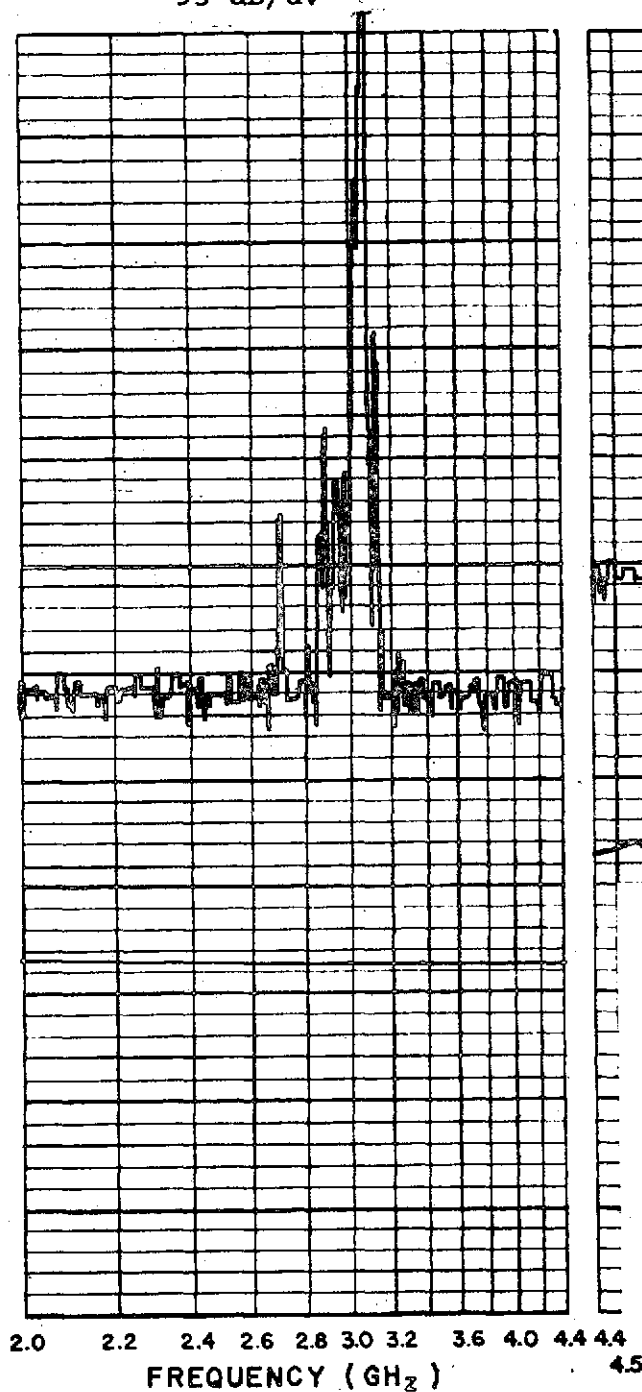
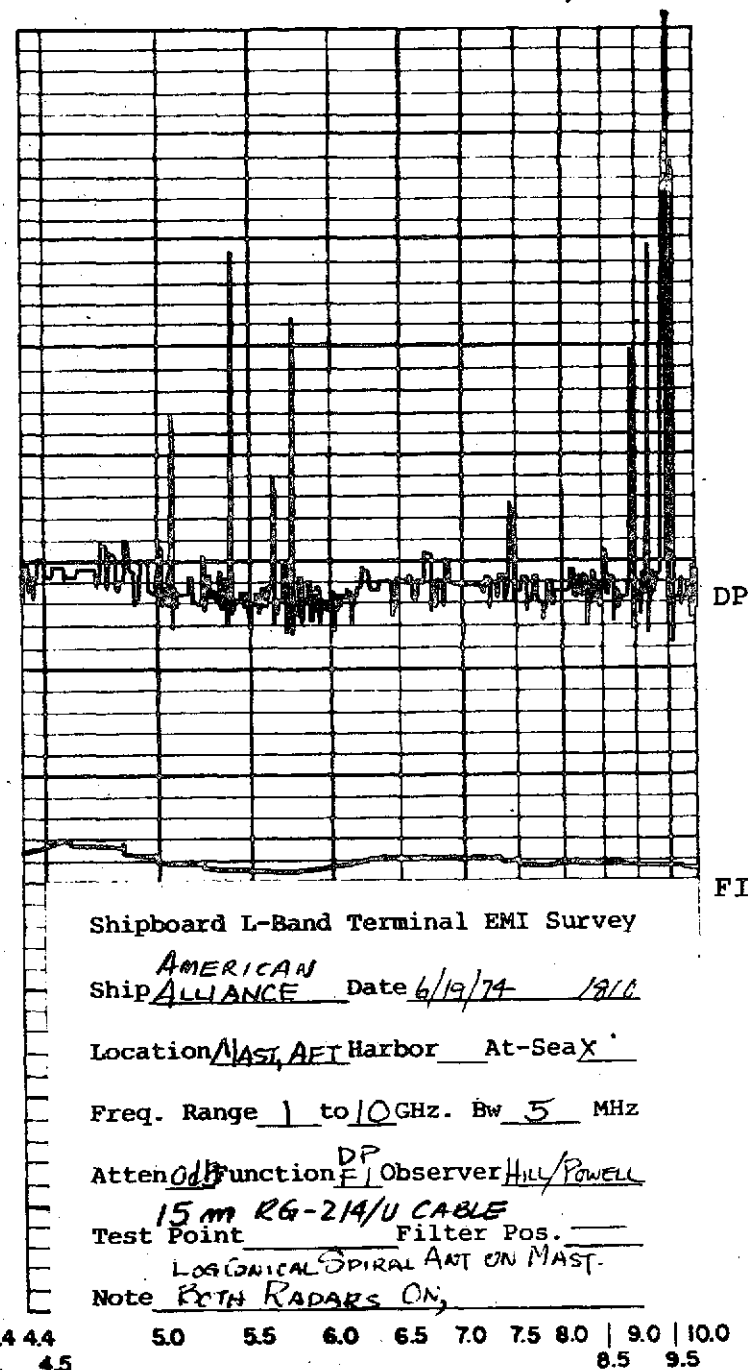


CHART B-10

95 dB/uv



104 dB/uv



Shipboard L-Band Terminal EMI Survey

Ship AMERICAN ALLIANCE Date 6/19/74 1910Location NAST, AET Harbor At-Sea XFreq. Range 1 to 10 GHz. Bw 5 MHzAtten 0 dB Function DP Observer HILL/POWELLTest Point 15 m RG-214/U CABLE Filter Pos. LOGICAL SPIRAL ANT ON MAST.Note BOTH RADARS ON.

FI

dB/uv

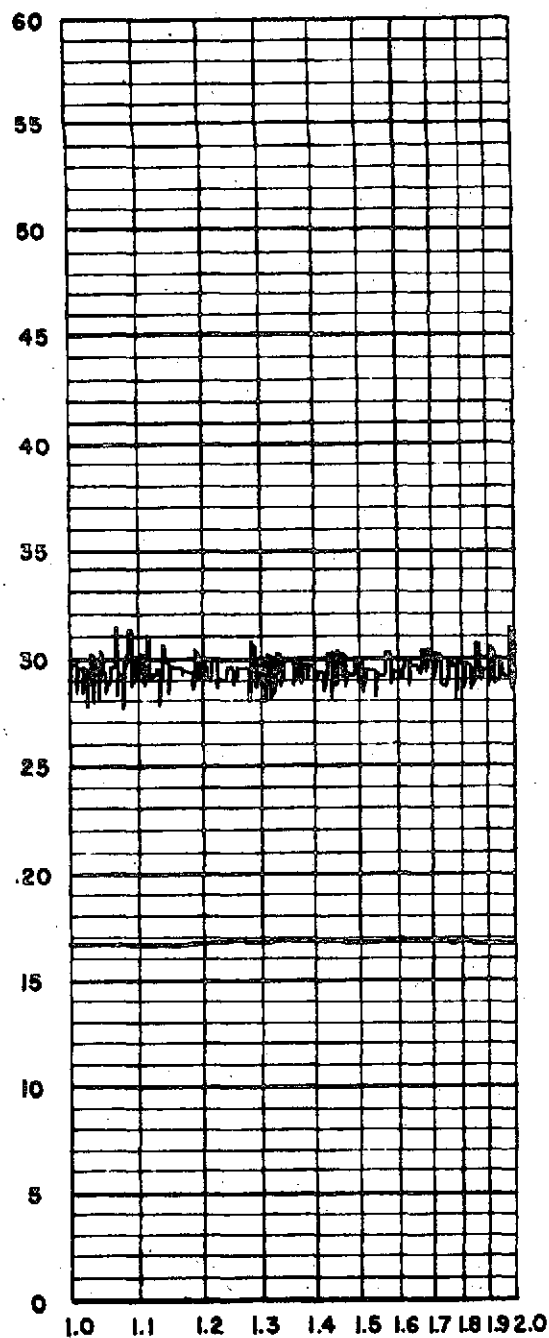
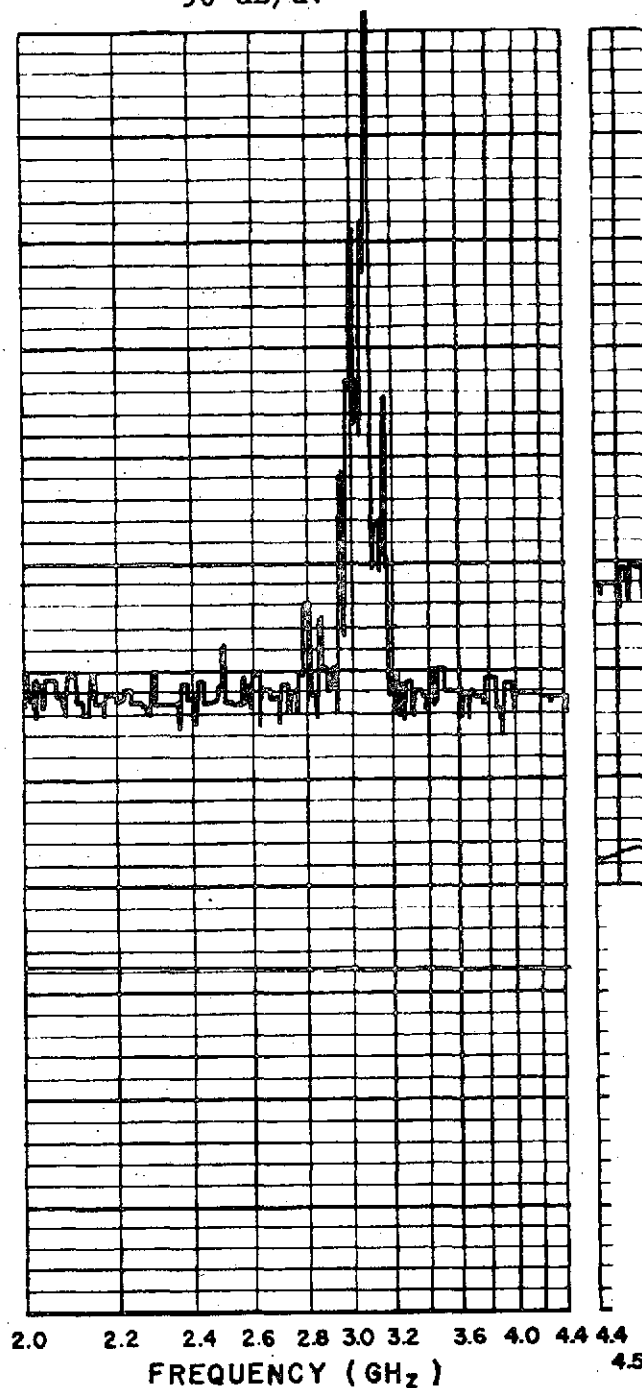
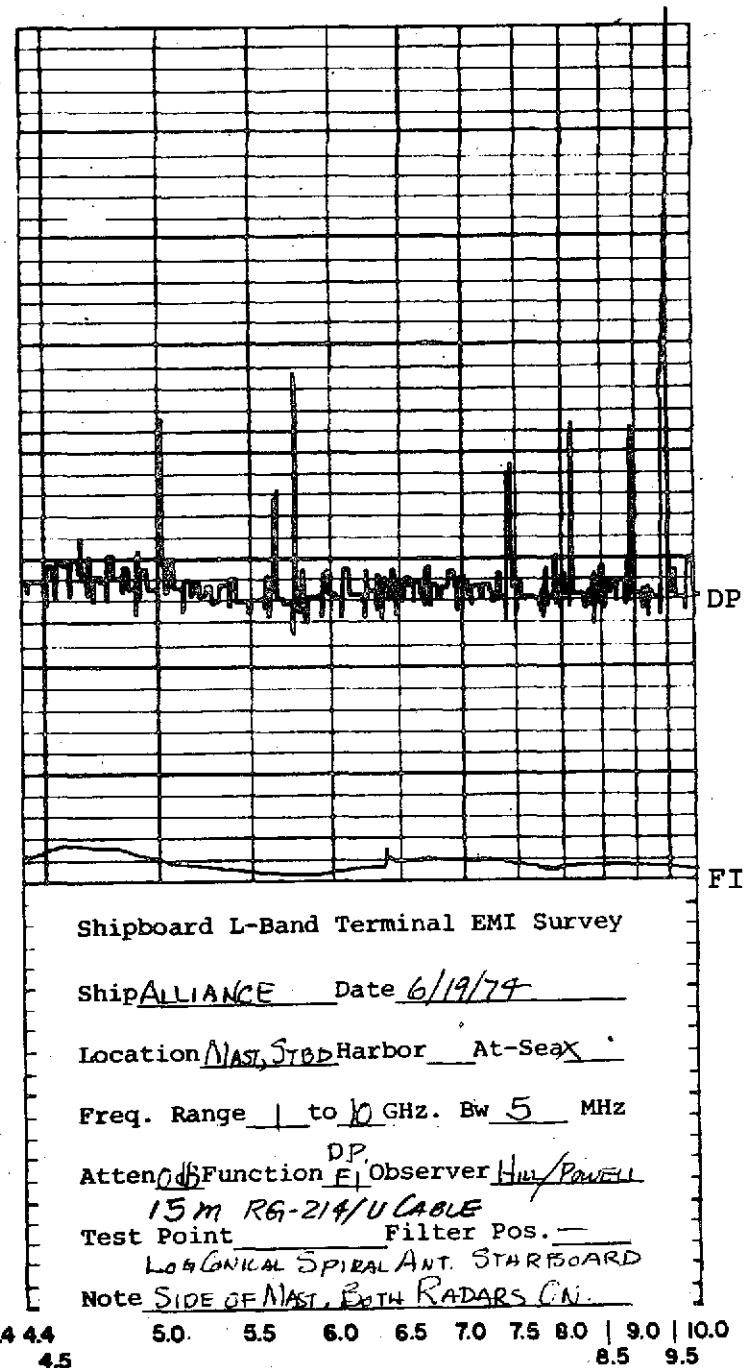


CHART B-11

90 dB/uv



99 dB/uv



Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/79Location NAST, STBD Harbor At-Sea XFreq. Range 1 to 10 GHz. BW 5 MHzAttenuation 0 dB Function FI Observer Hill/PowellTest Point 15m RG-214/U CABLE Filter Pos. —LOGICAL SPIRAL ANT. STARBOARDNote SIDE OF NAST, BOTH RADARS ON.

dB/uv

60

55

50

45

40

35

30

25

20

15

10

8

0

RADAR SIGNAL
12 sec/REV

D.P.

F.I.

1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 2.0

CHART B-12

2.0 2.2 2.4 2.6 2.8 3.0 3.2 3.6 4.0 4.4 4.5
FREQUENCY (GHz)

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/18/74 0930Location STBD FB Harbor PHILADELPHIA At-SeaFreq. Range 1 to 10 GHz Bw 5 MHzAtten 1 Function DP TOP 12mv LOW LOSS CABLE Observer EDTest Point FI BOTTOM Filter Pos. —4-Foot Dish Pointed Directly At
Note BRIDGE TRAFFIC & CRANE

DP

FI

5.0 5.5 6.0 6.5 7.0 7.5 8.0 8.5 9.0 9.5 10.0

dB/uv

60

55

50

45

40

35

30

25

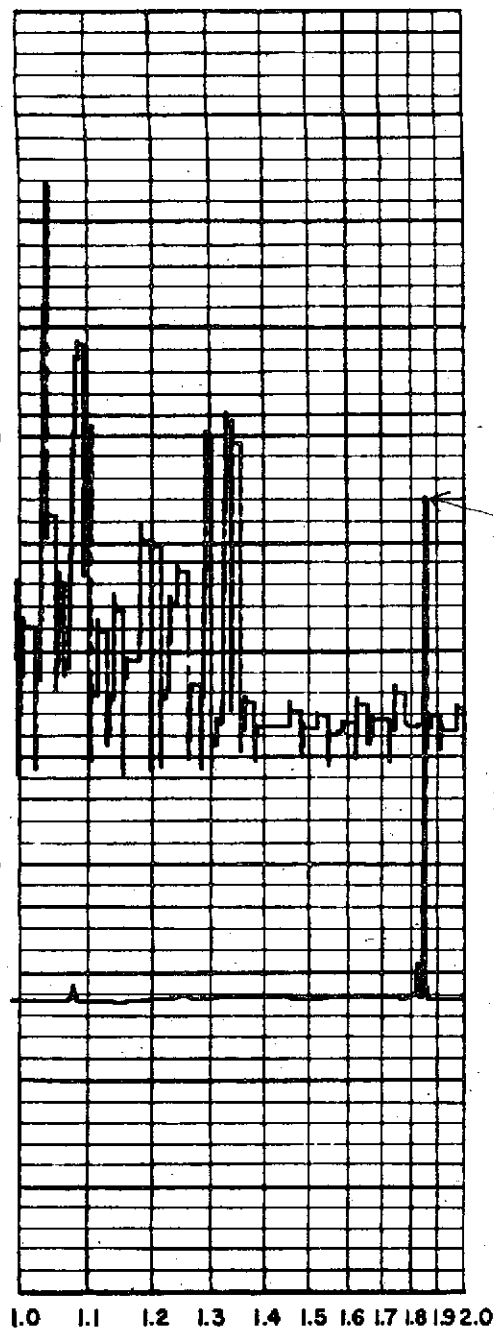
20

15

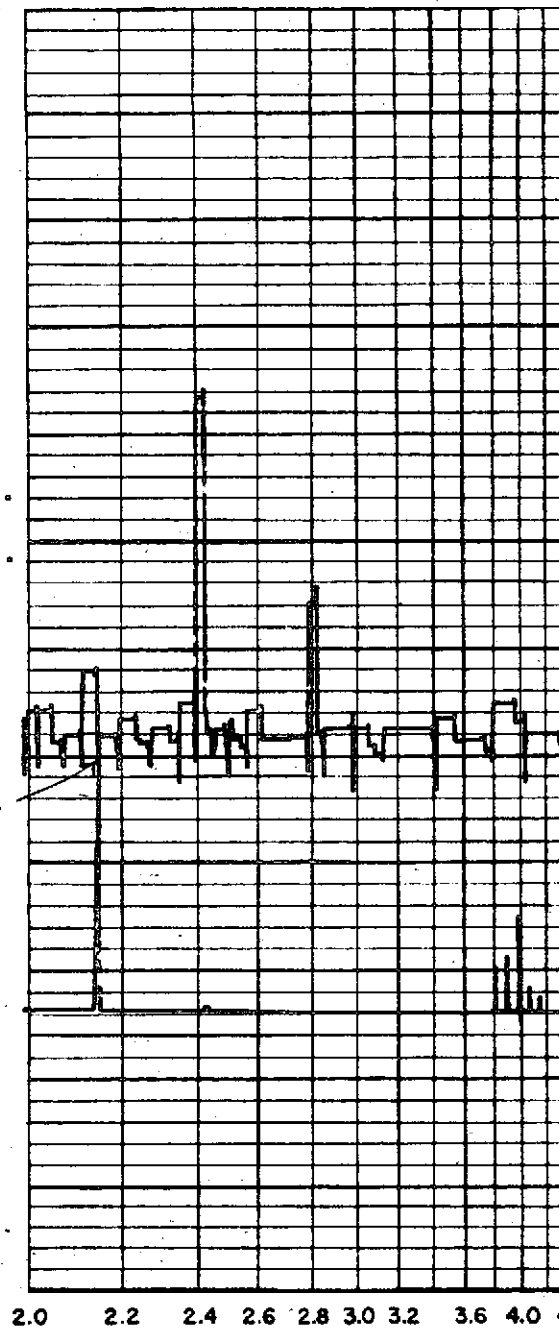
10

5

0

F.I.
&
D.P.

F.I.

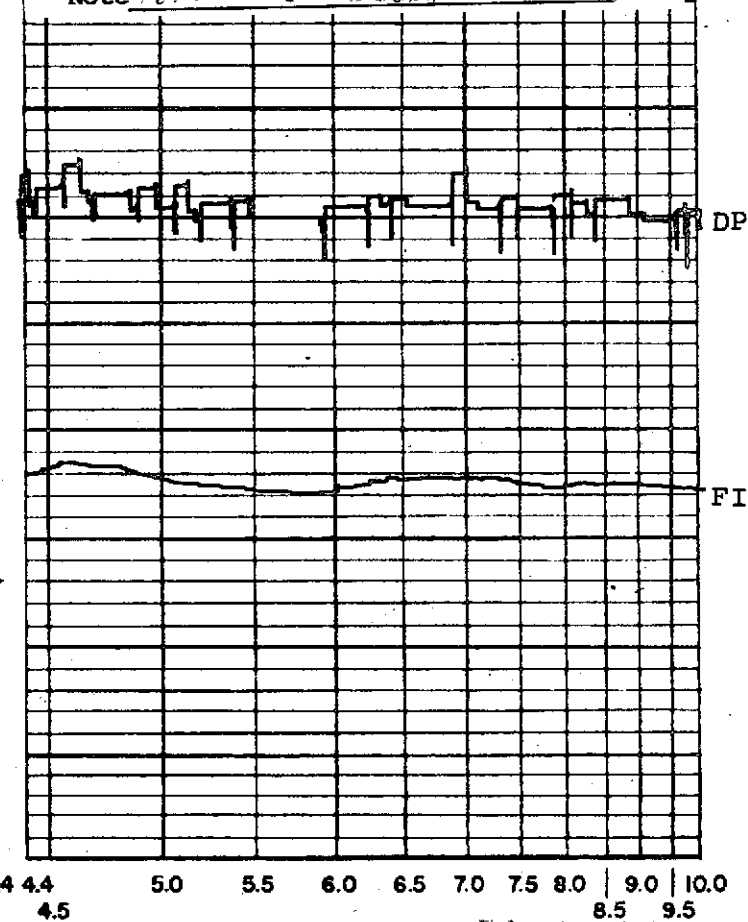


FREQUENCY (GHz)

Shipboard L-Band Terminal EMI Survey

Ship ALLANCE Date 6/10/79 WISNESLocation TBD FB. Harbor PHILADELPHIA
At-Sea
LOG SPIRAL ANT.Freq. Range 1 to 10 GHz. Bw 5 MHzAtten 0 12m Low Loss CABLE
Function DP Observer Hill/Dwell
SHIPS RADARS OFF

Test Point _____ Filter Pos. _____


Note POINTED ACROSS DELLA ROA
TOWARD POINTA PHILA.

DP

FI

CHART B-13

B-17


RADAR
 75 dB/uv
 60
 dB/uv

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/12/74 1430 Hrs

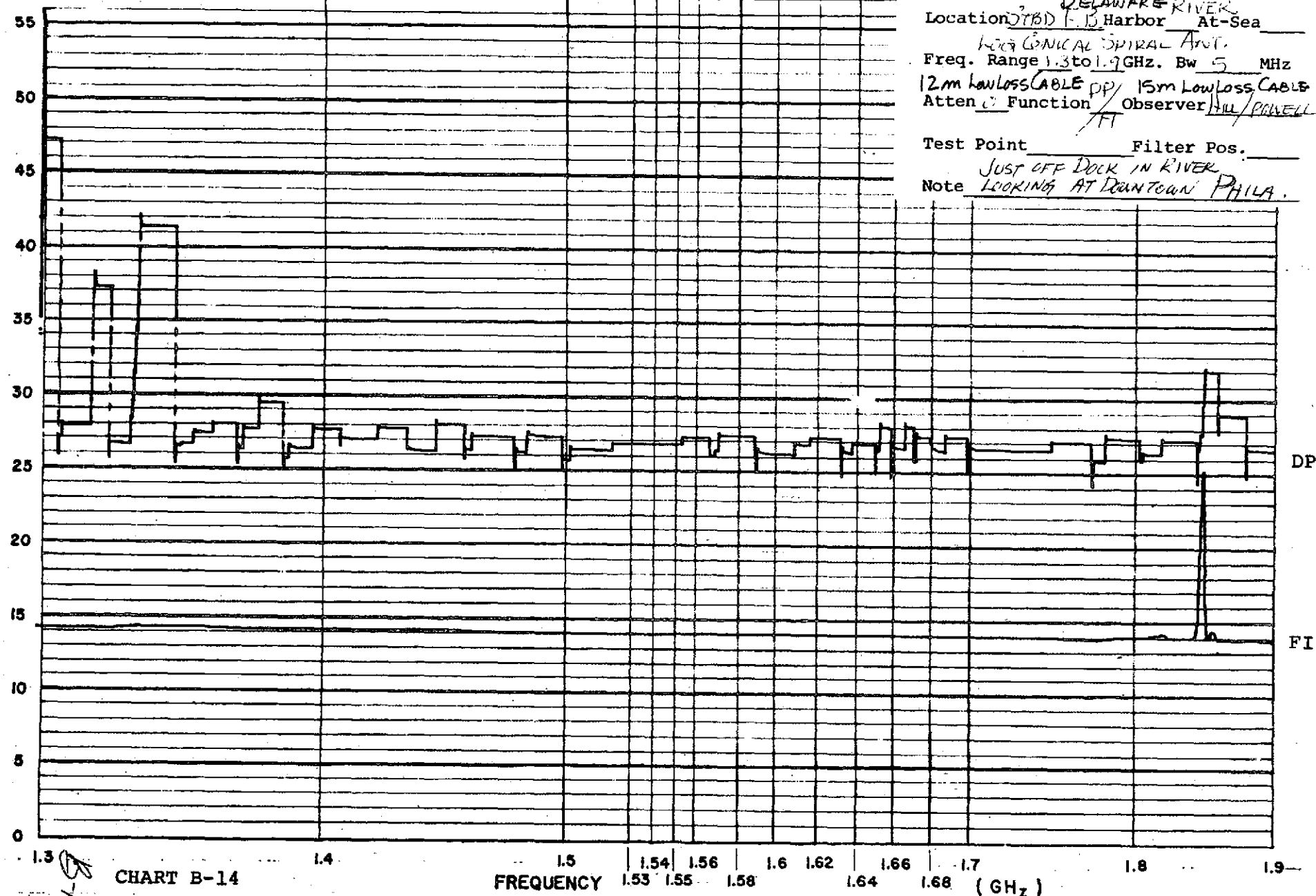
Location DELAWARE RIVER
DBD Harbor At-Sea

Ant. LOG CONICAL SPIRAL ANT.
 Freq. Range 1.3 to 1.9 GHz Bw 5 MHz

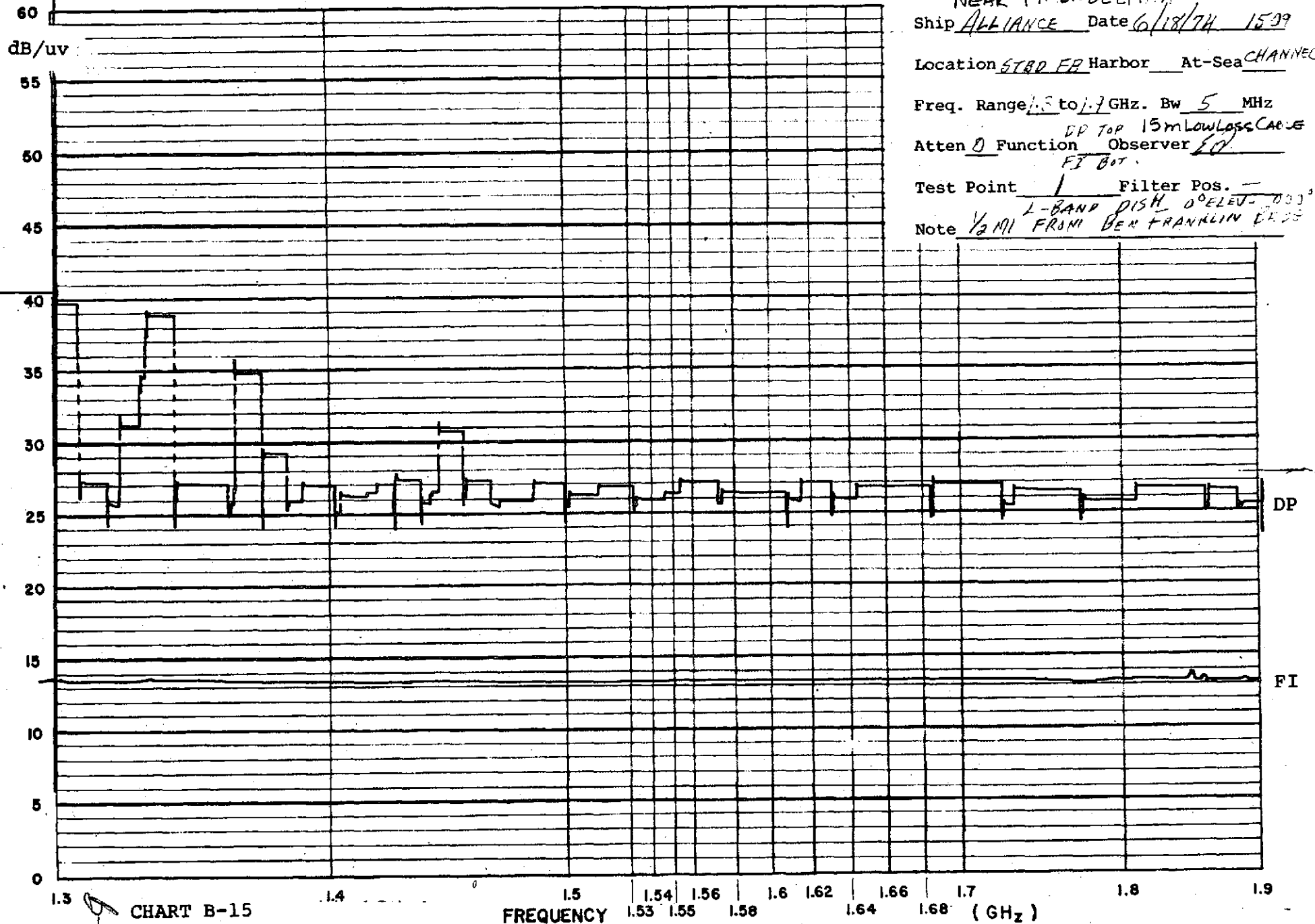
12m Low Loss Cable pp 15m Low Loss Cable
 Atten 0 Function / Observer HILL/POWELL
/FT

Test Point Filter Pos.

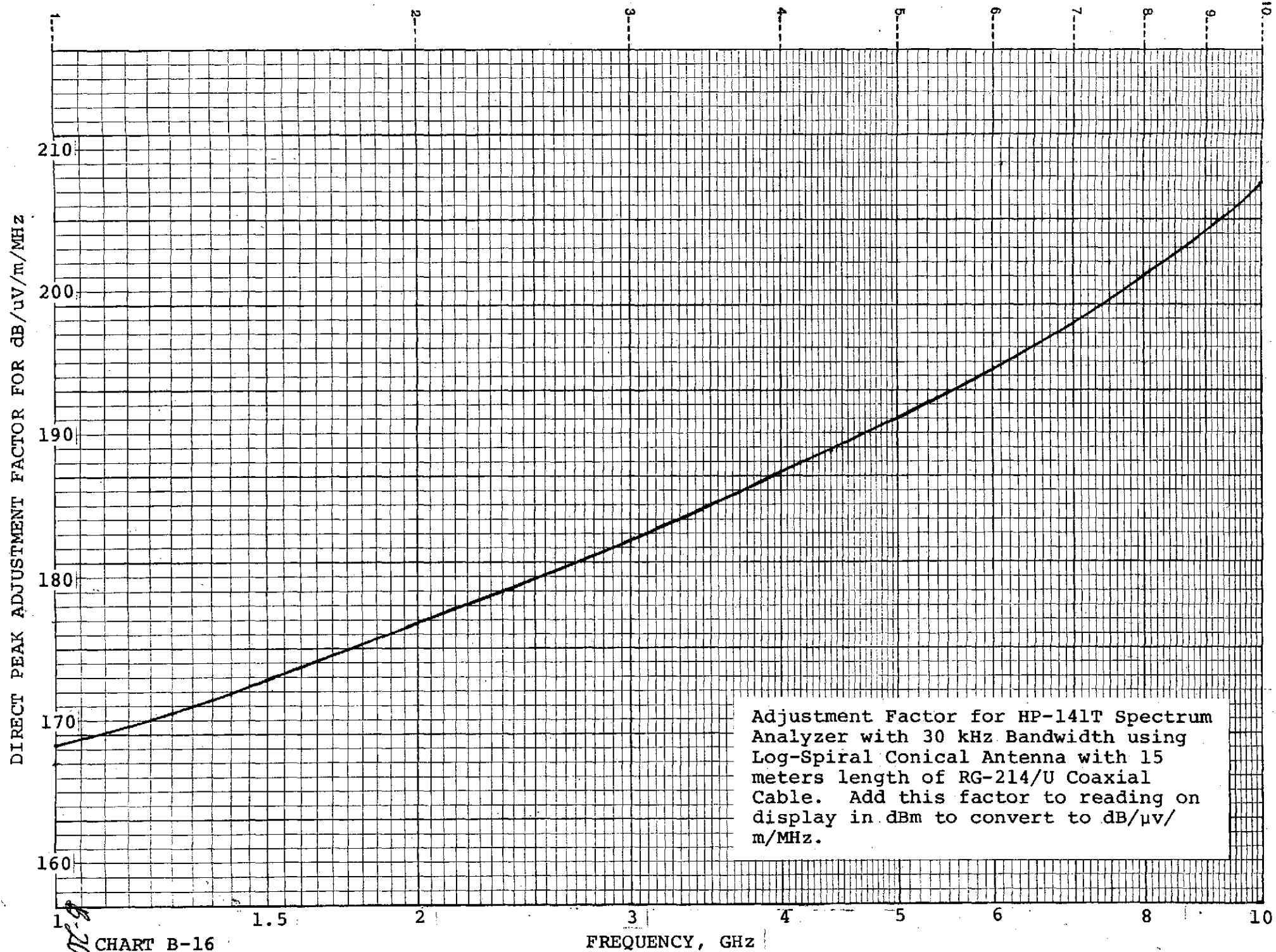
Note JUST OFF DOCK IN RIVER
LOOKING AT DOWNTOWN PHILA.



⌋ RADAR
110 dB/uv
12 sec/rev.



RIVER AMBIENT
Shipboard L-Band Terminal EMI Survey
NEAR PHILADELPHIA
Ship ALLIANCE Date 6/18/74 1539
Location STAR FR Harbor At-Sea CHANNEL
Freq. Range 1.5 to 1.7 GHz. Bw 5 MHz
Atten 0 Function DP TOP 15m LOW LOSS CABLE Observer ED
FI Bot.
Test Point 1 Filter Pos. —
Note 1/2 MI L-BAND DISH 0° ELEV. 000°
FROM BEN FRANKLIN BRIDGE



Spectrum Display B-1

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1920

Center Freq. 3050 MHz, Bandwidth 30 KHz

Scan Width 50 MHz/div, Log Ref Level -40 dBm

15m RG-214/U CABLE

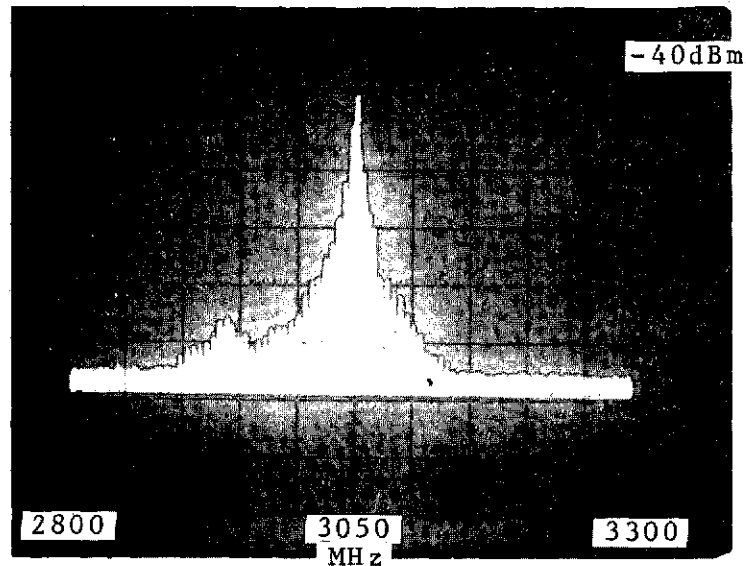
Test Point LOG CONICAL Filter Pos.

ANT ON STARBOARD SIDE OF RADAR MAST

Location Harbor At-Sea X

S BAND RADAR ON SCAN TIME

Date Note 1 SEC/DIV Observer Hill/POWELL



The spectrum display photograph data must be adjusted for antenna factor, cable loss, and bandwidth using Chart B-16. For explanation see first page of Appendix B. The vertical scale on the spectrum display is 10 dB per major division.

Spectrum Display B-2

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1908

Center Freq. 9330 MHz, Bandwidth 30 KHz

Scan Width 10 MHz/div, Log Ref Level -40 dBm

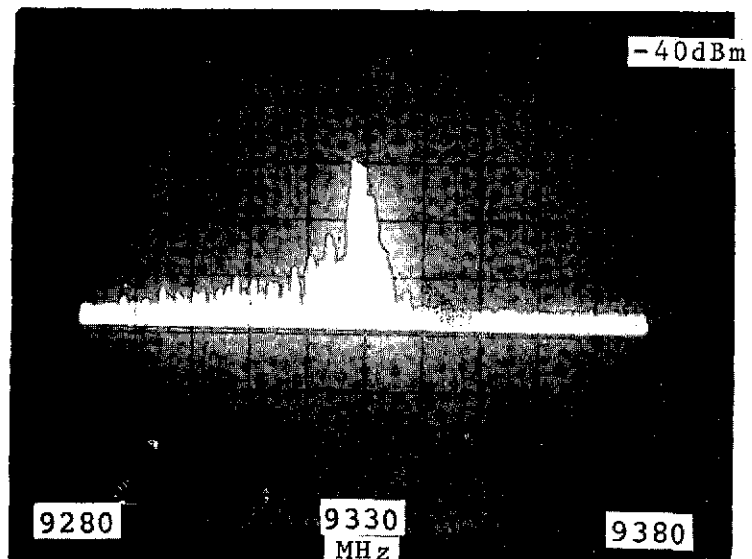
Test Point LOG CONICAL SPIRAL ANT Filter Pos.

WITH 50' OF RG-214U, LOOKING TOWARD PORTSIDE

Location MAST, STBD Harbor At-Sea X

X BAND RADAR ON SCAN TIME

Date Note 2 SEC/DIV Observer Hill/POWELL



B-21

APPENDIX C, FILTER EVALUATION

Chart C-1, T.P.1, Radars Off, Monday PM, In Harbor
Chart C-2, T.P.1, Radars Off, Tuesday AM, In Harbor
Chart C-3, T.P.1, Radars Off, At-Sea
Chart C-4, T.P.1, Radars Off, In-Band, At-Sea
Chart C-5, T.P.1, S-Band Radar On
Chart C-6, T.P.1, S-Band Radar On, In-Band
Chart C-7, T.P.1, Radars On, In-Band
Chart C-8, T.P.1, Radars On
Chart C-9, T.P.1, Radars On, Filter In
Chart C-10, T.P.2, Radars Off
Chart C-11, T.P.2, Radars Off, In-Band
Chart C-12, T.P.2, S-Band Radar On
Chart C-13, T.P.2, S-Band Radar On, In-Band
Chart C-14, T.P.2, Radars On, Filter In
Chart C-15, T.P.3, Radars Off
Chart C-16, T.P.3, Radars Off, In-Band, LNA Ser. No. 001
Chart C-17, T.P.3, Radars Off, In-Band, LNA Ser. No. 010
Chart C-18, T.P.3, S-Band Radar On
Chart C-19, T.P.3, S-Band Radar On, In-Band
Chart C-20, T.P.3, Output of LNA
Chart C-21, T.P.3A, Radars Off, In-Band, LNA Ser. No. 010
Chart C-22, S-Band Radar On, TX Port of Duplexer
Chart C-23, Adjustment Factor, NM-65T, Two Terminal Voltmeter

APPENDIX C, Continued

Spectrum Display C-1, T.P.1, S-Band Radar On
Spectrum Display C-2, T.P.1, X-Band Radar On
Spectrum Display C-3, T.P.2, S-Band Radar On
Spectrum Display C-4, T.P.1, Radars Off, Shore Signal
Spectrum Display C-5, T.P.1, S-Band Radar On
Spectrum Display C-6, T.P.1, Radars On
Spectrum Display C-7, T.P.1, S-Band Radar On
Spectrum Display C-8, T.P.1, S-Band Radar On
Spectrum Display C-9, T.P.1, S-Band Radar On, 0.5-2.5 GHz
Spectrum Display C-10, T.P.2, S-Band Radar On, 0.5-2.5 GHz
Spectrum Display C-11, T.P.3, S-Band Radar On, 0.5-2.5 GHz
Spectrum Display C-12, T.P.1, S-Band Radar On, 2.07-6.15 GHz
Spectrum Display C-13, T.P.2, S-Band Radar On, 2.07-6.15 GHz
Spectrum Display C-14, T.P.3, S-Band Radar On, 2.07-6.15 GHz
Spectrum Display C-15, T.P.1, S-Band Radar On, 6.17-10.25 GHz
Spectrum Display C-16, T.P.2, S-Band Radar On, 6.17-10.25 GHz
Spectrum Display C-17, T.P.3, S-Band Radar On, 6.17-10.25 GHz
Spectrum Display C-18, T.P.4, Radars Off
Spectrum Display C-19, T.P.4, Radars Off
Spectrum Display C-20, Spectrum Analyzer Spurious Display
Spectrum Display C-21, T.P.4, Radars Off, Filter In
Spectrum Display C-22, T.P.4, Radars Off, Filter Out
Spectrum Display C-23, T.P.4, Radars On, Filter Out
Spectrum Display C-24, T.P.4, Radars On, Filter In

APPENDIX C, Continued

Comments on the Use of the Charts and Spectrum Displays

The Charts C-1 through C-22, made with the Stoddart NM-65 Radio Interference Analyzer, require interpretation with an adjustment factor which is supplied in Chart C-23. This adjustment factor compensates for the variation of gain with frequency when the NM-65 is calibrated at one frequency, as it must be for use with the X-Y recorder.

For example, refer to Chart C-5 at the frequency 3.1 GHz, the broadband magnitude on the chart scale is 53 dB for the DP trace.

From Chart C-5	53 dB
Attenuator setting	<u>20 dB</u>
	73 dB
Adjustment Factor from Chart C-23	<u>-4 dB/μv/MHz</u>
Adjusted value	69 dB/μv/MHz

Thus 69 dB/μv/MHz is the adjusted level at 3.1 GHz at Test Point 1 with the S-band radar on. The spectrum display photographs require no adjustment to obtain the peak signal level in dBm. Each major division on the vertical scale on the spectrum display is 10 dB. To convert to dB/μv/MHz requires an adjustment for bandwidth. This bandwidth factor is equal to $20 \log \frac{1 \text{ MHz}}{\text{BW}}$. For example by reference to Spectrum Display C-4, where the maximum signal level is -58 dBm at approximately 1296.5 MHz and the bandwidth is 100 kHz, the signal level in dB/μv/MHz would be found as follows:

APPENDIX C, Continued

Signal level from Spectrum Display C-4	- 58 dBm
conversion to μv	<u>+107 dB</u>
	49 dB/ μv
bandwidth adjustment A_{BW}	<u>+ 20 dB/MHz</u>
adjusted value of broadband signal	69 dB/ μv /MHz
where $A_{\text{BW}} = 20 \log \frac{1 \text{ MHz}}{100 \text{ kHz}} = 20 \text{ dB}$	

Note that various bandwidths (30 kHz, 100 kHz, and 300 kHz) have been used in the operation of the spectrum analyzer.

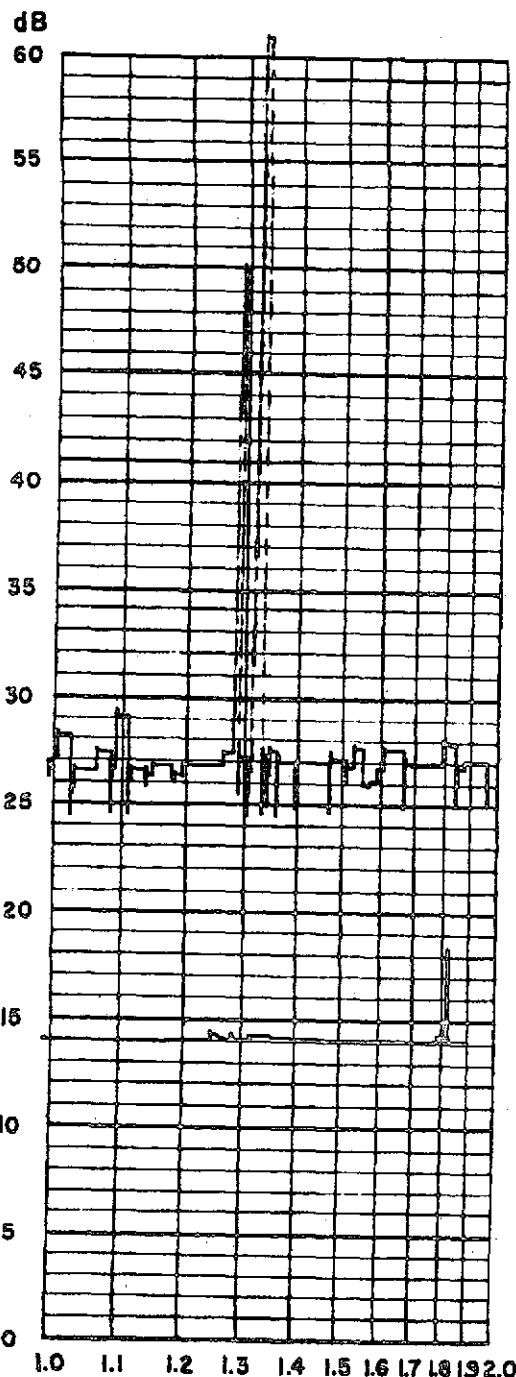
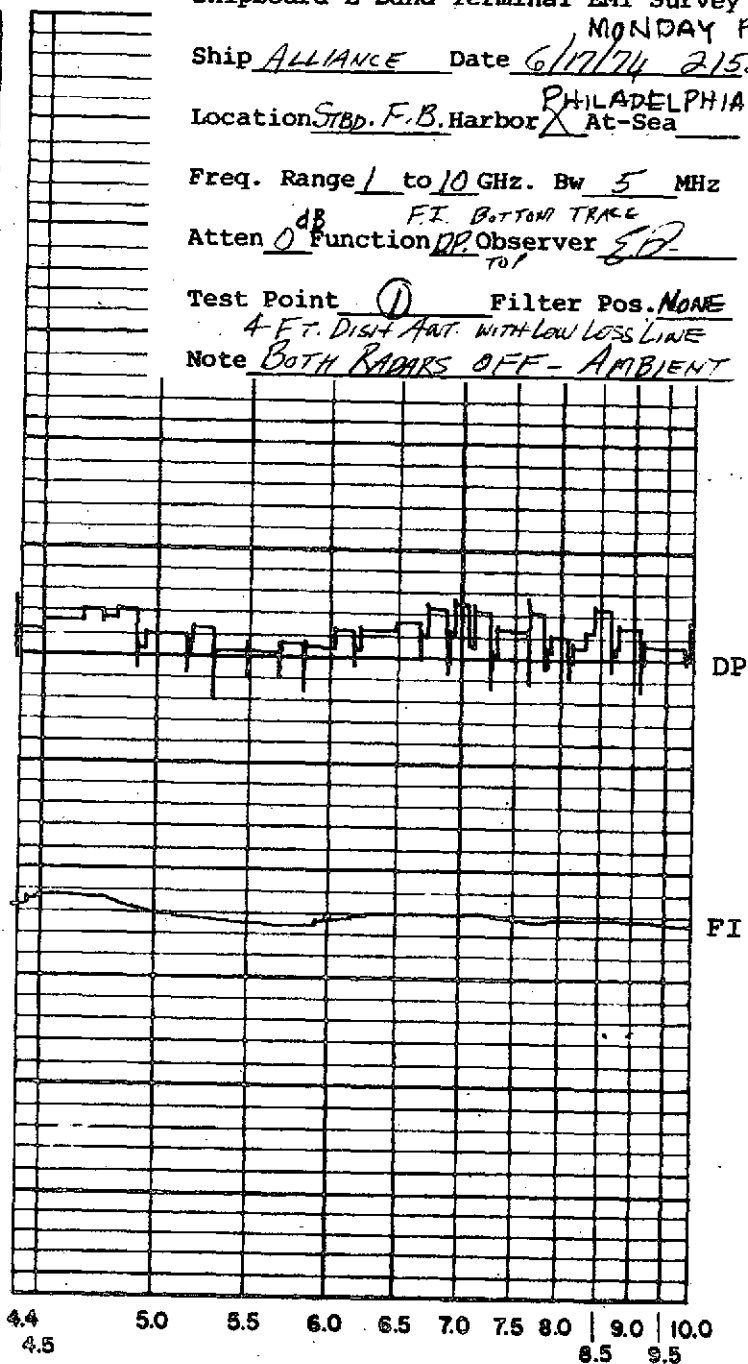
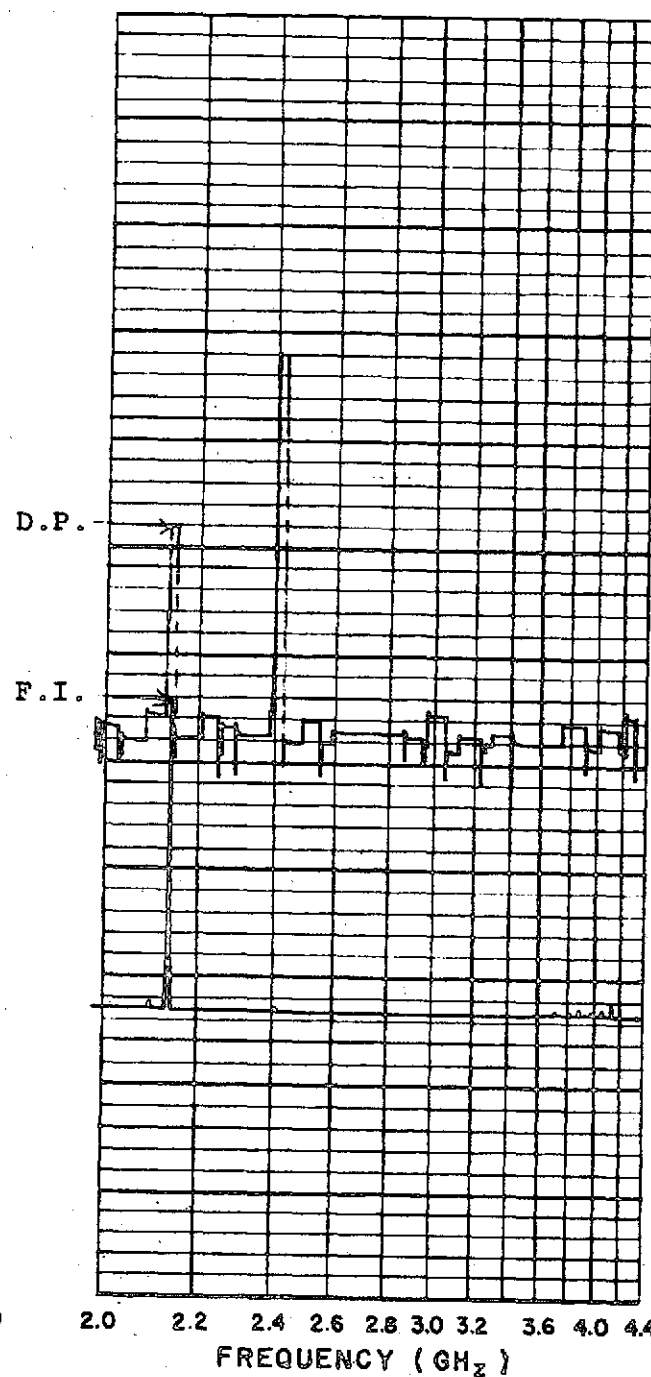


CHART C-1



PHILA. HARBOUR
 Shipboard L-Band Terminal EMI Survey
 Ship ALLIANCE Date 6/17/74 2152 MONDAY P.M.
 Location STBD. F.B. Harbor PHILADELPHIA
At-Sea
 Freq. Range 1 to 10 GHz. Bw 5 MHz
 Atten 0 dB F.I. BOTTOM TRACE
 Function DP Observer ED
 Test Point ① Filter Pos. NOISE
4 FT. DIST ANT. WITH LOW LOSS LINE
 Note BOTH RADARS OFF - AMBIENT

dB
60

55

50

45

40

35

30

25

20

15

10

5

0

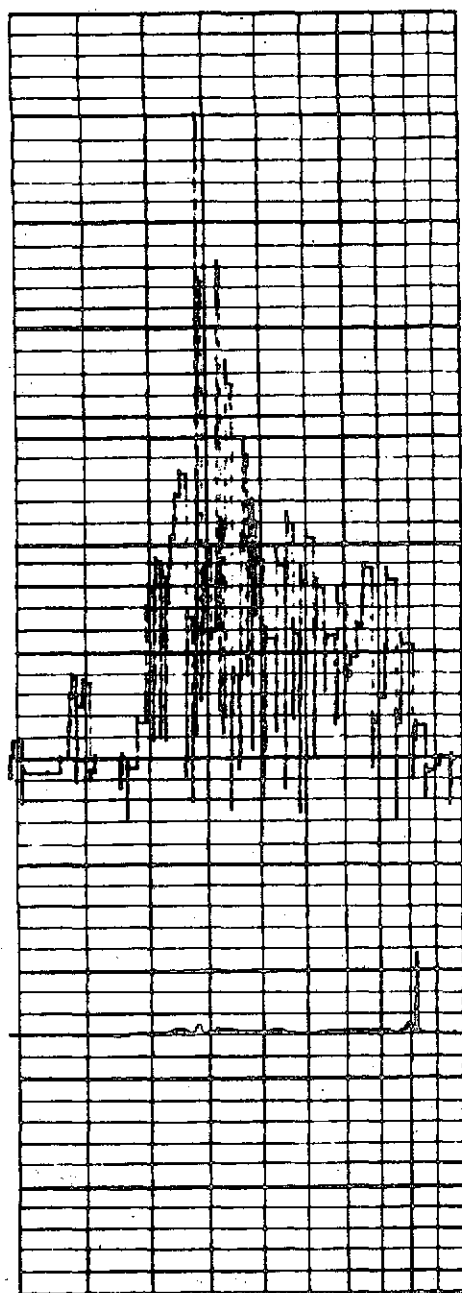
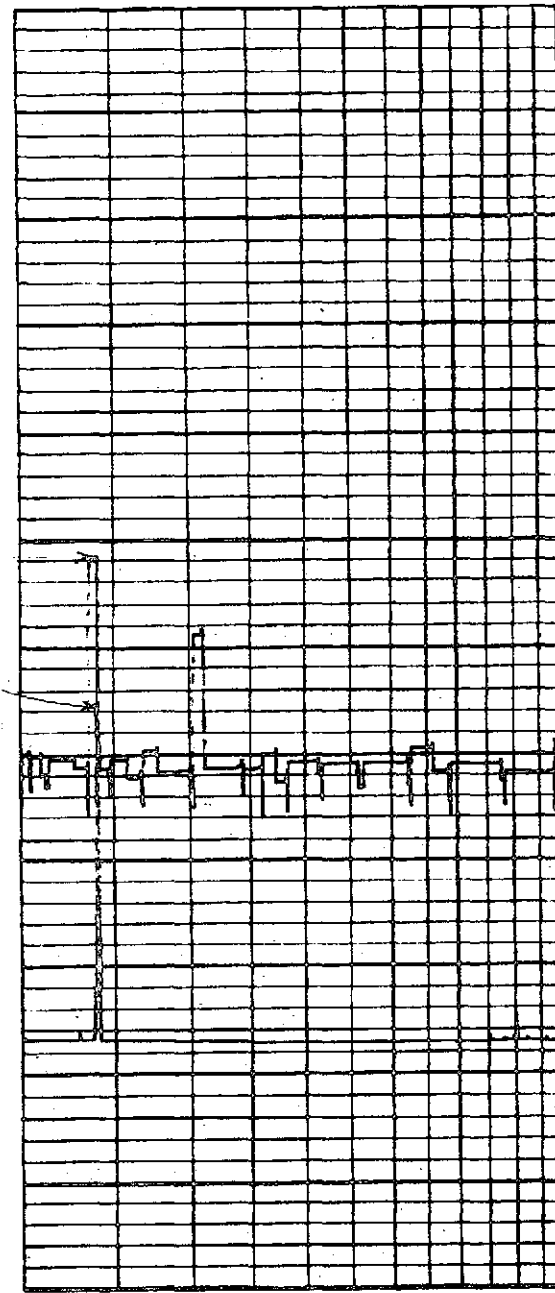


CHART C-2

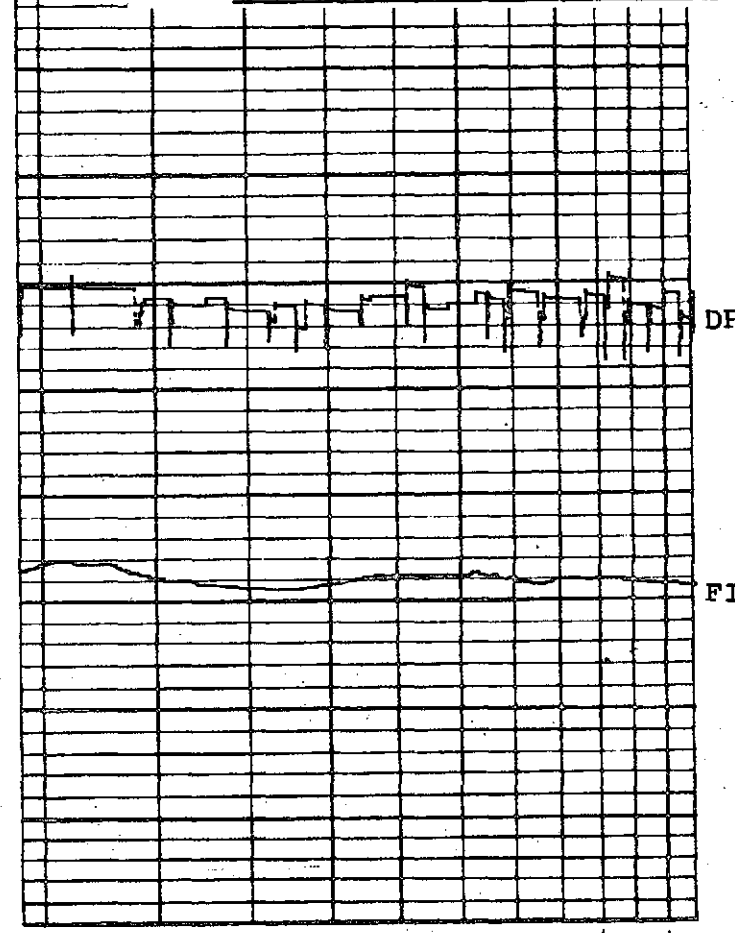
D.P.

F.I.



FREQUENCY (GHz)

HARBOR AMBIENT - PHILA.
Shipboard L-Band Terminal EMI Survey
TUESDAY A.M.
Ship ALLIANCE Date 6/18/74 0900HRS
Location F.B. PHILADELPHIA Harbor STBD At-Sea ✓
Freq. Range 1 to 10 GHz. Bw 5 MHz
Atten 0dB Function F.I. Bottom Observer E.P.
Test Point ① Filter Pos. NONE
4 FT. DISH ANT + LOW LOSS LINE
Note BOTH RADARS OFF



DP

FI

dB
60

55

50

45

40

35

30

25

20

15

10

5

0

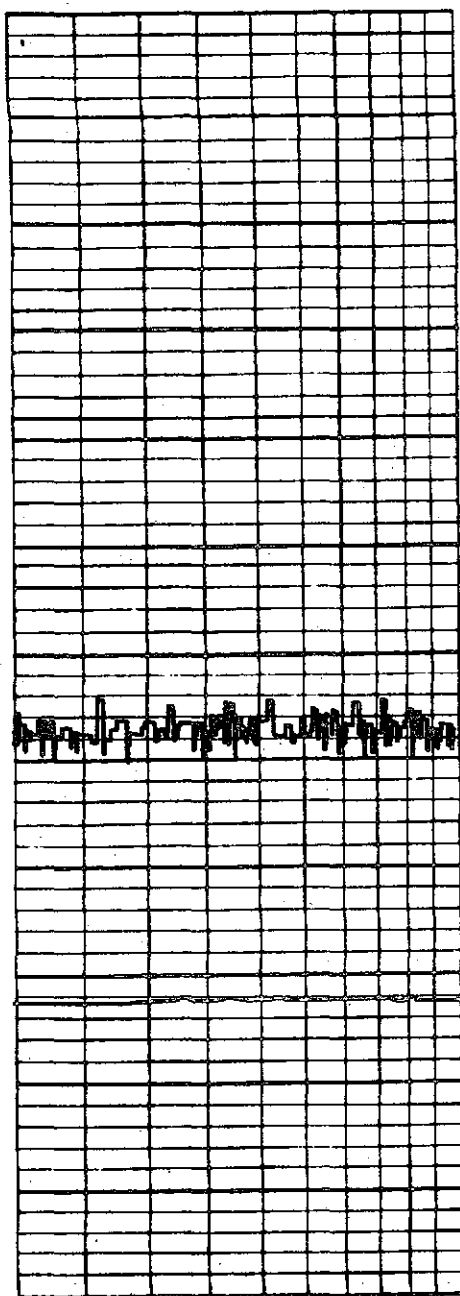
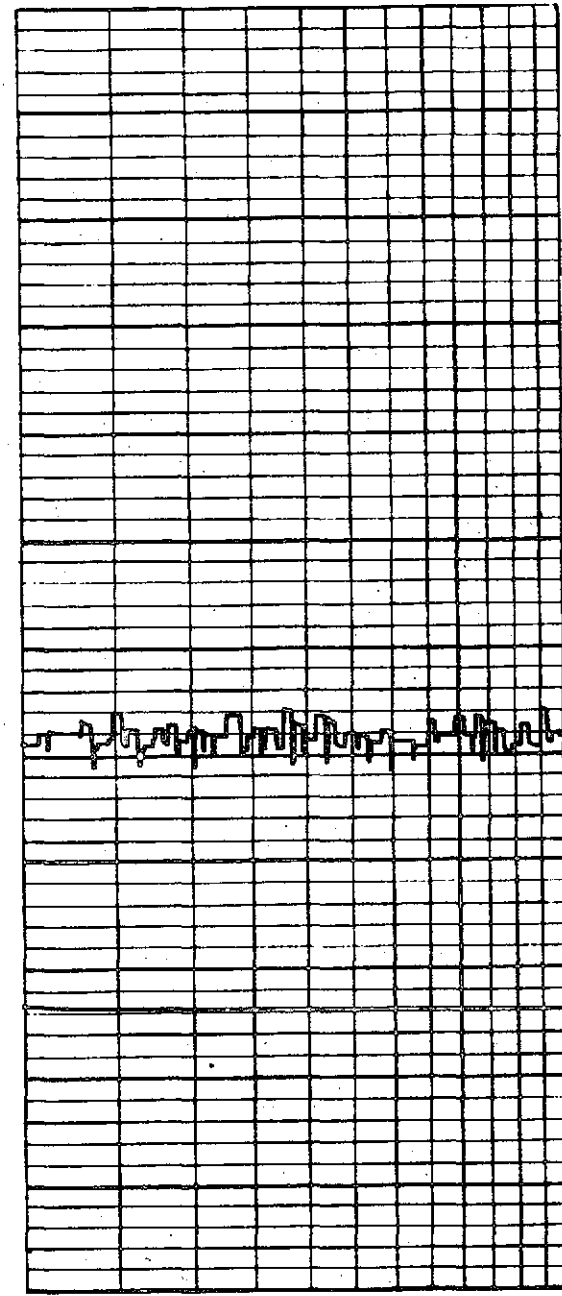


CHART C-3

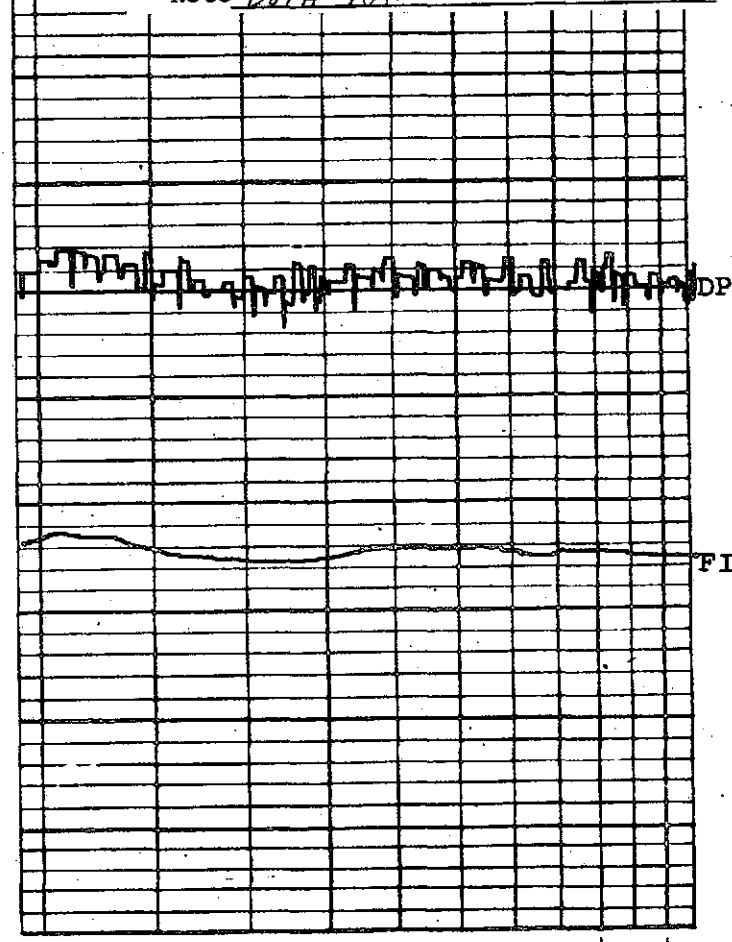


FREQUENCY (GHz)

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1215Location STBD F.B. Harbor At-Sea ☒Freq. Range 1 to 10 GHz. Bw 5 MHzAtten 0 dB Function DP TOP Observer HILL/POWELL
FI BITTest Point ① Filter Pos. NONE

4 FT DISH POINTED AT RADAR ANTS.

Note BOTH RADARS OFF

FI

dB

60

55

50

45

40

35

30

25

20

15

10

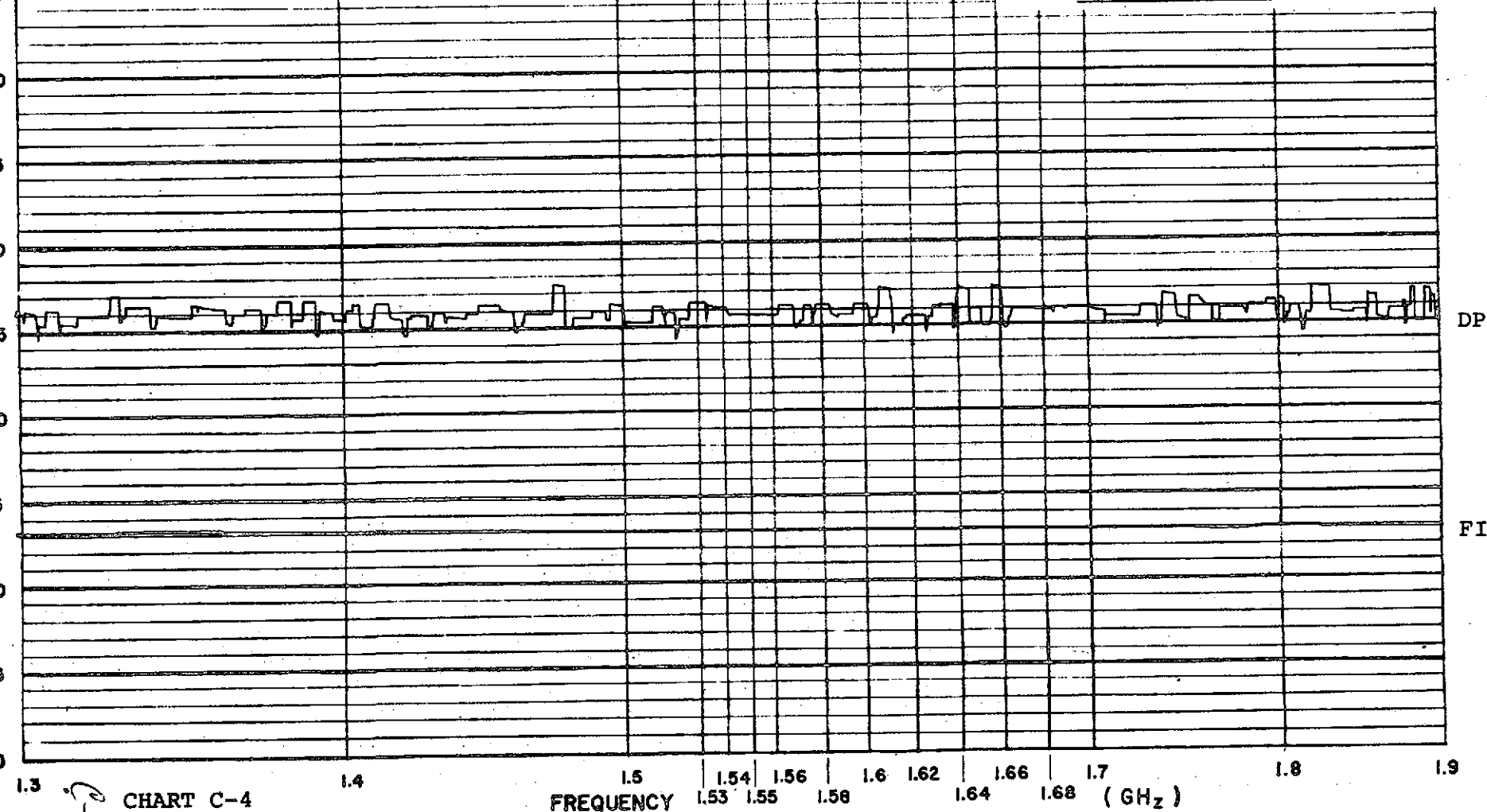
5

0

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74Location STBD F.B. Harbor At-Sea ☒Freq. Range 1.3 to 1.9 GHz. Bw 5 MHzAtten 0 ^{dB} Function DP TOP Observer Hill/PowellTest Point ① ^{FI B-} Filter Pos. NONE

AFY DISH POINTED AT RADAR ANTS

Note BOTH RADARS OFF

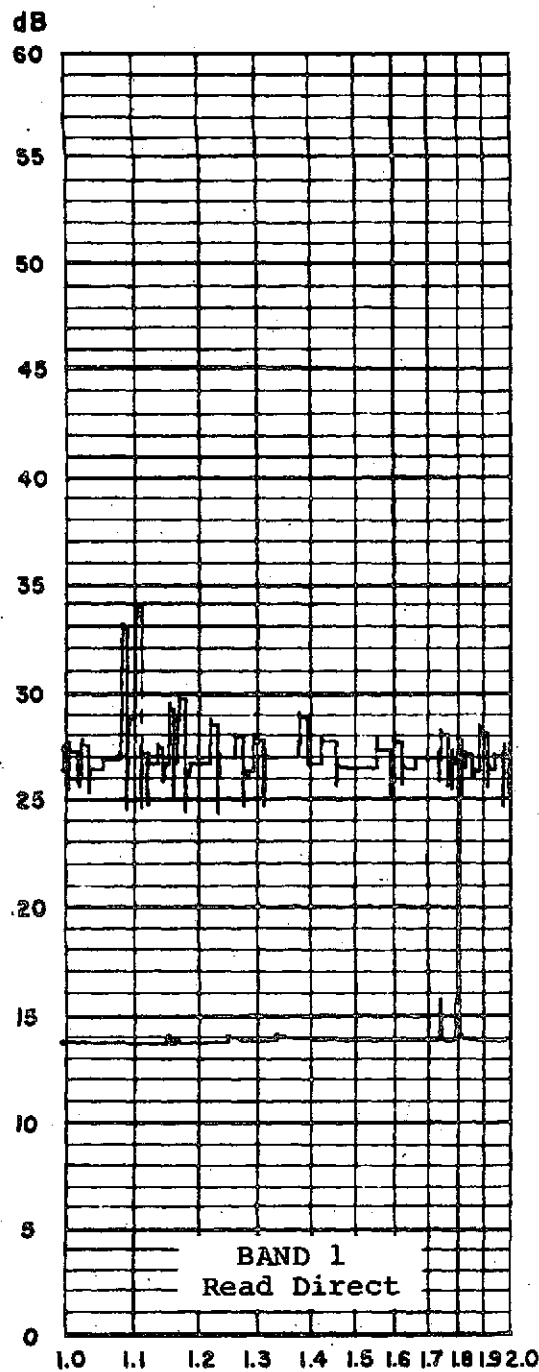
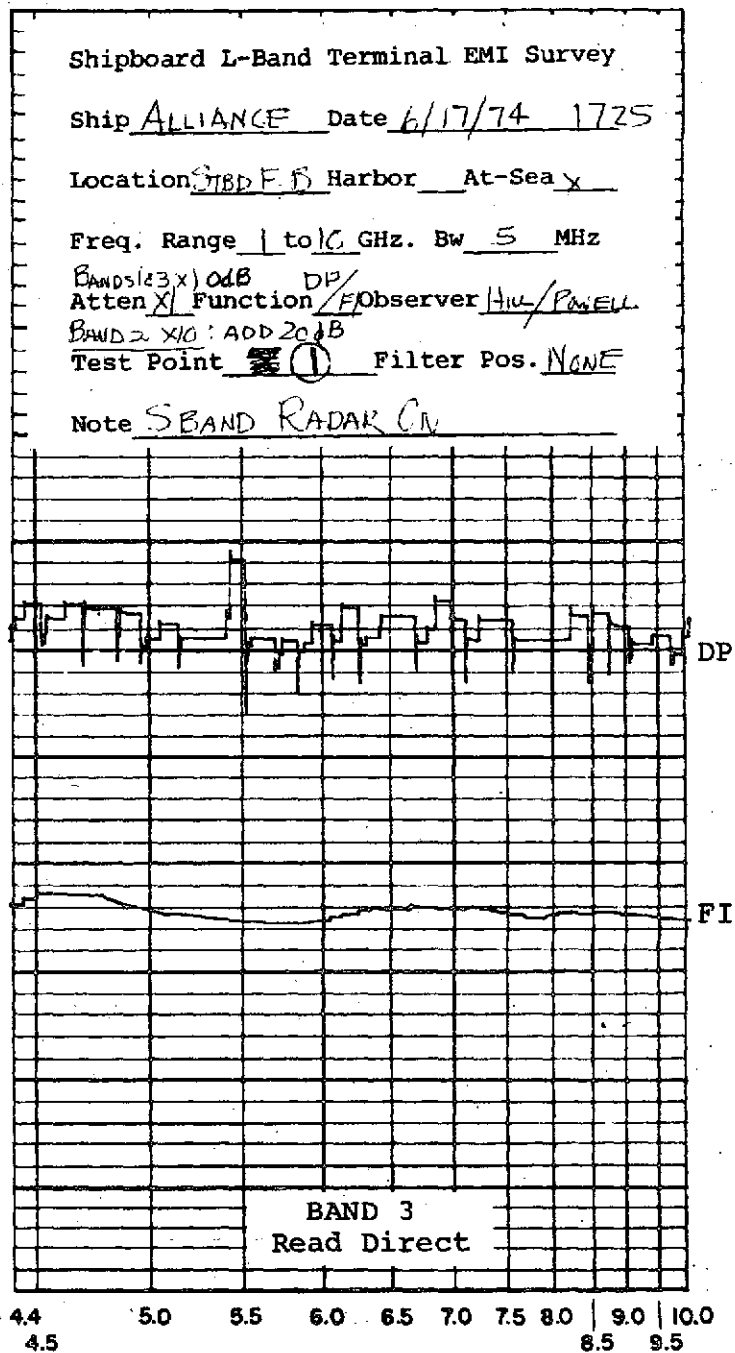
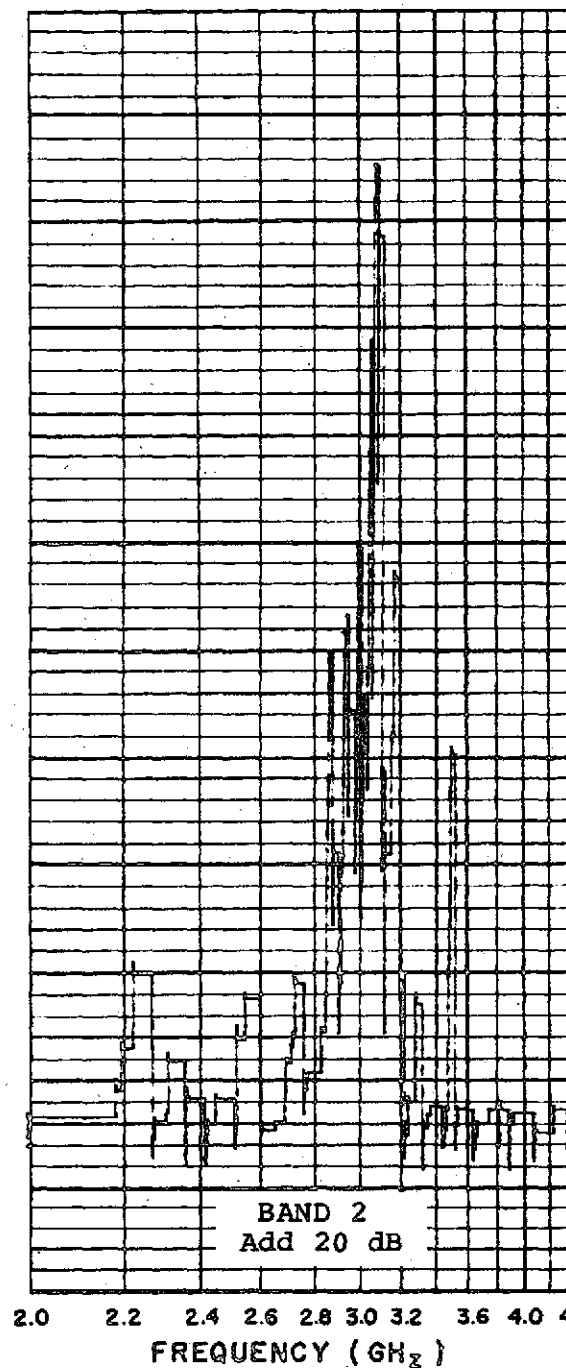


CHART C-5



dB
60

55

50

45

40

35

30

25

20

15

10

5

0

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/92 1515

Location SEP. F.B. Harbor At-Sea 1

Freq. Range 1.3 to 1.9 GHz. Bw 5 MHz

Atten 0 Function DR Observer HILL/PWELL

Test Point (1) F.I. Filter Pos. CLT

Note SEA RADAR ON - AG L.P. FILTER

D.P.

F.I.

CHART C-6

FREQUENCY

(GHz)

C-10

dB
60

55

50

45

40

35

30

25

20

15

10

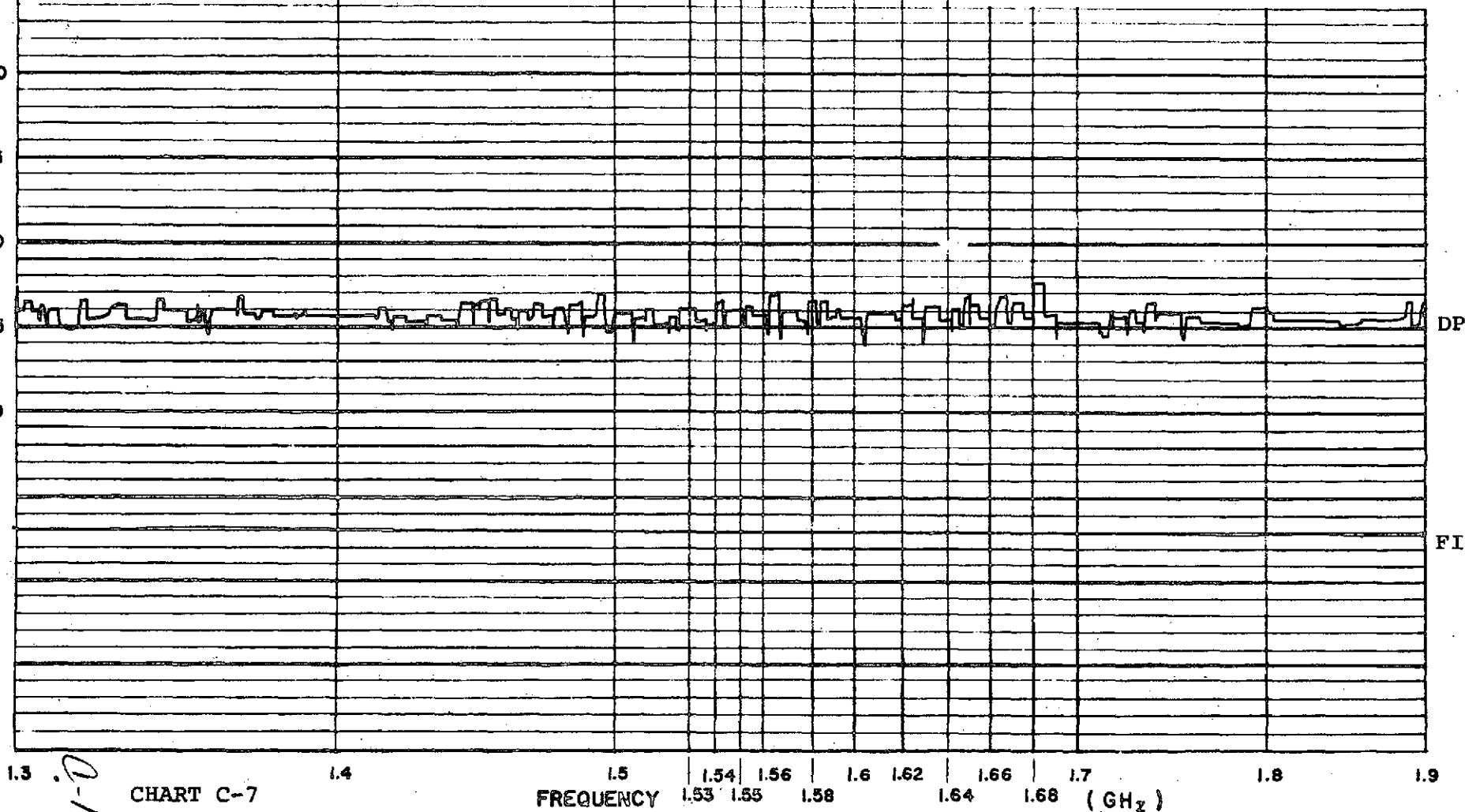
5

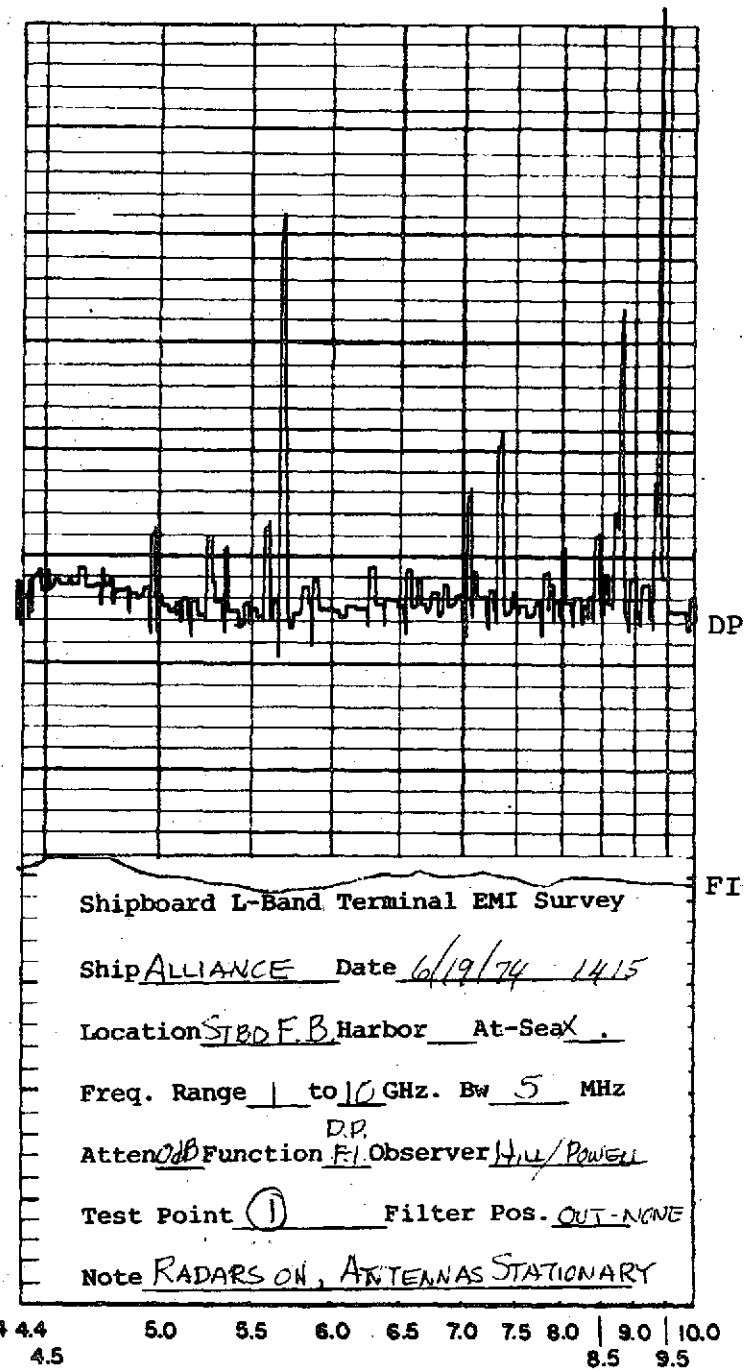
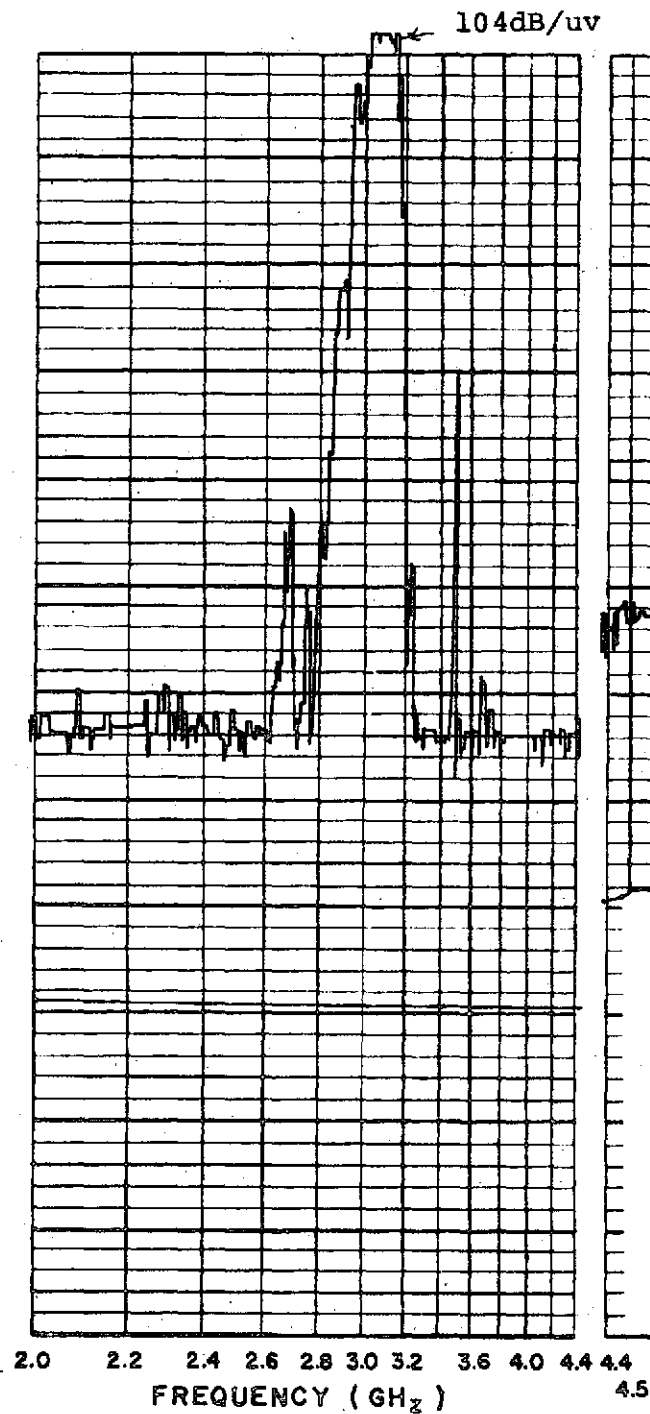
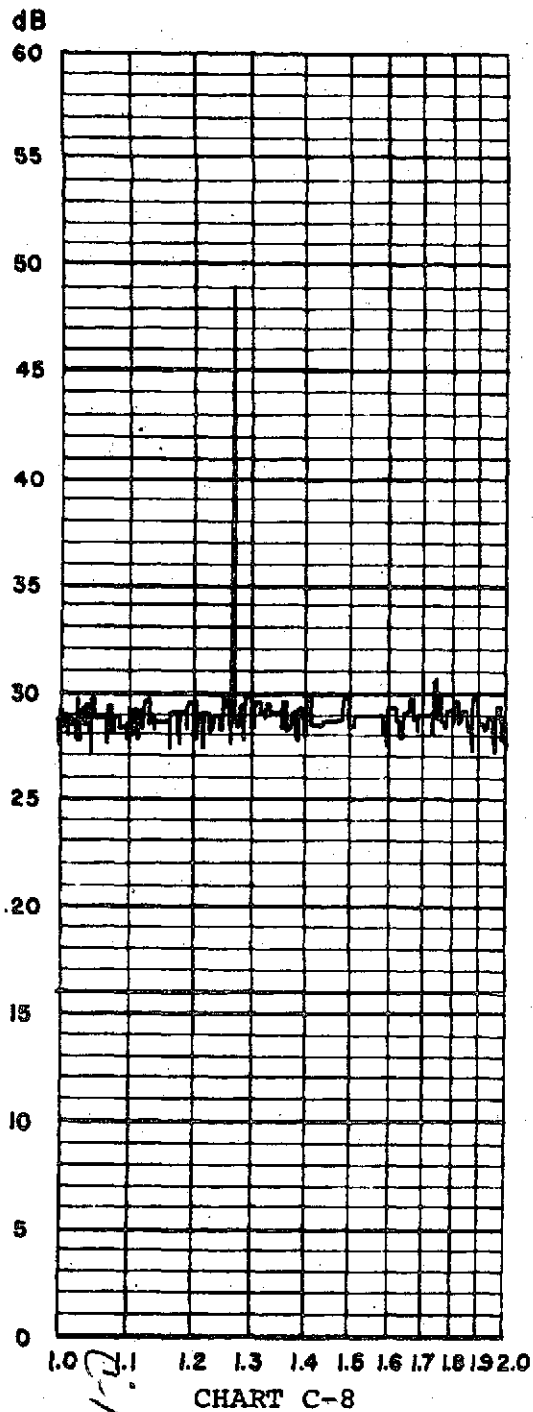
0

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1400Location STBD F.B. Harbor At-Sea ☒Freq. Range 1.3 to 1.9 GHz. Bw 5 MHzAtten 0 dB Function DP TDR Observer Hill/POWELLTest Point (1) Filter Pos. No. 1

4-5 DISK IN 1-2 AT HARBOR TIDE

Note BOTH HANDS ON. A-STOPPED



dB
60

55

50

45

40

35

30

25

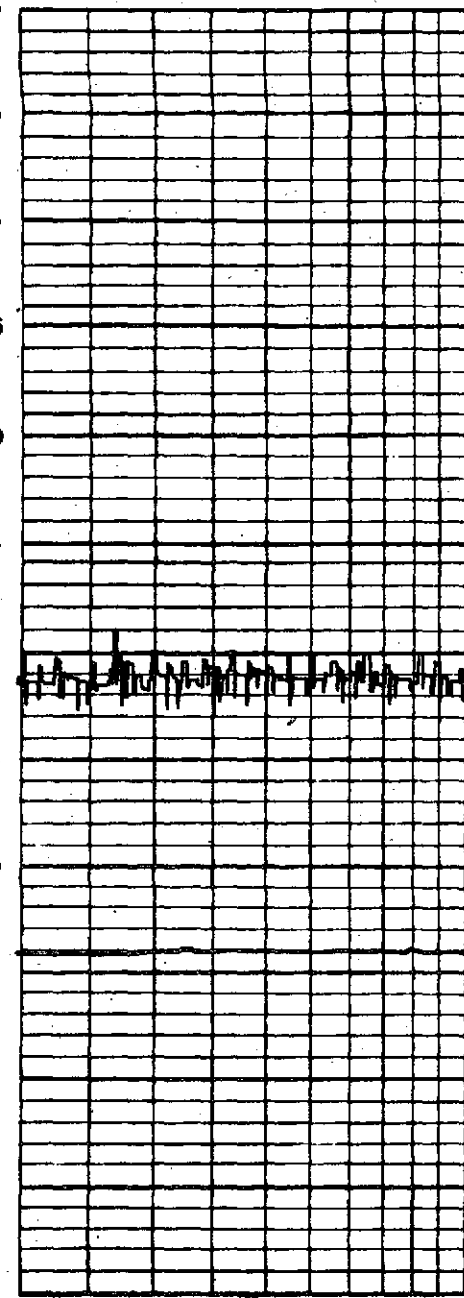
20

15

10

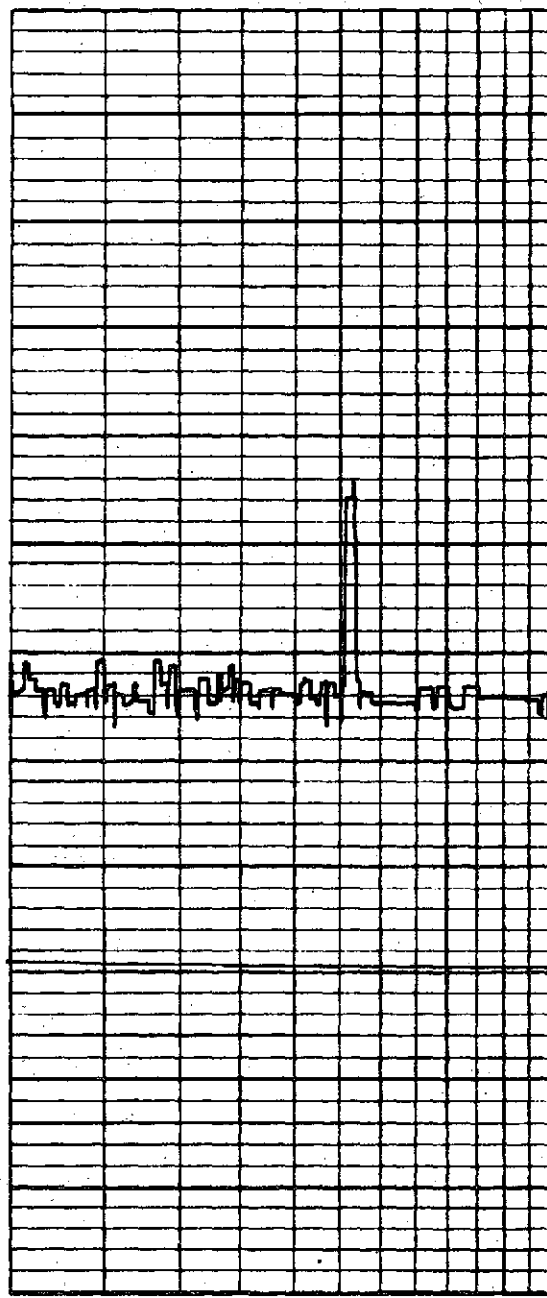
5

0



1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 2.0

CHART C-9



2.0 2.2 2.4 2.6 2.8 3.0 3.2 3.6 4.0 4.4 4.5

FREQUENCY (GHz)

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1426

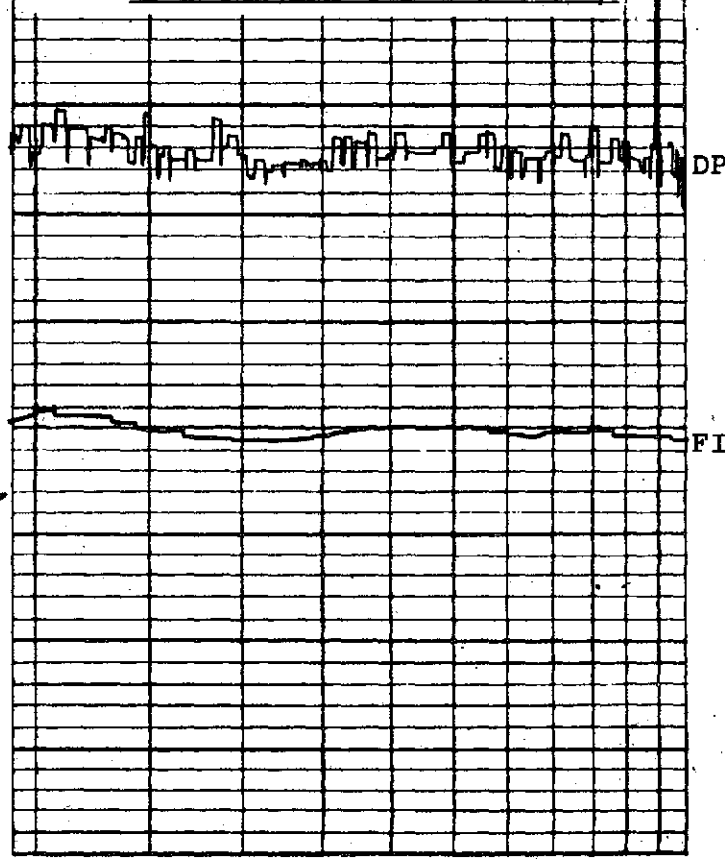
Location STBD F.B. Harbor At-Sea X

Freq. Range 1 to 10 GHz. Bw 5 MHz

Atten 0 dB Function DP Observer HILL/POWELL

Test Point 0 Filter Pos. OUT OF FILTER

Note RADARS ON, ANTENNAS STATIONARY



4.4 4.5 5.0 5.5 6.0 6.5 7.0 7.5 8.0 8.5 9.0 9.5 10.0

dB
60

55

50

45

40

35

30

25

20

15

10

5

0

1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 2.0

CHART C-10

2.0 2.2 2.4 2.6 2.8 3.0 3.2 3.6 4.0 4.4

FREQUENCY (GHz)

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/9/2010

Location STBD F.B Harbor At-Sea ☒

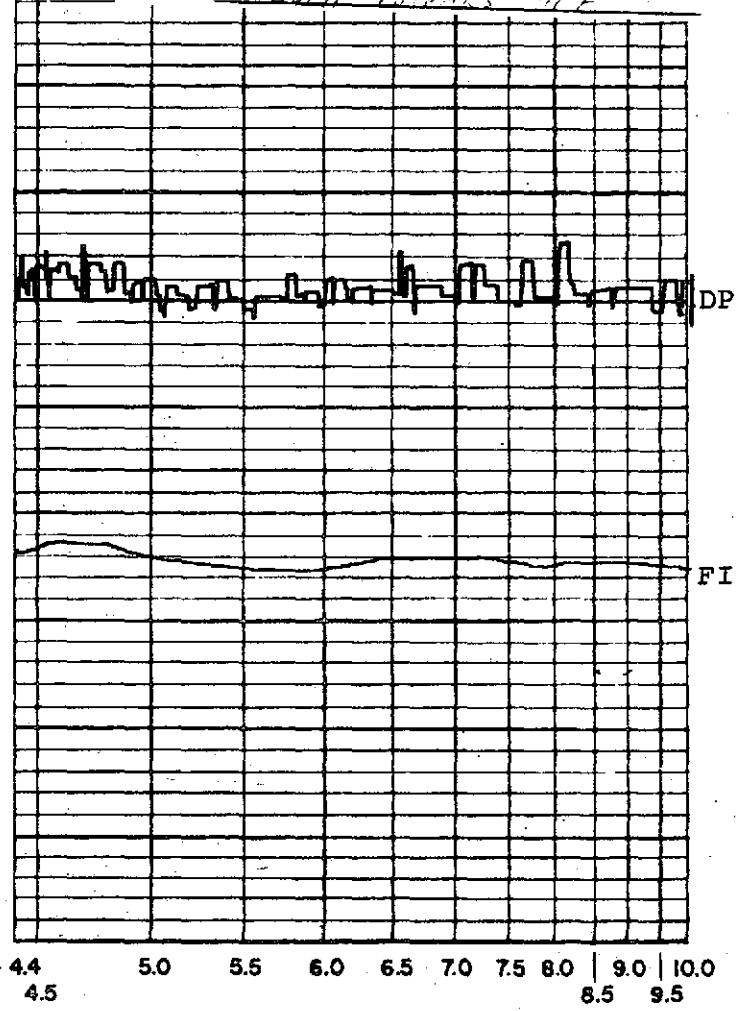
Freq. Range 1 to 10 GHz. Bw 5 MHz

Atten 0 dB Function DP Top Observer HAY/KAVEL

Test Point 2 FI BI Filter Pos. NONE

4-Ft Dish Pointed at 4-12-10

Note BOTH BANDS ARE



dB

60

55

50

45

40

35

30

25

20

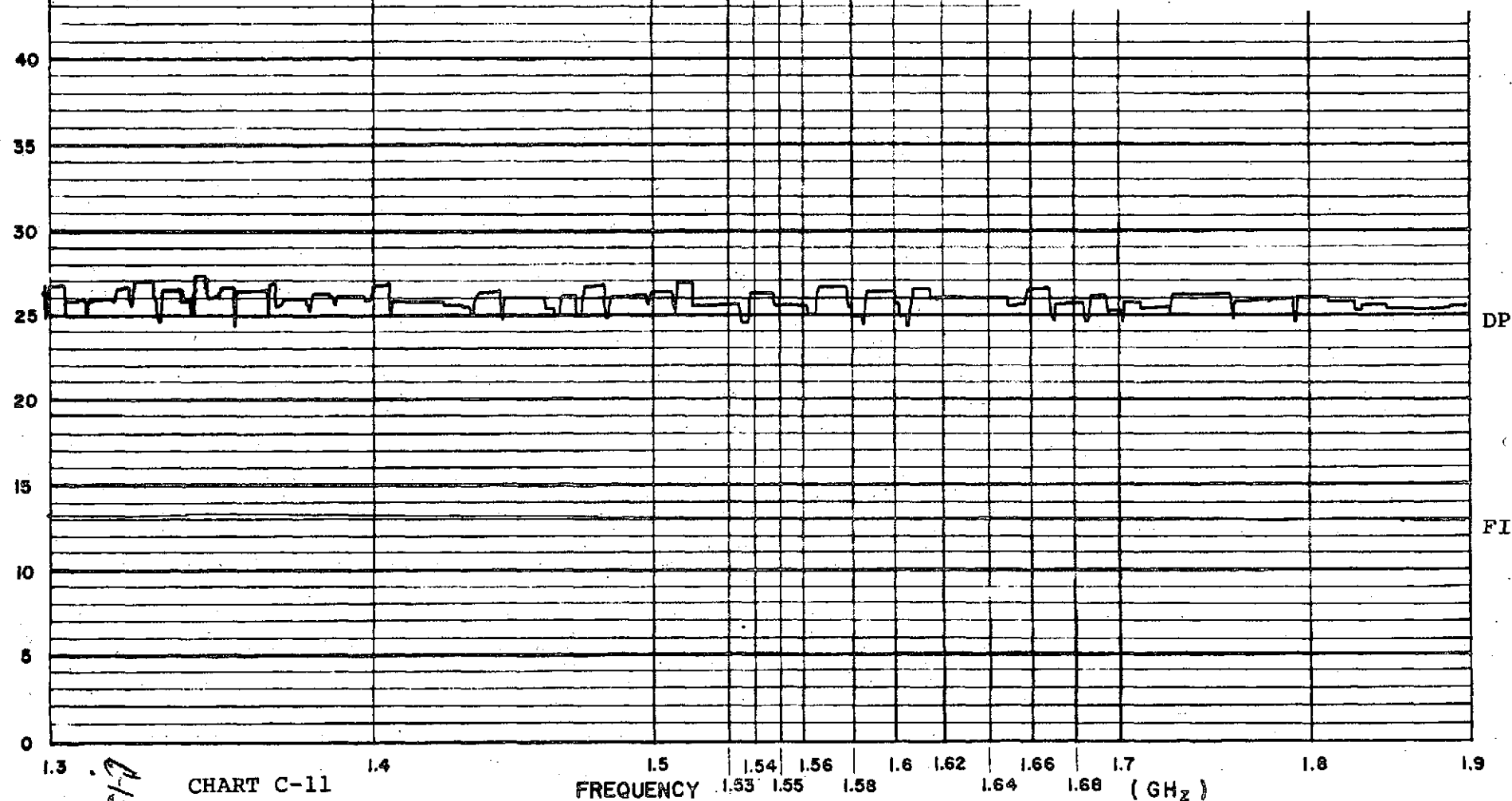
15

10

5

0

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1343Location STBD F.B. Harbor At-Sea ☒Freq. Range 1.3 to 1.9 GHz. Bw 5 MHzAtten 0 ^{dB} Function DP ^{TSC} Observer Hill/PavellTest Point (2) ^{FI 0.5} Filter Pos. None4 FT DISH POINTED AT RAIR ANTENNA
Note Both RAIR OFF

dB
60

55

50

45

40

35

30

25

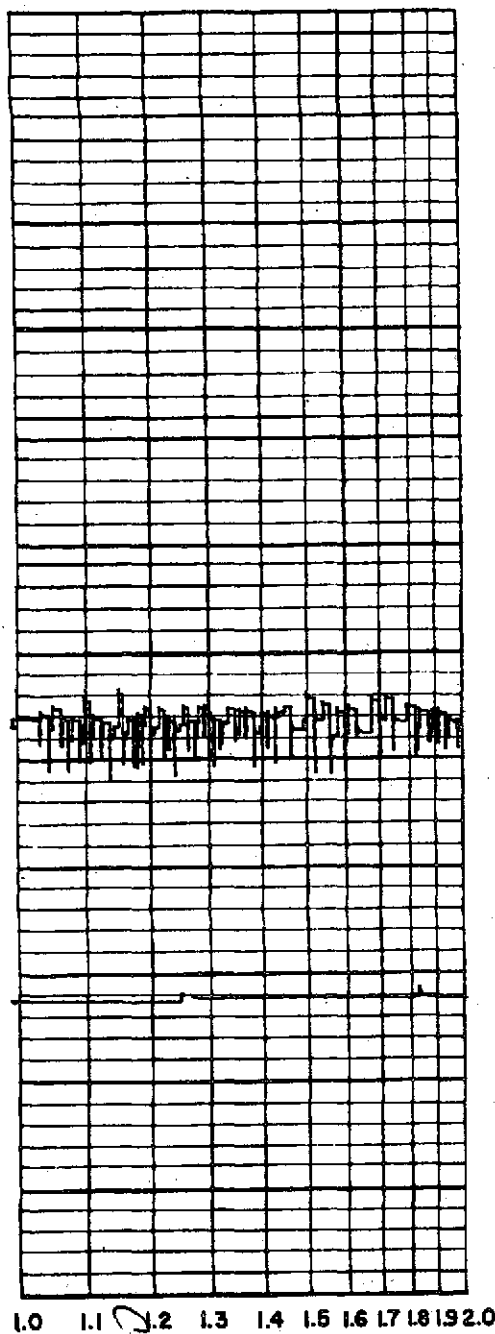
20

15

10

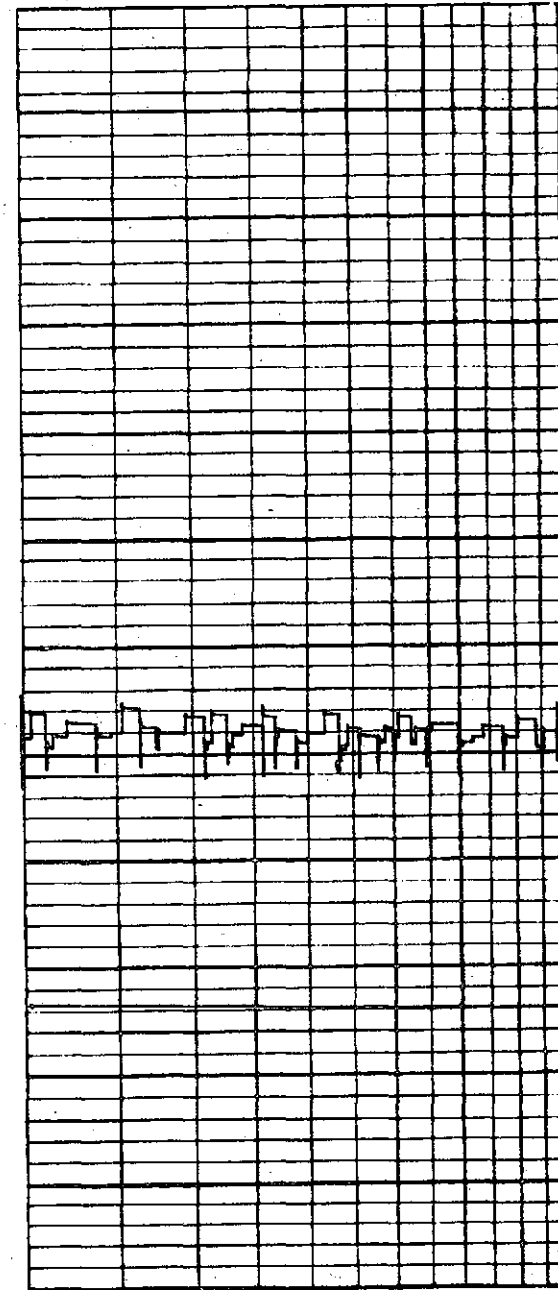
5

0



1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 2.0

CHART C-12



2.0 2.2 2.4 2.6 2.8 3.0 3.2 3.6 4.0 4.4 4.4

FREQUENCY (GHz)

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 1645

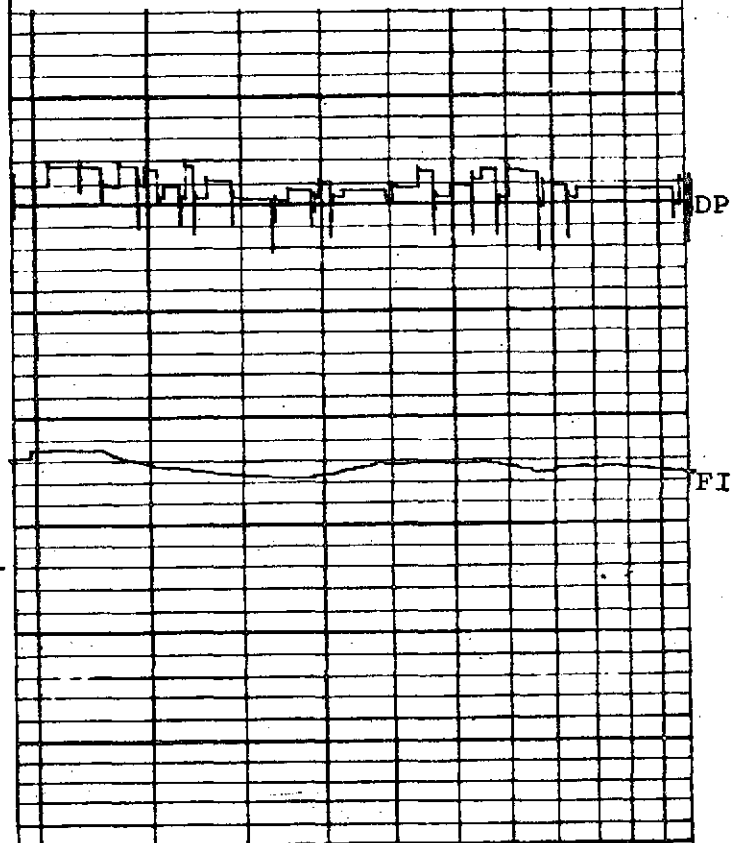
Location SIBD F.B. Harbor At-Sea x

Freq. Range 1 to 10 GHz. Bw 5 MHz

Atten 0dB Function DP Observer HILL/PINELL

Test Point (2) Filter Pos. NONE

Note 5-FAID RADAR CN



4.5 5.0 5.5 6.0 6.5 7.0 7.5 8.0 8.5 9.0 9.5 10.0

dB
60

55

50

45

40

35

30

25

20

15

10

5

0

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74

Location JTBD F.B. Harbor At-Sea X

Freq. Range 1.3 to 1.9 GHz. Bw 5 MHz

Atten X ^{0dB} Function DP Observer Hill/POWELL

Test Point (2) Filter Pos. OUT

Note S BAND RADAR CN

D.P.

F.I.

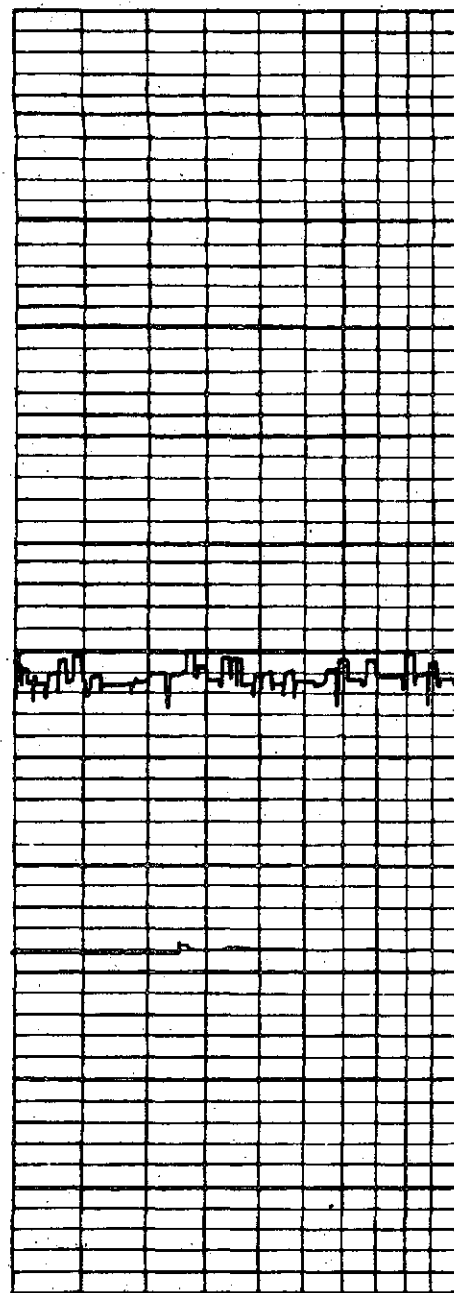
CHART C-13

FREQUENCY

1.3 1.4 1.5 1.53 1.54 1.55 1.56 1.58 1.6 1.62 1.64 1.66 1.68 1.7 1.8 1.9 (GHz)

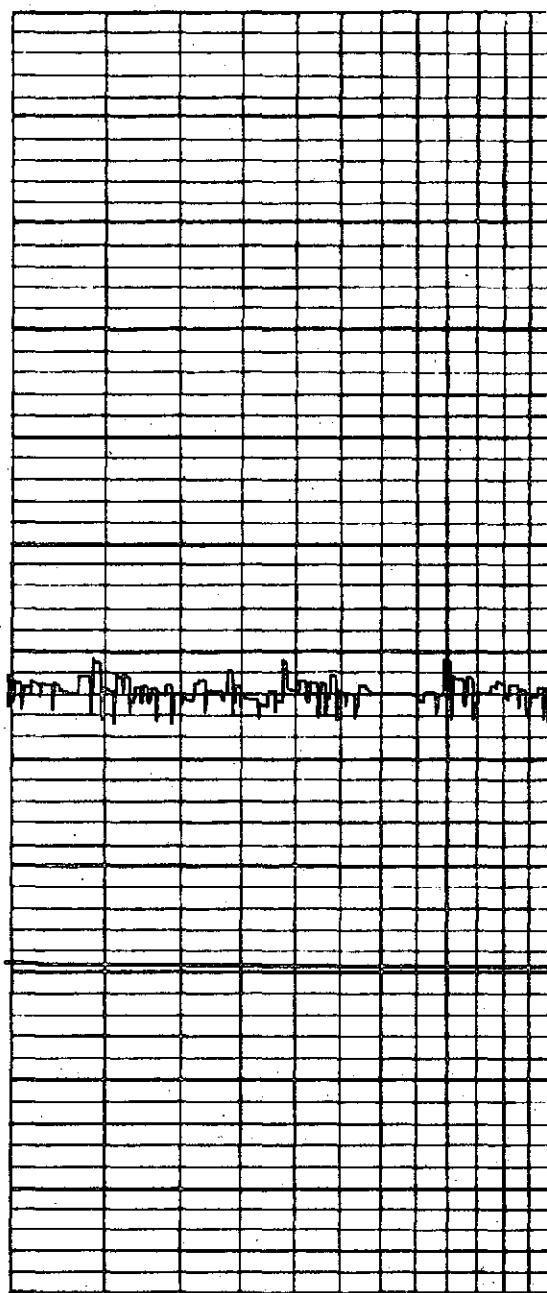
2-17

dB
60
55
50
45
40
35
30
25
20
15
10
5
0



1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 2.0

CHART C-14



2.0 2.2 2.4 2.6 2.8 3.0 3.2 3.6 4.0 4.4 4.4

FREQUENCY (GHz)

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1445

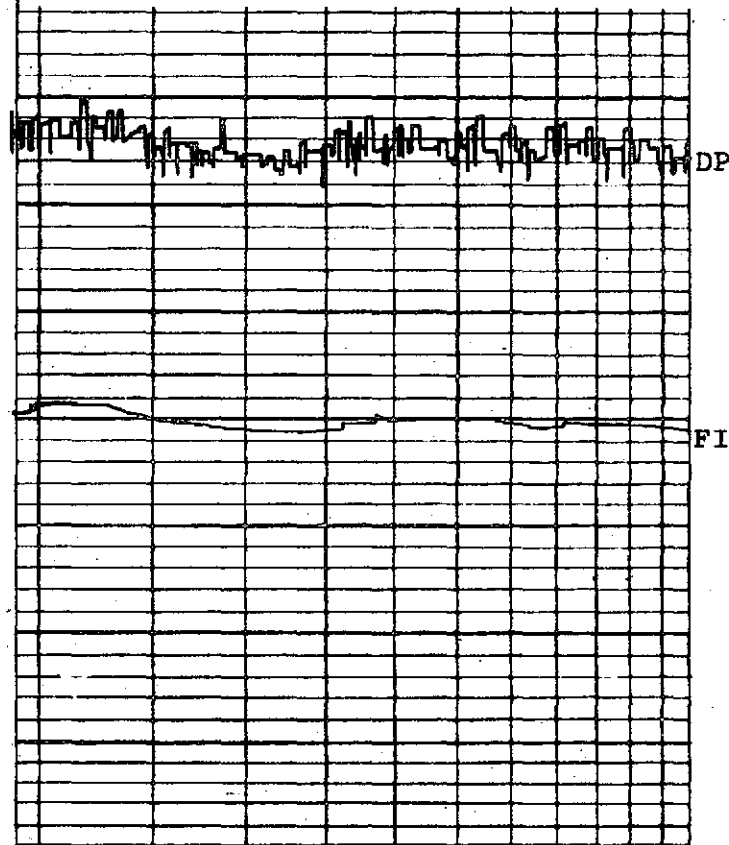
Location STBD F.B. Harbor At-Sea X

Freq. Range 1 to 10 GHz. Bw 5 MHz

Atten 0 dB Function DP Observer HILL/POWELL

Test Point (2) Filter Pos. 2 OUTPUT OF DX

Note RADARS ON; ANTENNAS STATIONARY



4.5 5.0 5.5 6.0 6.5 7.0 7.5 8.0 8.5 9.0 9.5 10.0

dB

60

55

50

45

40

35

30

25

20

15

10

5

0

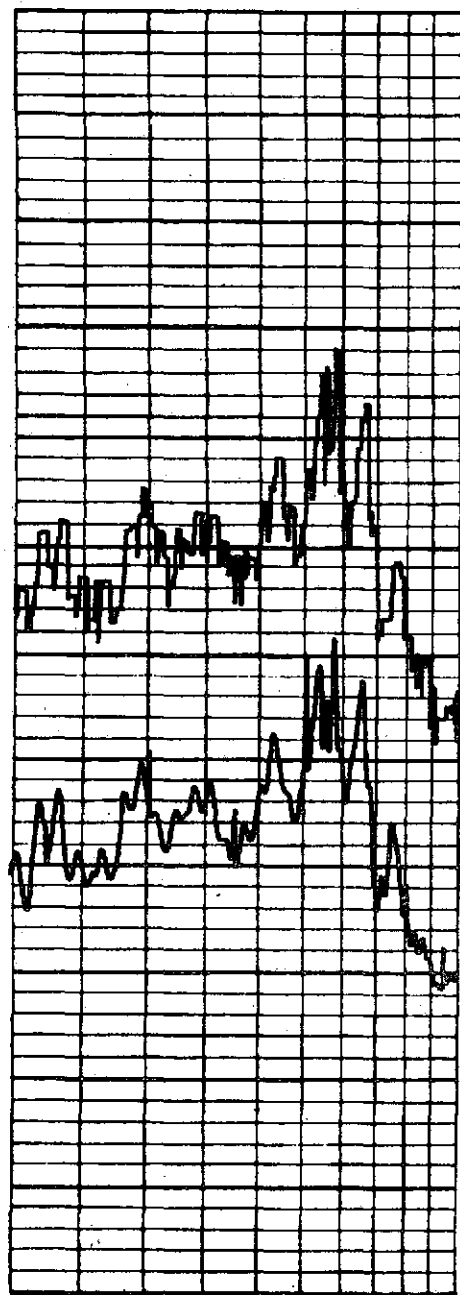


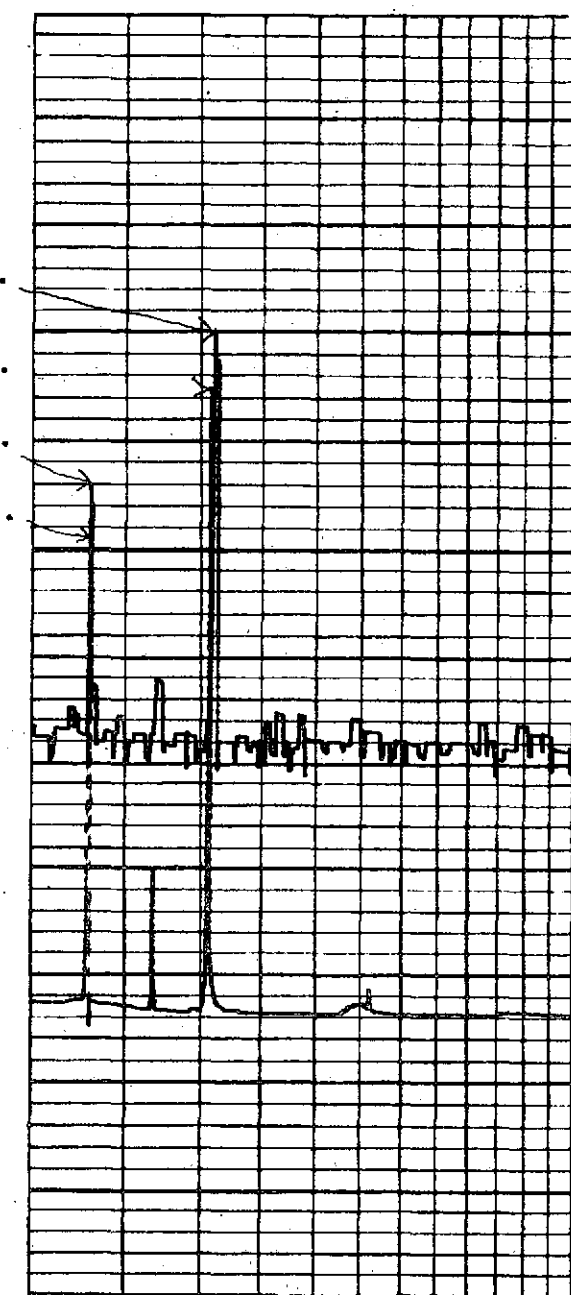
CHART C-15

D.P.

F.I.

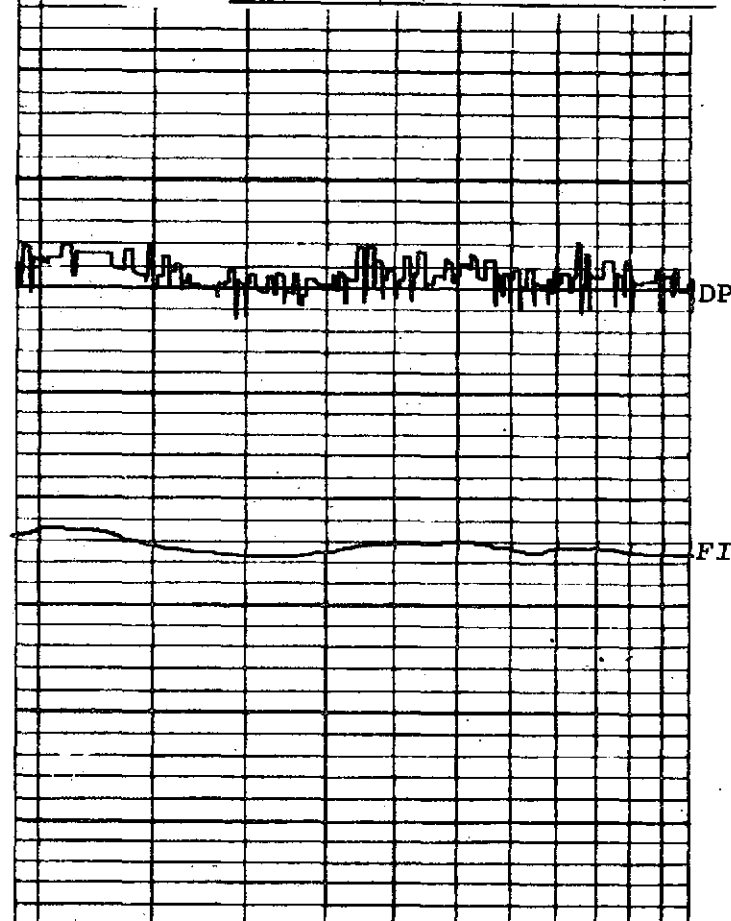
D.P.

F.I.



FREQUENCY (GHz)

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1235Location STED F.B. Harbor At-Sea ☒Freq. Range 1 to 10 GHz. Bw 5 MHzAtten 0 dB DP Top Observer Hu/PanzerTest Point (3) FI Bit Filter Pos. NONENote 4-FOOT DIZH POINTED AT RADAR
BOTH RADARS ARE OFF

FREQUENCY (GHz)

dB
60

55

50

45

40

35

30

25

20

15

10

5

0

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1255

Location SBD F.B. Harbor At-Sea ✓

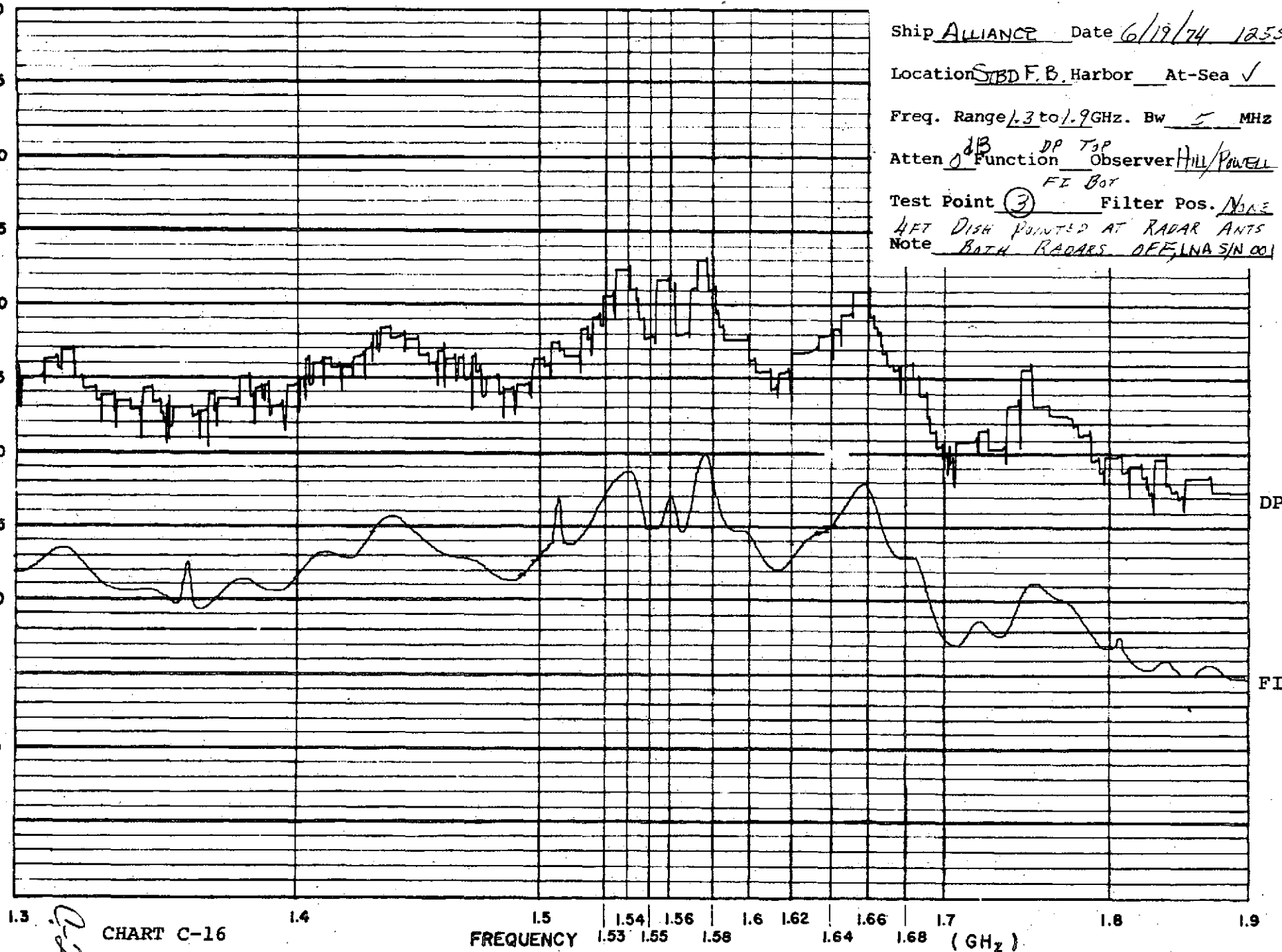
Freq. Range 1.3 to 1.9 GHz. Bw 5 MHz

Atten 0 ^{dB} Function DP TSP Observer Hill/Powell
FI BOT

Test Point (3) Filter Pos. None

4FT DISH POINTED AT RADAR ANTS

Note BOTH RADARS OFF LNA SIN COI



dB

60

55

50

45

40

35

30

25

20

15

10

5

0

Shipboard L-Band Terminal EMI Survey

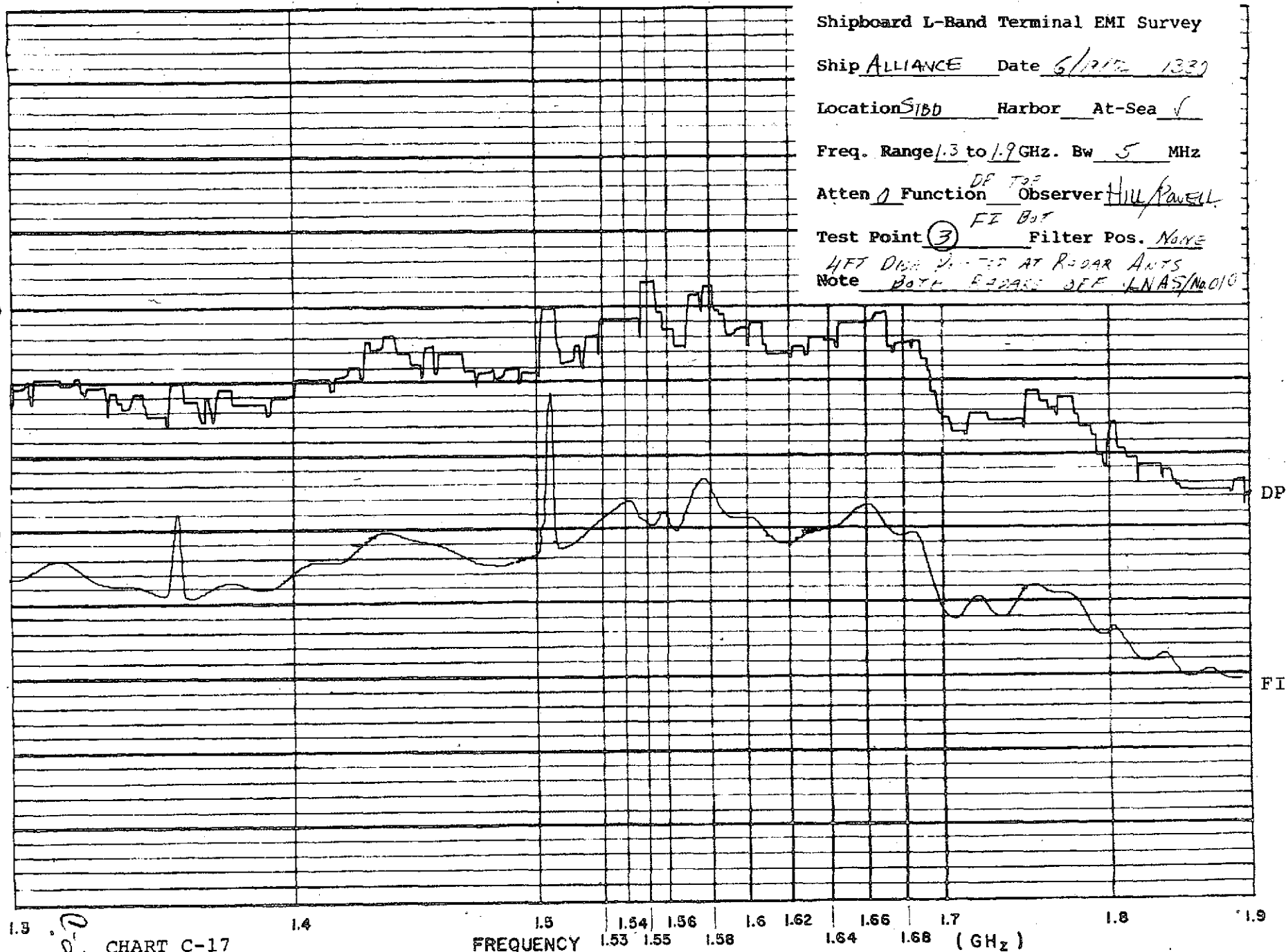
Ship ALLIANCE Date 6/17/72 1330Location SIBD Harbor At-Sea ☒Freq. Range 1.3 to 1.9 GHz. Bw 5 MHzAtten 1 Function ^{DF TOP} Observer Hill/PowellTest Point (3) ^{FE BOT} Filter Pos. NoiseNote 4FT DNR JITTER AT REAR ANTS
NOTE RECESS OFF LNAS/NaOIO

CHART C-17

FREQUENCY (GHz)

dB
60

55

50

45

40

35

30

25

20

15

10

5

0

1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 2.0

CHART C-18



2.0 2.2 2.4 2.6 2.8 3.0 3.2 3.6 4.0 4.4 4.5
FREQUENCY (GHz)

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74

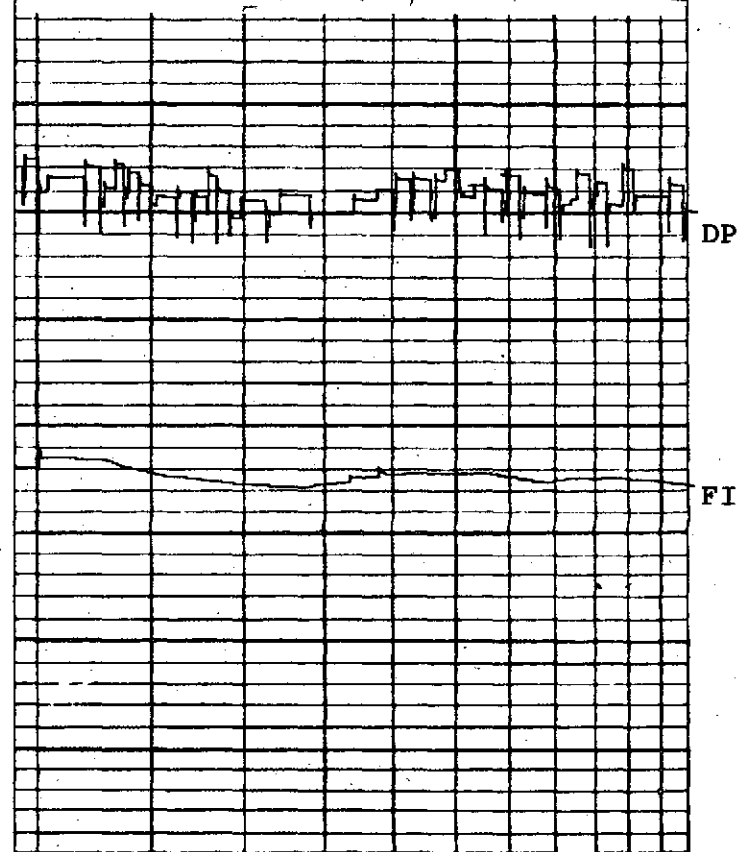
Location STBD F.B. Harbor At-Sea X

Freq. Range 1 to 10 GHz. Bw 5 MHz

Atten 9dB Function DP/FI Observer Hilly/POWELL

Test Point (3) Filter Pos. NONE

Note S BAND RADAR ON



4.5 5.0 5.5 6.0 6.5 7.0 7.5 8.0 8.5 9.0 9.5 10.0

dB
60

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74

Location STSD F.B. Harbor At-Sea X

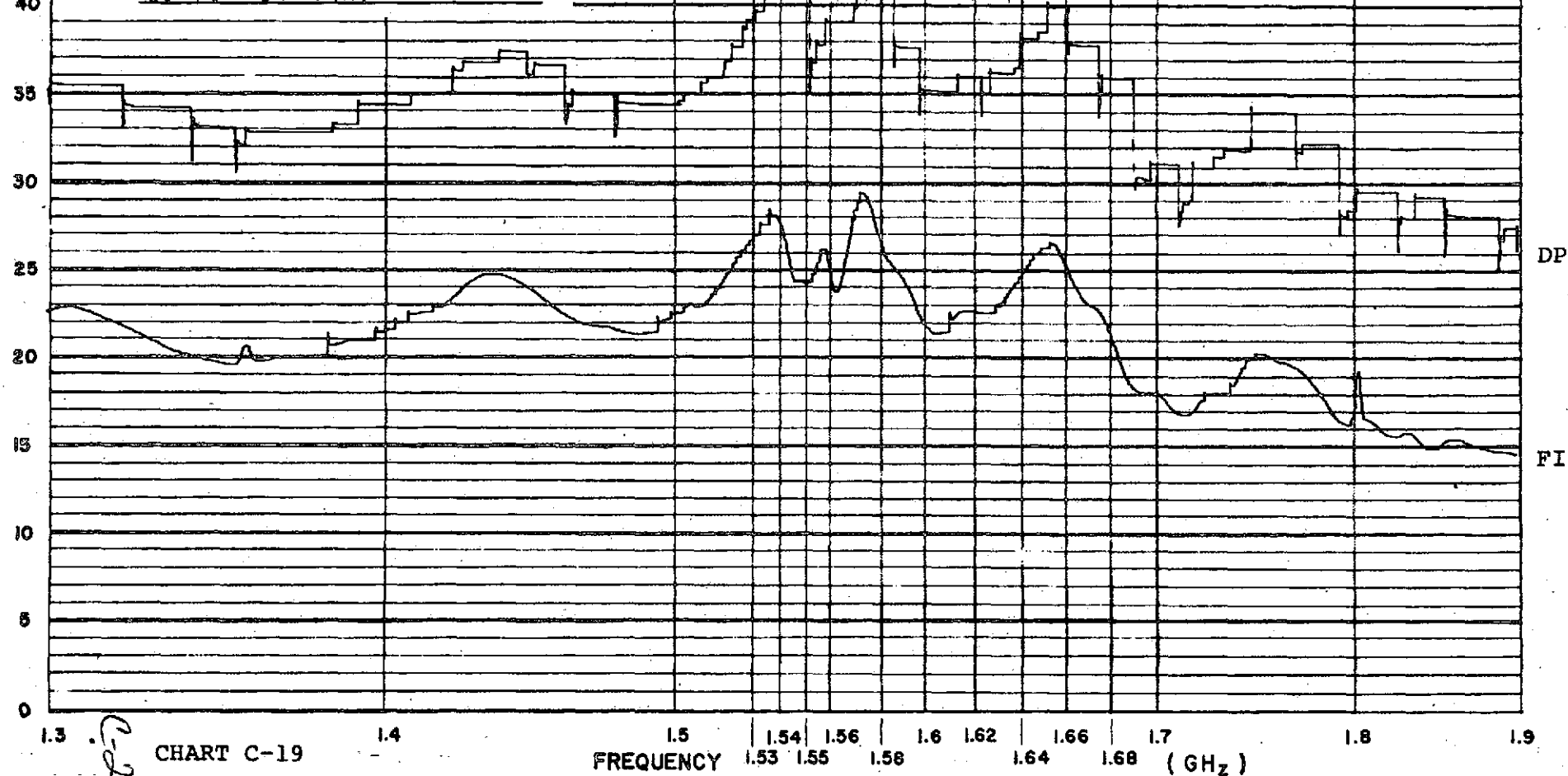
Freq. Range 1.3 to 1.9 GHz Bw 5 MHz

Atten 0dB Function DP/F Observer HILL/POWELL

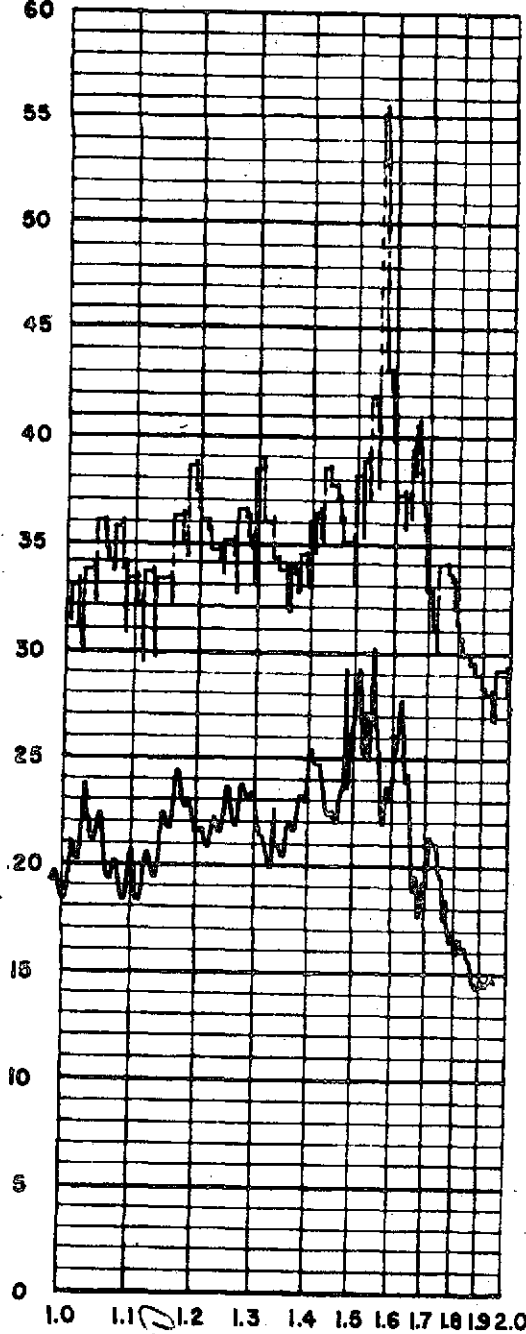
Test Point (3) Filter Pos. NONE

5 BAND RADAR ON

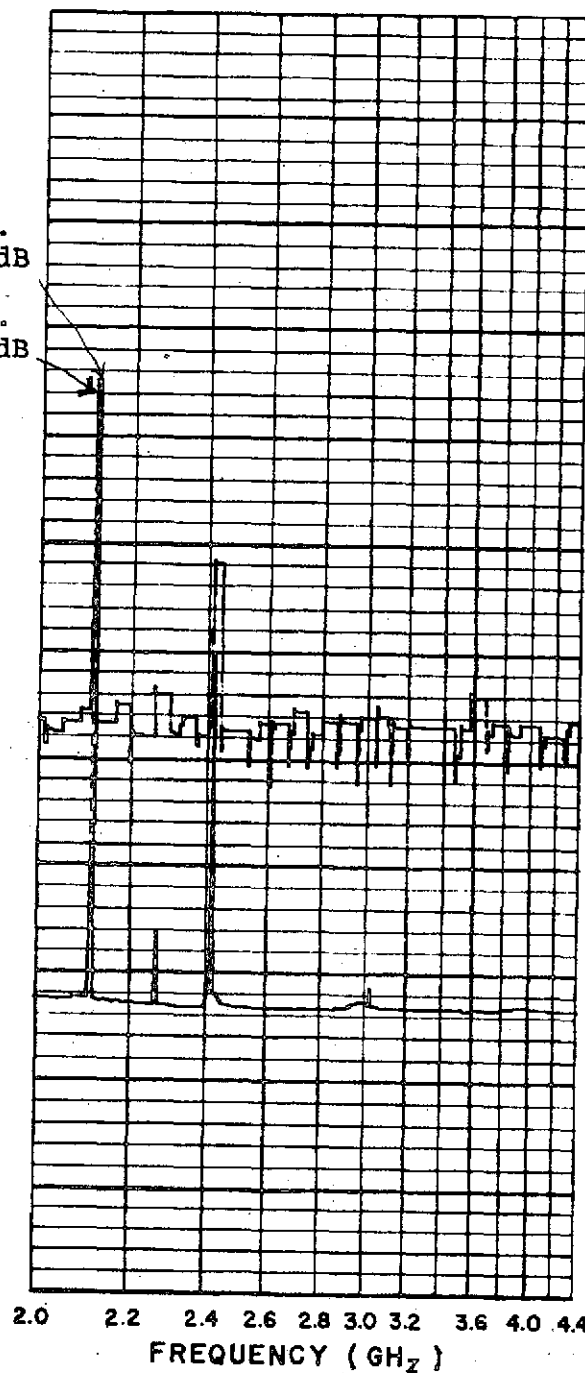
Note OUTPUT OF LNA



dB
60



D.P.
43 dB
F.I.
42 dB



Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 2230

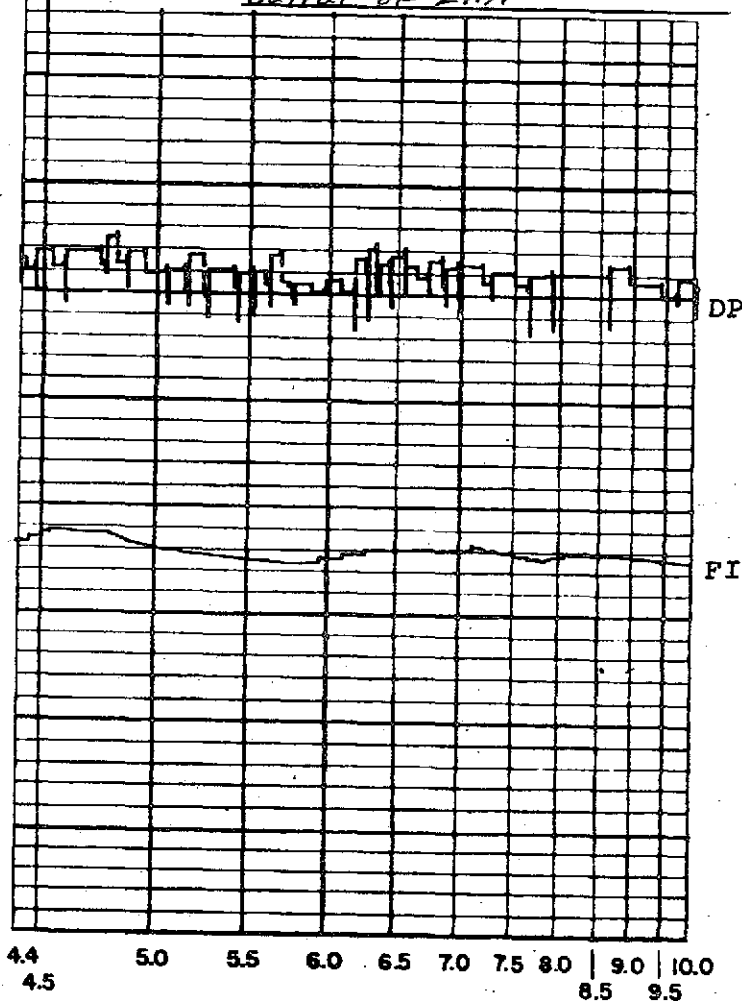
Location SBD.F.B. Harbor PHILADELPHIA At-Sea

Freq. Range 1 to 10 GHz. Bw 5 MHz

Atten 0 dB F.I. Bot. Observer ED

Test Point (3) Filter Pos. NONE

Note OUTPUT OF LNA



dB

60

55

50

45

40

35

30

25

20

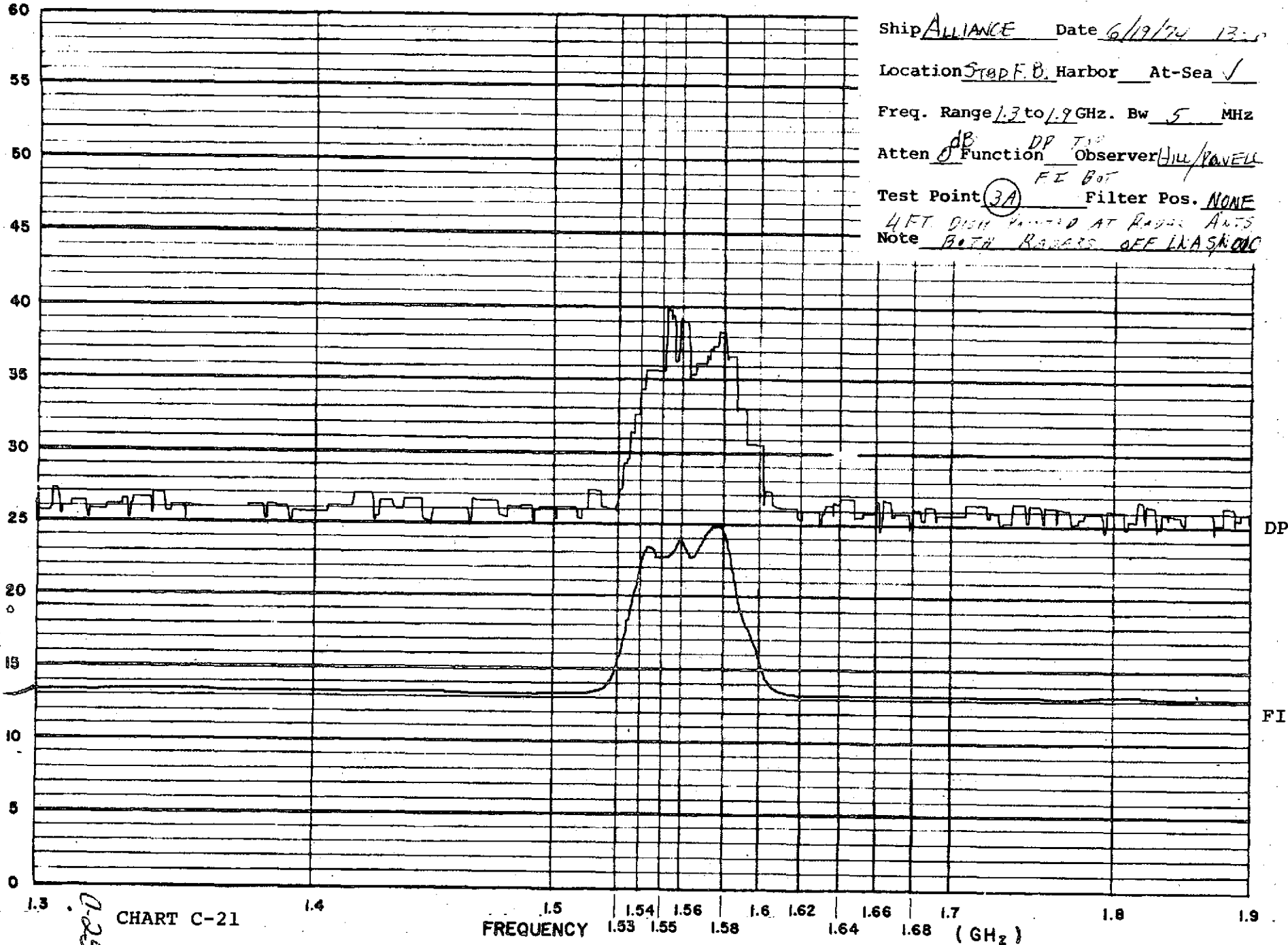
15

10

5

0

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 13:00Location Stad F.O. Harbor At-Sea ☒Freq. Range 1.3 to 1.9 GHz. Bw 5 MHzAtten 0 dB Function DP Observer Hill/PAVELLTest Point (3A) Filter Pos. NONE4 FT. DISK MOUNTED AT RADAR ANTS
Note BOTH RADARS OFF IN AS NOC

dB

60

55

50

45

40

35

30

25

20

15

10

5

0

Shipboard L-Band Terminal EMI Survey

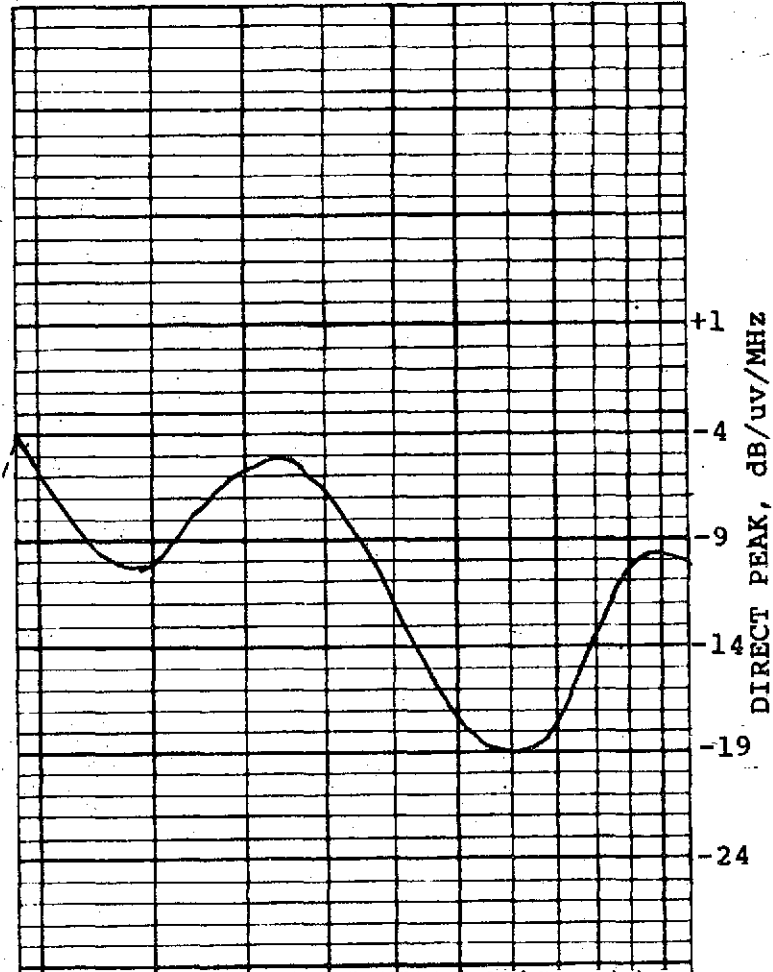
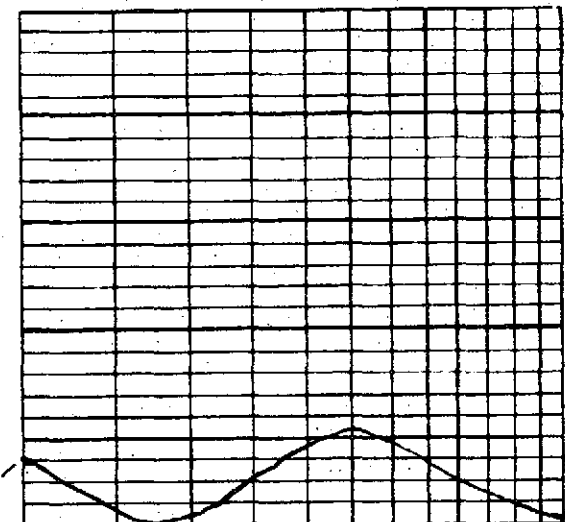
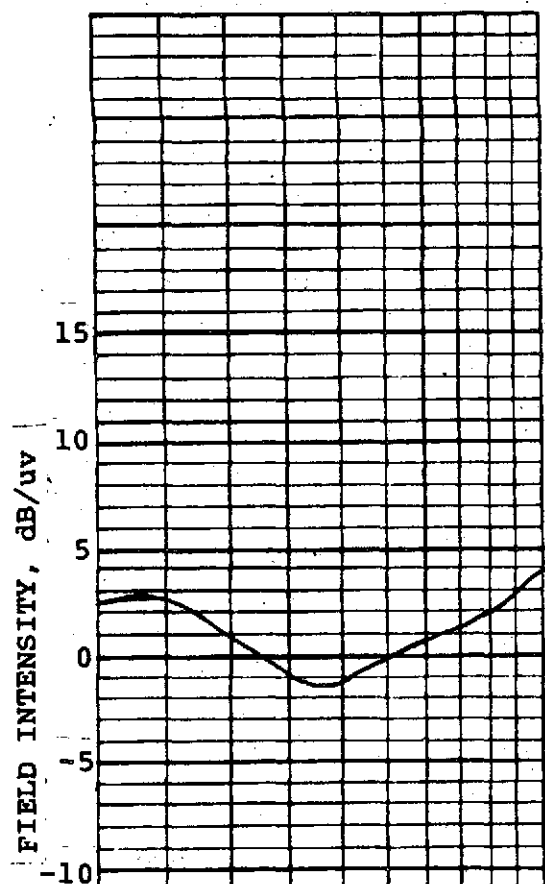
Ship ALLIANCE Date 6/17/74Location STED. F.B. Harbor At-Sea XFreq. Range 1.3 to 1.9 GHz. Bw 5 MHzAtten 0dB Function D.P./F.I. Observer HILL/POWELLTest Point _____ Filter Pos. NONENote 5 BAND RADAR ON
TAKEN ON XMITT PORT OF DUPLEXER

D.P.

F.I.

1.3 1.4 1.5 1.53 1.54 1.55 1.56 1.58 1.6 1.62 1.64 1.66 1.68 1.7 1.8 1.9
FREQUENCY (GHz)

CHART C-22



ADJUSTMENT FACTOR FOR
SINGER STODDART NM-65T
AS A TWO TERMINAL VOLTMETER
FIELD INTENSITY (FI) FUNCTION,
DIRECT PEAK (DP) FUNCTION.

1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 2.0
CHART C-23

2.0 2.2 2.4 2.6 2.8 3.0 3.2 3.6 4.0 4.4 4.5
FREQUENCY (GHz)

4.5 5.0 5.5 6.0 6.5 7.0 7.5 8.0 8.5 9.0 9.5 10.0

Spectrum Display C-1

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 ²⁰²⁰~~1955~~
2.07 to 6.15 GHz FULL BAND
 Center Freq. MHz, Bandwidth 300 KHz

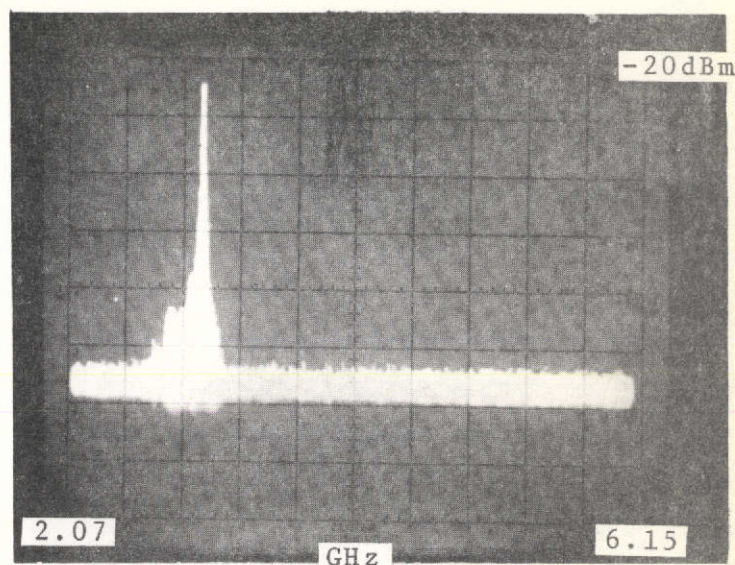
Scan Width MHz/div, Log Ref Level -20 dBm

Test Point # 1 4 FT DISH Filter Pos. NONE
S-BAND RADAR INTO 4 FT. DISH

Location STED F. B. Harbor At-Sea X
RADAR ANT. STATIONARY

Date Note Observer Hill/POWELL

PHOTO C-1



Spectrum Display C-2

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 ²¹¹⁵~~1956~~

Center Freq. MHz, Bandwidth 300 KHz

6.17 to 10.25 GHz FULL BAND

Scan Width MHz/div, Log Ref Level -30 dBm

X-BAND RADAR INTO 4 FT. DISH ANT.

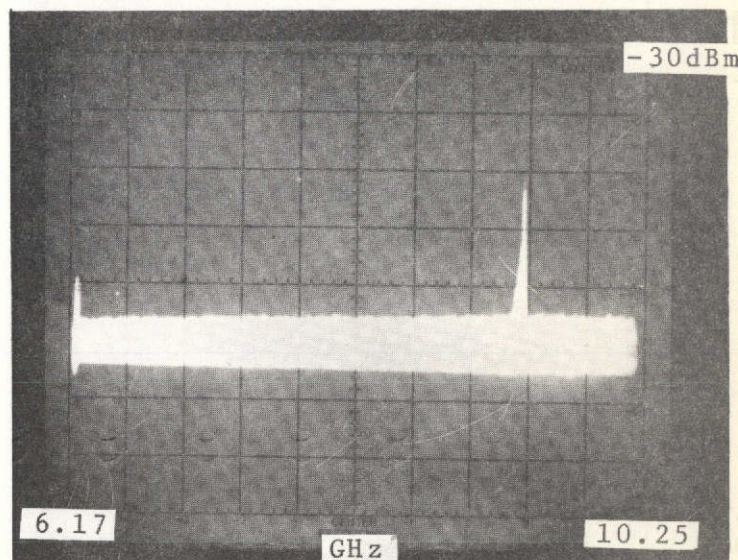
Test Point # 1 4 FT DISH Filter Pos. NONE

Location STED F. B. Harbor At-Sea X

RADAR ANT. STATIONARY

Date Note 5 SEC/DIV Observer

PHOTO C-2



Spectrum Display C-3

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 1715

Center Freq. 1.5 GHz, Bandwidth 100 KHz

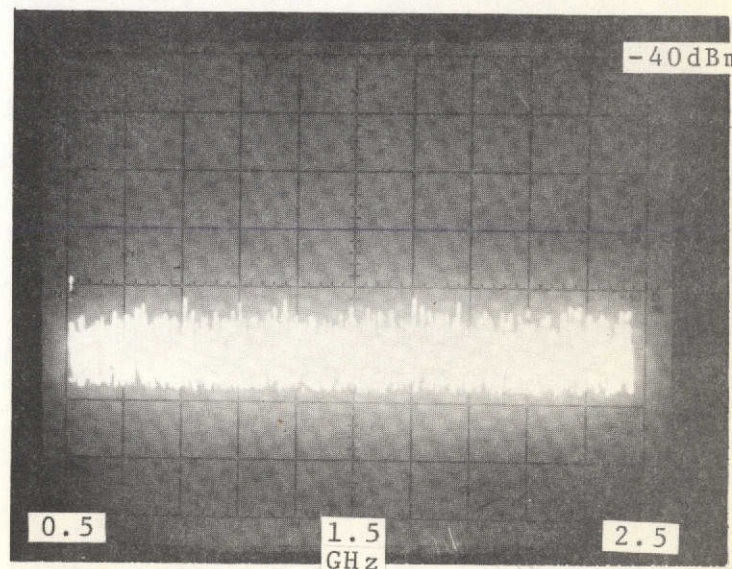
Scan Width 200 MHz/div, Log Ref Level -40 dBm

Test Point 2 Filter Pos. NONE

Location STED F. B. Harbor At-Sea X

Date S BAND Note RADAR ON Observer Hill/POWELL

PHOTO C-3



Spectrum Display C-4

HARBOR AMBIENT

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 2203

Center Freq. 1296 MHz, Bandwidth 100 KHz

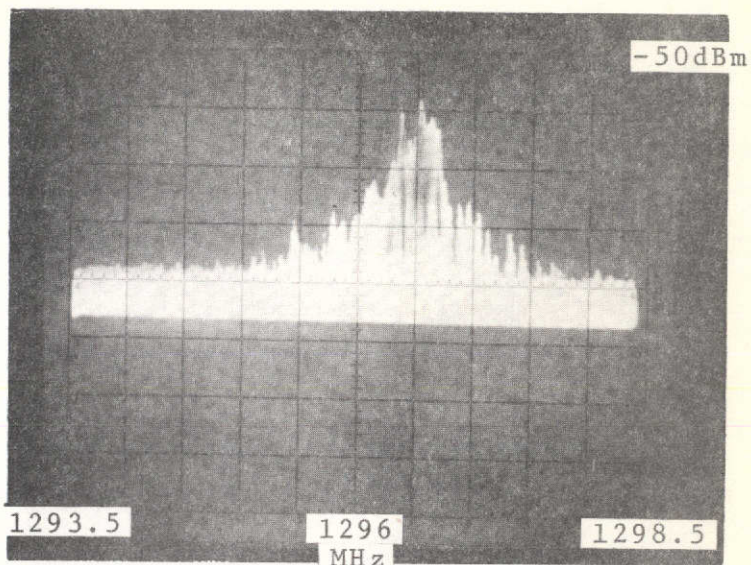
Scan Width 5 MHz/div, Log Ref Level -50 dBm

Test Point 1 Filter Pos. NONE

Location STBD FB Harbor PHILA At-Sea

Date Note BOTH RADARS OFF Observer EB
SHORE SIGNAL

PHOTO C-4



Spectrum Display C-5

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1520

Center Freq. 1500 MHz, Bandwidth 100 KHz

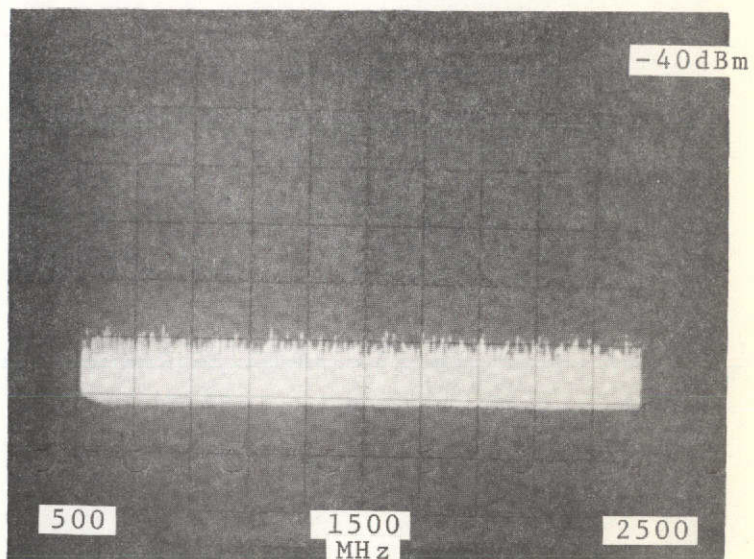
Scan Width 200 MHz/div, Log Ref Level -40 dBm

Test Point 1 Filter Pos. NONE

Location STBD F.B. Harbor At-Sea X

S BAND RADAR ON
Date Note Observer HILL/POWELL

PHOTO C-5



Spectrum Display C-6

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1527

Center Freq. 1500 MHz, Bandwidth 100 KHz

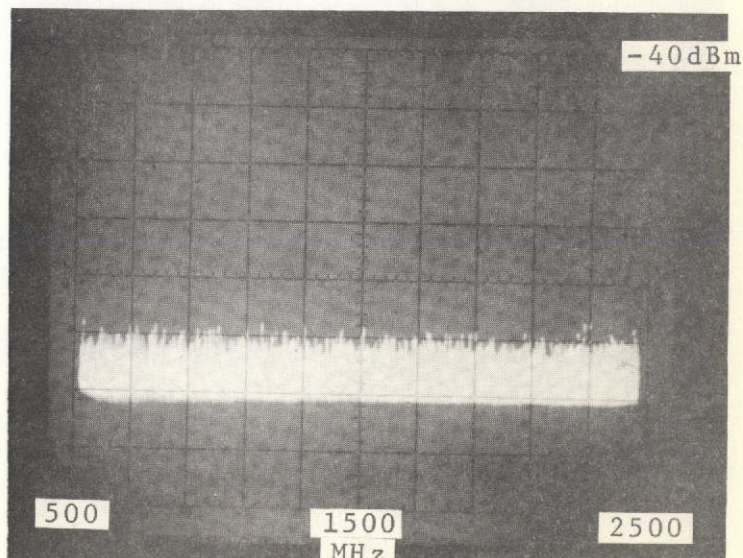
Scan Width 200 MHz/div, Log Ref Level -40 dBm

Test Point 1 Filter Pos. NONE

Location STBD F.B. Harbor At-Sea X

BOTH RADARS ON
Date Note Observer HILL/POWELL

PHOTO C-6



Spectrum Display C-7

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1946

Center Freq. 3050 MHz, Bandwidth 30 KHz

Scan Width 50 MHz/div, Log Ref Level -30 dBm

Test Point 1 Filter Pos. NONE

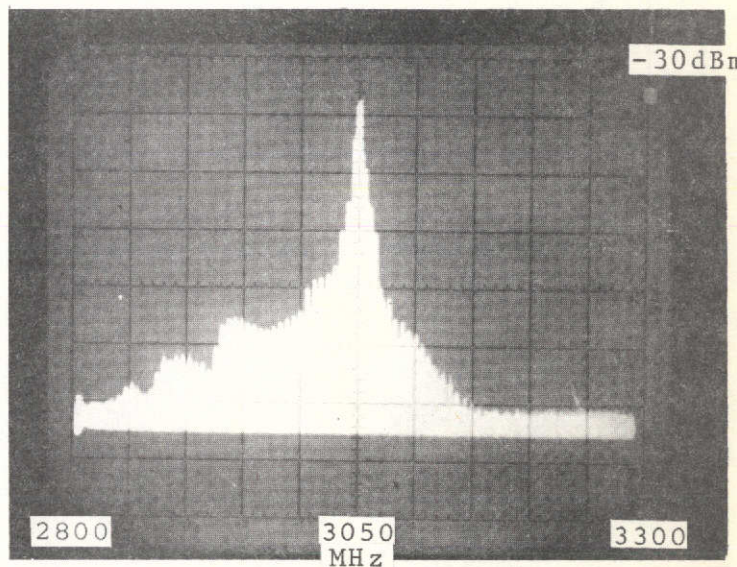
S BAND RADAR INTO 4 FT DISH

Location STBD F. B. Harbor At-Sea ☒

RADAR ANT. STATIONARY

Date 6/19/74 Note SCAN TIME 1 SEC/DIV Observer HILL/POWELL

PHOTO C-7



Spectrum Display C-8

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 2000 Hr

Center Freq. 3060 MHz, Bandwidth 100 KHz

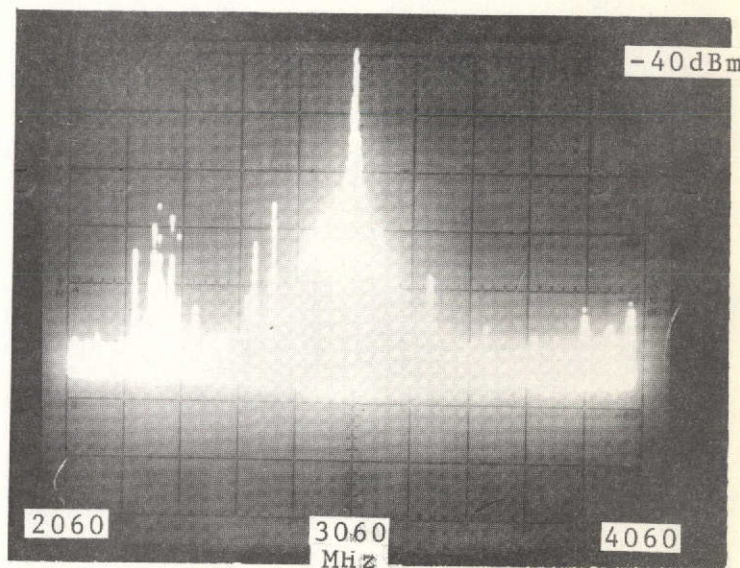
Scan Width 200 MHz/div, Log Ref Level -40 dBm

Test Point 1 Filter Pos. NONE

Location STBD F. B. Harbor IN RIVER At-Sea ☐

Date S BAND Note RADAR ON Observer HILL/POWELL

PHOTO C-8



C-30

Spectrum Display C-9

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 1900

Center Freq. 1.5 GHz, Bandwidth 100 KHz

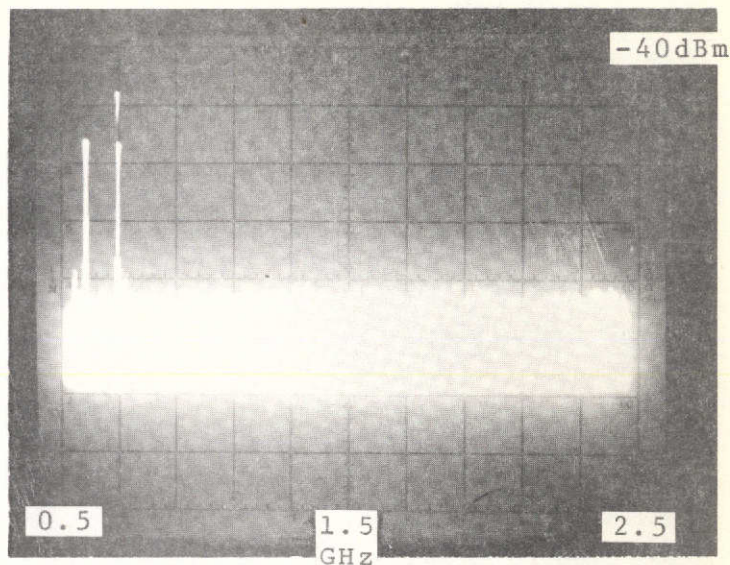
Scan Width 200 MHz/div, Log Ref Level -40dBm

Test Point 1 Filter Pos. NONE

Location STBD F.B. Harbor At-Sea

Date S BAND Note RADAR ON Observer HILL/POWELL

PHOTO C-9



Spectrum Display C-10

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 1714

Center Freq. 1.559 GHz, Bandwidth 100 KHz

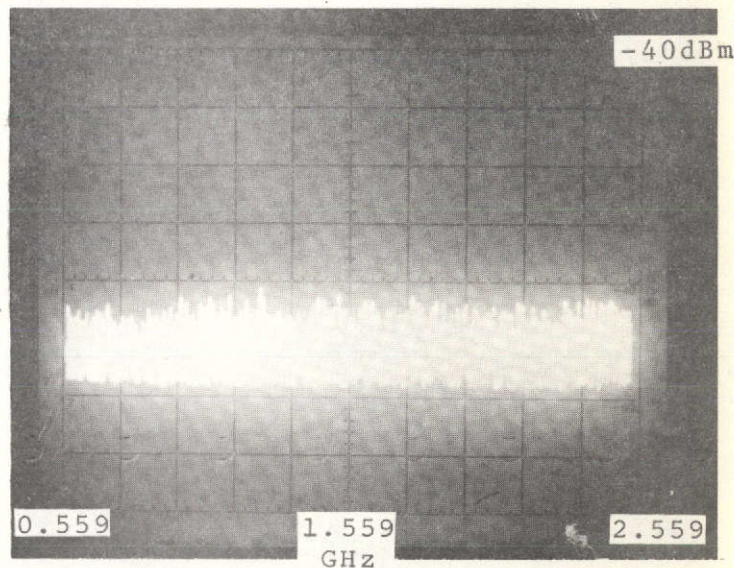
Scan Width 200 MHz/div, Log Ref Level -40dBm

Test Point 2 Filter Pos. NONE

Location STBD F.B. Harbor At-Sea

Date S BAND Note RADAR ON Observer HILL/POWELL

PHOTO C-10



Spectrum Display C-11

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74

Center Freq. 1.559 GHz, Bandwidth 100 KHz

Scan Width 200 MHz/div, Log Ref Level -40dBm

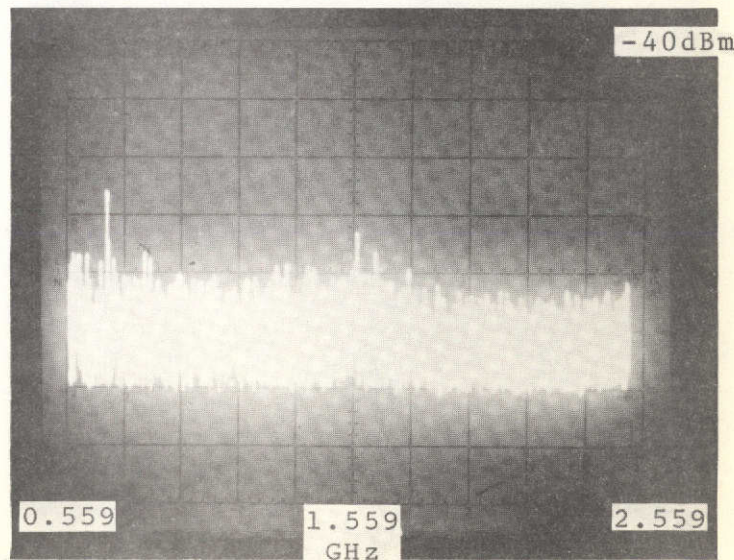
Test Point 3 Filter Pos. NONE

Location STBD F.B. Harbor At-Sea

Date 6/17/74 Note S BAND R-ON Observer HILL/POWELL

C-31

PHOTO C-11



Spectrum Display C-12

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 2010 Hrs

Center Freq. MHz, Bandwidth 100 KHz

2.07-6.15 GHz Full Band -40

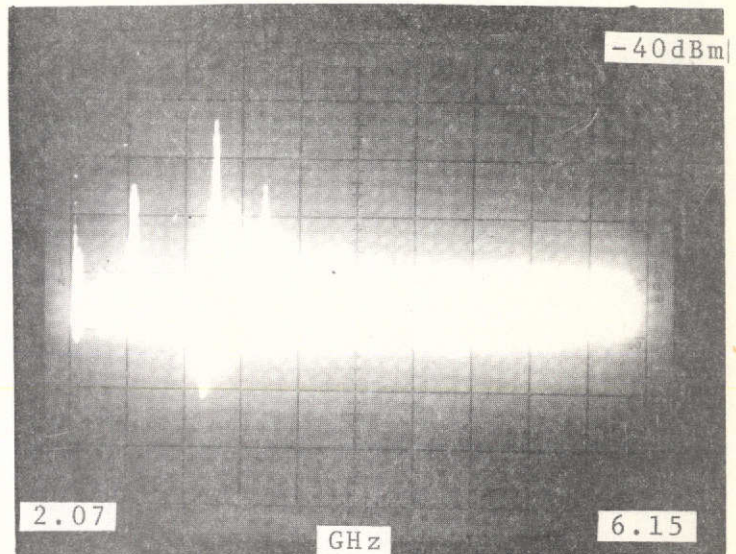
Scan Width MHz/div, Log Ref Level -20 dBm

Test Point 1 Filter Pos. NONE

Location STBD F.B. Harbor IN RIVER (DELAWARE)
At-Sea

Date S BAND Note RADAR ON Observer HILL/POWELL

PHOTO C-12



Spectrum Display C-13

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 1712

Center Freq. MHz, Bandwidth 100 KHz

2.07-6.15 GHz Full Band -50

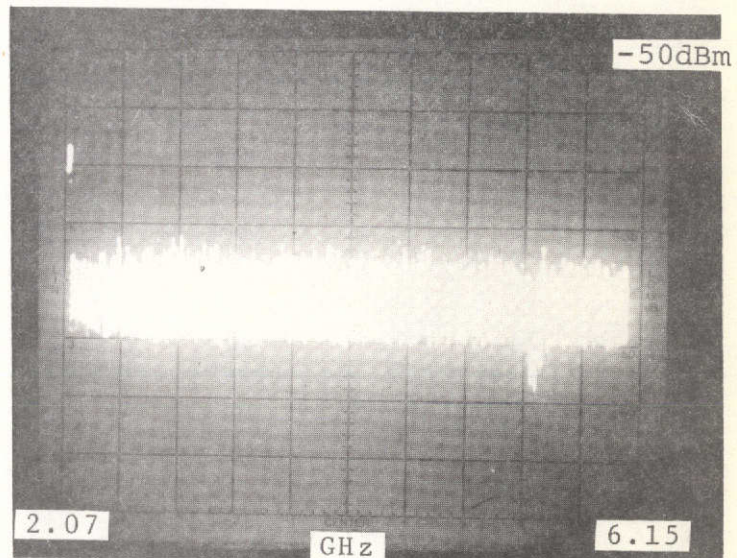
Scan Width MHz/div, Log Ref Level -40 dBm

Test Point 2 Filter Pos. NONE

Location STBD F.B. Harbor At-Sea ✓

Date S BAND Note RADAR ON Observer HILL/POWELL

PHOTO C-13



Spectrum Display C-14

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 1635

Center Freq. MHz, Bandwidth 100 KHz

2.07-6.15 GHz Full Band

Scan Width MHz/div, Log Ref Level -40 dBm

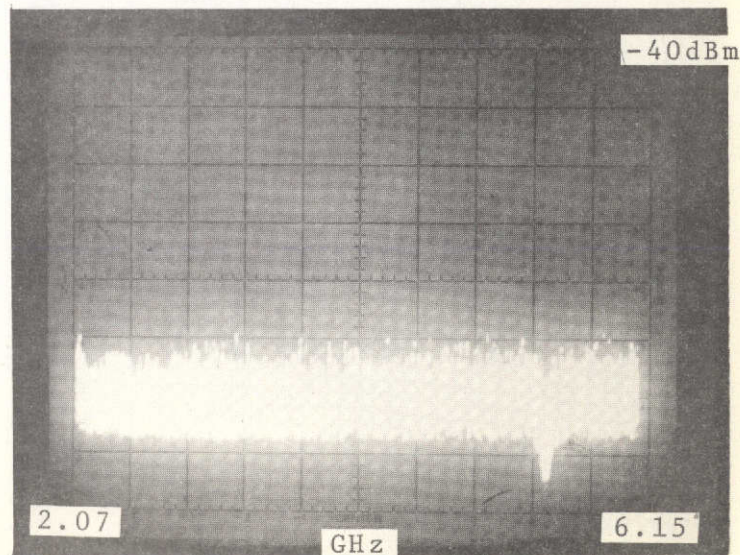
Test Point 3 Filter Pos. NONE

Location STBD F.B. Harbor At-Sea ✓

Date S-BAND Note RADAR ON Observer HILL/POWELL

C-32

PHOTO C-14



Spectrum Display C-15

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 2015 Hr

Center Freq. MHz, Bandwidth 100 KHz

6.17 - 10.25 GHz FULL BAND

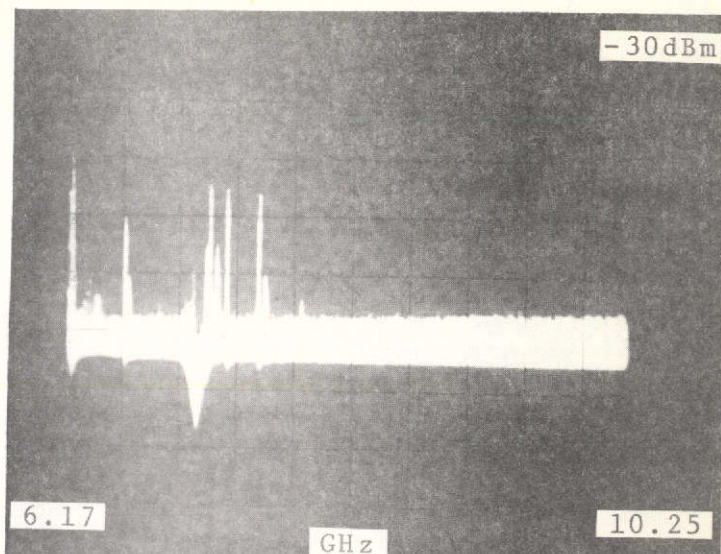
Scan Width MHz/div, Log Ref Level -30 dBm

Test Point 1 Filter Pos. NONE

Location STBD F.B. Harbor IN RIVER At-Sea

Date S BAND Note RADAR ON Observer Hill/Powell

PHOTO C-15



Spectrum Display C-16

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 1710

Center Freq. MHz, Bandwidth 100 KHz

6.17 - 10.25 GHz FULL BAND

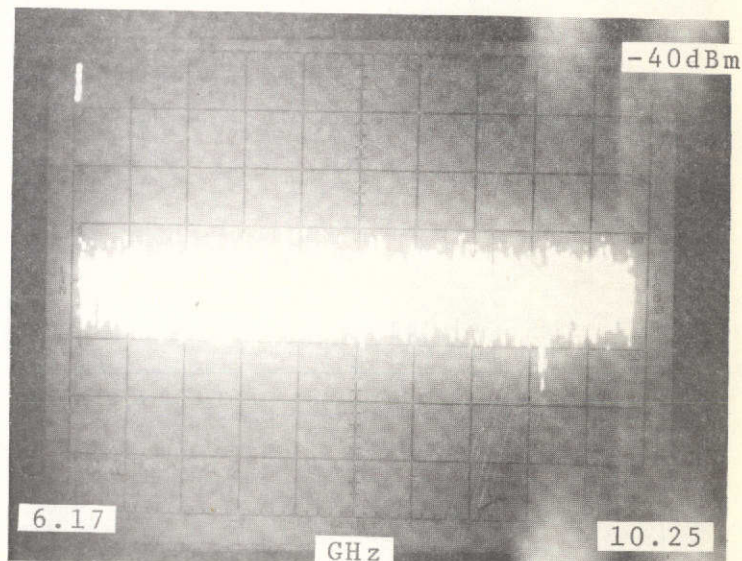
Scan Width MHz/div, Log Ref Level -40 dBm

Test Point 2 Filter Pos. NONE

Location STBD F.B. Harbor At-Sea X

Date S BAND Note RADAR ON Observer Hill/Powell

PHOTO C-16



Spectrum Display C-17

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 1640

Center Freq. MHz, Bandwidth 100 KHz

6.17 - 10.25 GHz FULL BAND

Scan Width MHz/div, Log Ref Level -20 dBm

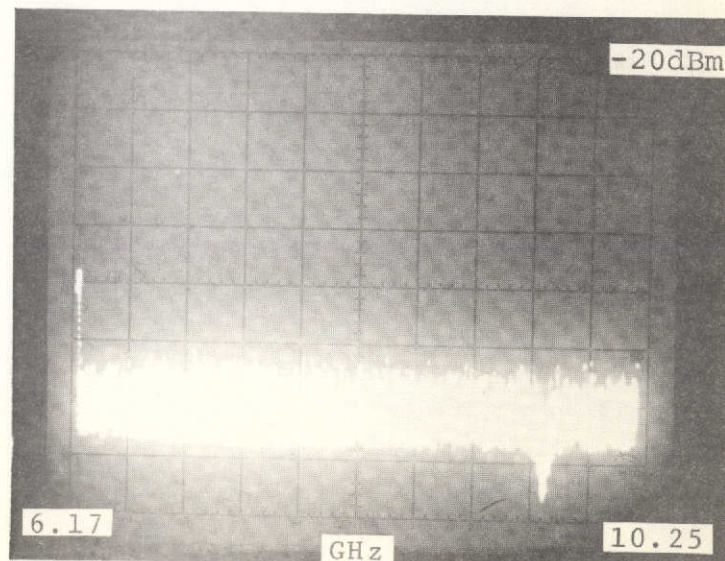
Test Point 3 Filter Pos. NONE

Location STBD F.B. Harbor At-Sea X

Date S-BAND Note RADAR ON Observer Hill/Powell

C-33

PHOTO C-17



Spectrum Display C-18

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 1110

Center Freq. 50 MHz, Bandwidth 100 KHz

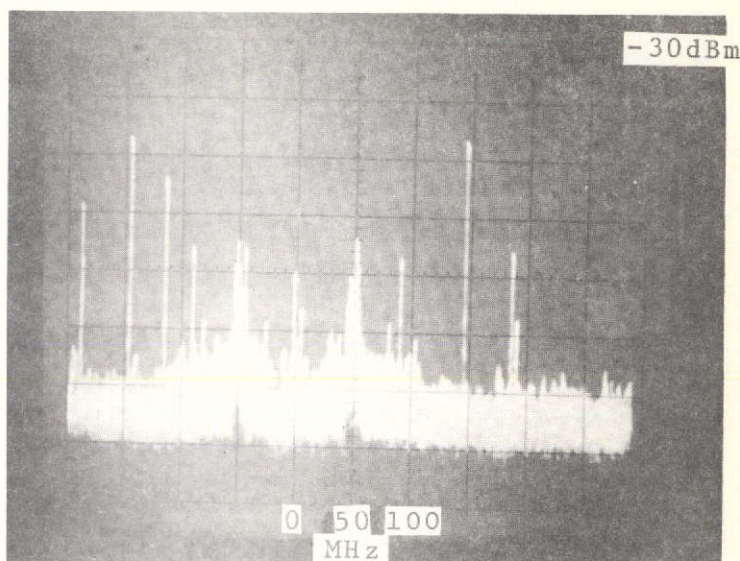
Scan Width 50 MHz/div, Log Ref Level -30 dBm

Test Point 4 Filter Pos. NONE

Location STAD FB Harbor ☒ At-Sea ☐

BOTH RADARS OFF
Date Note Observer ED

PHOTO C-18



Spectrum Display C-19

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 1100

Center Freq. 50 MHz, Bandwidth 100 KHz

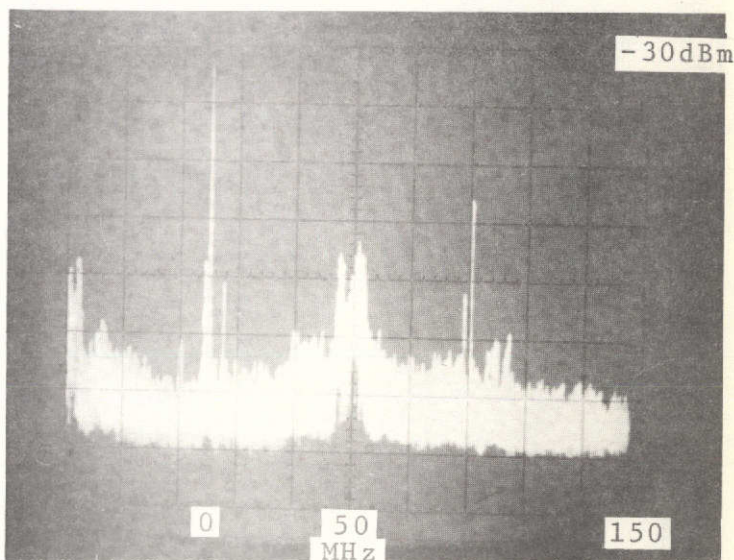
Scan Width 20 MHz/div, Log Ref Level -30 dBm

Test Point 4 Filter Pos. NONE
SCAN TIME 2 milli/sec/div

Location STAD FB Harbor ☒ At-Sea ☐

BOTH RADARS OFF
Date Note Observer ED

PHOTO C-19



Spectrum Display C-20

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/17/74 1105

Center Freq. 50 MHz, Bandwidth 100 KHz

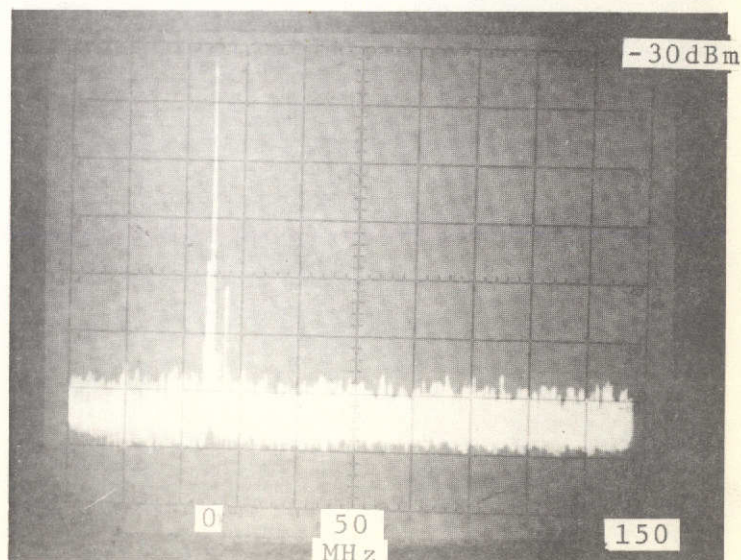
Scan Width 20 MHz/div, Log Ref Level -30 dBm

SPURIOUS RESPONSE IN SPECTRUM ANALYZER
Test Point NONE Filter Pos. NONE

Location STAD FB Harbor ☒ At-Sea ☐

BOTH RADARS OFF
Date Note Observer ED

C-34 PHOTO C-20



Spectrum Display C-21

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/20/74 0805

Center Freq. 50 MHz, Bandwidth 100 KHz

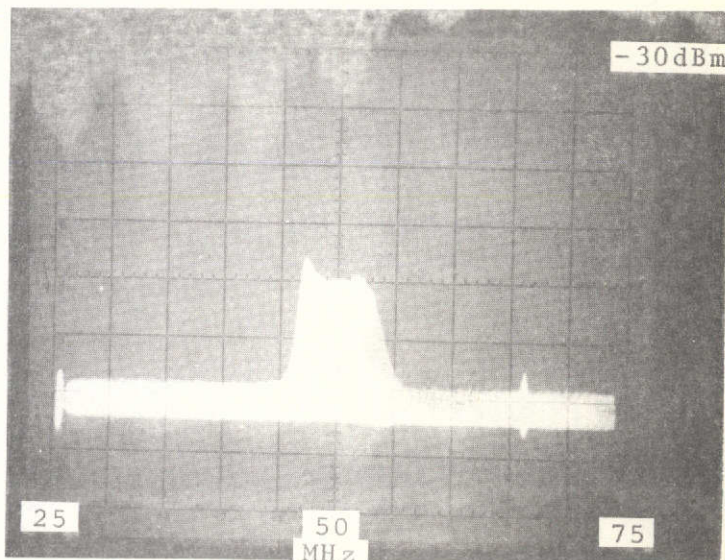
Scan Width 5 MHz/div, Log Ref Level 30 dBm

Test Point 4A After B.P.F. Filter Pos. POINT ① ^{IN ATTEST}

BOTH RADARS ON
Location Harbor SAVANNAH At-Sea

Date Note 1 SEC/DIV SCAN TIME Observer HILL/PINELL

— PHOTO C-21



Spectrum Display C-22

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/20/74 0750

Center Freq. 50 MHz, Bandwidth 100 KHz

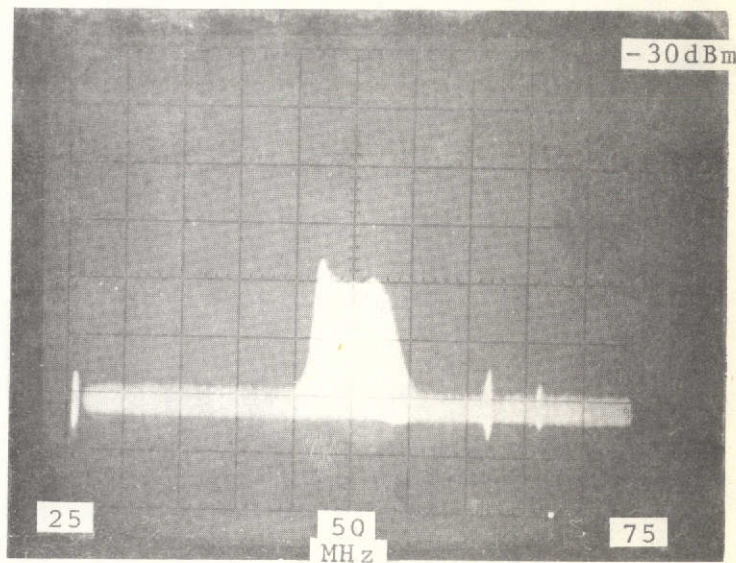
Scan Width 5 MHz/div, Log Ref Level 30 dBm

Test Point 4A After B.P.F. Filter Pos. NONE

BOTH RADARS ON
Location Harbor SAVANNAH At-Sea

Date Note 1 SEC/DIV Observer HILL/PINELL

— PHOTO C-22



C-35

Spectrum Display C-23

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1500 Hrs

Center Freq. 50 MHz, Bandwidth 100 KHz

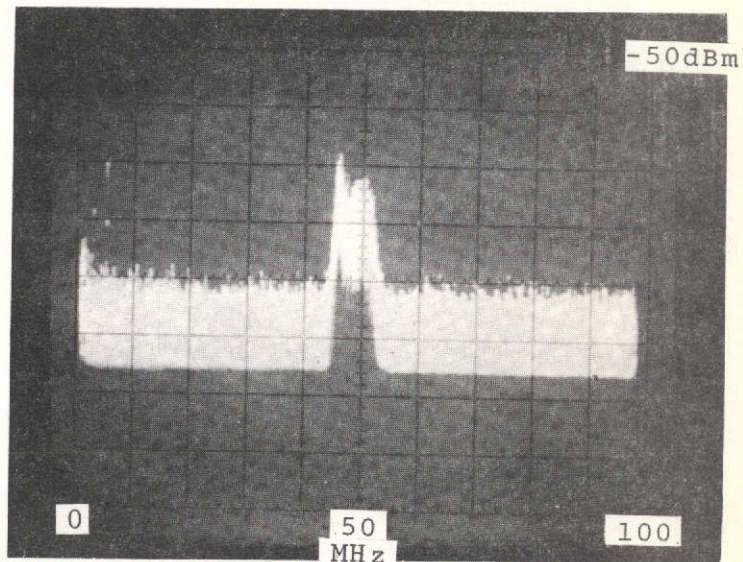
Scan Width 10 MHz/div, Log Ref Level -50 dBm

Test Point 4A Filter Pos. NONE

Location STBD F.B. Harbor At-Sea X

RADARS ON, ANTENNAS STATIONARY
Date _____ Note _____ Observer HILY/POWELL

PHOTO C-23



Spectrum Display C-24

Shipboard L-Band Terminal EMI Survey

Ship ALLIANCE Date 6/19/74 1505 Hrs

Center Freq. 50 MHz, Bandwidth 100 KHz

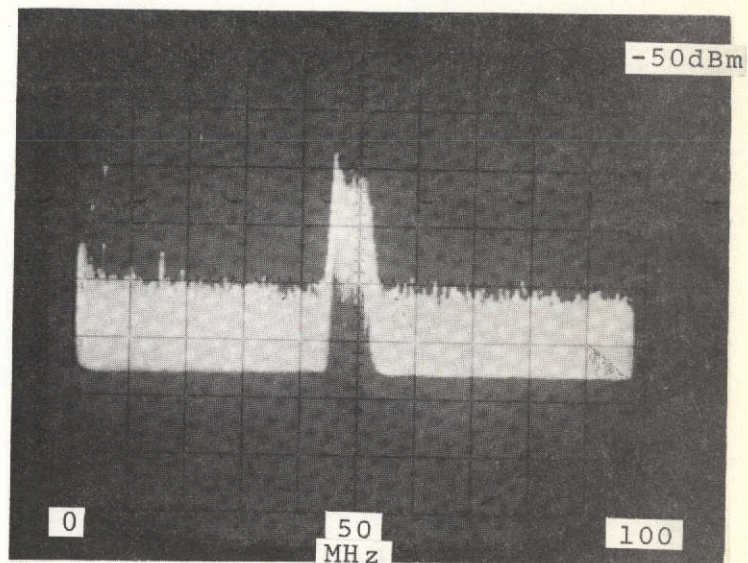
Scan Width 10 MHz/div, Log Ref Level -50 dBm

Test Point 4A ^{FILTER IN} Filter Pos. 1

Location STBD F.B. Harbor At-Sea X

RADARS ON, ANTENNAS STATIONARY
Date _____ Note _____ Observer HIL/POWELL

PHOTO C-24



C-36

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